STORMWATER POLLUTION PREVENTION PLAN & DRAINAGE ANALYSIS

Self Storage Addition 560 Fenimore Road Mamaroneck - New York

February 8, 2018 Revised September 27, 2018



Hudson Engineering & Consulting, P.C.

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1.) NYSDEC Contractor Certification Statement

CONTRACTOR and SUBCONTRACTOR CERTIFICATION STATEMENT

for the New York State Department of Environmental Conservation (DEC) State Pollutant Discharge Elimination System Permit for Stormwater Discharges from Construction Activity (GP-0-15-002)

As per *Part III.A.5* on page 19 of *GP-0-15-002* (effective January 29, 2015):

'Prior to the *commencement of construction activity*, the *owner or operator* must identify the contractor(s) and subcontractor(s) that will be responsible for installing, constructing, repairing, replacing, inspecting and maintaining the erosion and sediment control practices included in the SWPPP; and the contractor(s) and subcontractor(s) that will be responsible for constructing the post-construction stormwater management practices included in the SWPPP. The *owner or operator* shall have each of the contractors and subcontractors identify at least one person from their company that will be responsible for implementation of the SWPPP. This person shall be known as the *trained contractor*. The *owner or operator* shall ensure that at least one *trained contractor* is on site on a daily basis when soil disturbance activities are being performed.'

The owner or operator shall have each contractor and subcontractor involved in soil disturbance sign a copy of the following certification statement before they commence <u>any</u> construction activity:

416 Waverly Avenue	NYR		Village of Mamaroneck	
Name of Construction Site	DEC Permit ID		Municipality (MS4)	
"I hereby certify under penalty of law that I understand and agree to comply with the terms and conditions of the SWPPP and agree to implement any corrective actions identified by the qualified inspector during a site inspection. I also understand that the owner or operator must comply with the terms and conditions of the most current version of the New York State Pollutant Discharge Elimination System ("SPDES") general permit for stormwater discharges from construction activities and that it is unlawful for any person to cause or contribute to a violation of water quality standards. Furthermore, I am aware that there are significant penalties for submitting false information, that I do not believe to be true, including the possibility of fine and imprisonment for knowing violations."				
Responsible Corporate Officer/Partn	er Signature	Date		
Name of above Signatory		Name of Co	mpany	
Title of above Signatory		Mailing Add	lress	
Telephone of Company		City, State a	nd Zip	
Identify the specific elements of the S	SWPPP the cor	ntractor or sub	ocontractor is responsible for:	
The contractor shall be responsible for the				
and sediment control p	ractices for the du	uration of constru	ction activities.	
'TRAINED CONTRACTOR' FOR TH	E CERTIFIEI	O CONTRACT	FOR OR SUBCONTRACTOR	
Name of Trained Employee	Title of Trai	ned Employee		

2.) Narrative

STORMWATER POLLUTION PREVENTION PLAN Self Storage Addition 560 Fenimore Road Mamaroneck - New York

A. INTRODUCTION

This Stormwater Pollution Prevention Plan & Stormwater Analysis presents the proposed Best Management Practices (BMPs) to control erosion, sedimentation, and manage stormwater during the construction of a new four (4) story addition to an existing self storage building, and associated parking and landscaping, located at 560 Fenimore Road (SBL 8-25-70) in the Village of Mamaroneck, Westchester County, New York.

This Plan consists of this narrative and a plan set entitled: "Self Storage Building Addition, 560 Fenimore Road, Village of Mamaroneck, Westchester County, New York", all as prepared by Hudson Engineering and Consulting, P.C., Elmsford, New York, dated September 27, 2018. The design is in accordance with the Village of Mamaroneck requirements. The plans have also been prepared to meet the requirements of the New York State Department of Environmental Conservation (NYSDEC), per the Village code.

B. METHODOLOGY

The stormwater analysis was developed utilizing the Soil Conservation Service (SCS) TR-20 methodologies (HydroCad®) to assist with the drainage analysis and design of the mitigating practice. The "Complex Number" (CN) value determination is based on soil type, vegetation and land use. See Soil Map & Report contained herein. The "Time of Concentration" (T_c) is determined by the time wise longest flow path within each watershed. The CN and T_c data is input into the computer model. This project involves modifications to an existing developed property; therefore, this will be classified as redevelopment per the NYSDEC Phase II regulations.

The Pre and Post Impervious Area coverage was calculated as follows:

Pre and Post Impervious Coverage			
Total Existing Impervious Area	41,390-square feet		
Total Proposed Impervious Area	40,675-square feet		
Total Decrease in Impervious Area	715-square feet		
Percent Decrease	1.73%		

Per Section 9.2.1, B-III of the NYSDEC Manual, 75% of the Water Quality Volume from the disturbed, impervious area, as well as any additional runoff from tributary areas that are undisturbed, can be treated with the use of Alternative Stormwater Management Practices (SMPs), as listed in Section 9.4 of the NYSDEC Stormwater Management Design Manual.

The stormwater management design is based on the NYSDEC "New York State Stormwater Management Design Manual", latest edition and "Controlling Urban Runoff: A practical Manual for Planning and Designing Urban BMP'S", by the Metropolitan Washington Council of Governments. Stormwater quality has been analyzed in accordance with the guidelines set forth in the New York State General Permit for Storm Water Discharge, GP-0-15-002.

C. LIST OF PERMITS

The following is a list of permits and approvals required for the project along with the status.

- Village of Mamaroneck Building Permit Pending
- Village of Mamaroneck Zoning Board Approval Pending
- Village of Mamaroneck Planning Board Approval Pending
- Harbor Coastal Zone Management Commission Pending

D. PRE-DESIGN INVESTIGATIVE ANALYSIS

Due to the site's location partially within the 100-year flood limit line, it has been determined that percolation is not a viable option for stormwater on this site, and conventional stormwater management practices could not be utilized in the stormwater design (i.e. infiltration chambers, infiltration basins, etc.). Therefore, no deep hole testing or percolation testing was performed.

E. PRE-DEVELOPED CONDITION

In the pre-developed conditions, the proposed redevelopment project was modeled as five watersheds, Watershed 1A, 1B, 1C, 2 and 3. All five watersheds are tributary to the design point DP. Each watershed was analyzed as follows:

Watershed 1A is comprised of 2,252 square feet, of which all is impervious in the form of a portion of the existing 2 story building and driveway surface. The watershed has a weighted complex number (CN) value of 98 and a calculated time of concentration (Tc) of 0.8 Minutes. Stormwater from this tributary area flows overland to an existing catch basin located in the center of the parking area. The runoff is then conveyed via pipe to an existing hydrodynamic separator and enters the village's drainage system where it is conveyed to the design point.

Watershed 1B is comprised of 5,979 square feet, of which 5,522 square feet is impervious in the form of a portion of the driveway and 457 square feet is pervious in the form of lawn and landscaping. The watershed has a weighted complex number (CN) value of 97 and a calculated time of concentration (Tc) of 1.1 Minutes. Stormwater from this tributary area flows overland to an existing catch basin located in the center of the parking area. The runoff is then conveyed via pipe to an existing hydrodynamic separator and enters the village's drainage system where it is conveyed to the design point.

Watershed 1C is comprised of 2,849 square feet, of which 2,119 square feet is impervious in the form of a portion of the driveway and 730 square feet is pervious in the form of lawn and landscaping. The watershed has a weighted complex number (CN) value of 93 and a calculated time of concentration (Tc) of 0.9 Minutes. Stormwater from this tributary area flows overland to an existing catch basin located adjacent to the Waverly Avenue right-of-way. The runoff is then conveyed via pipe to an existing hydrodynamic separator and enters the village's drainage system where it is conveyed to the design point.

Watershed 2 is comprised of 10,733 square feet, of which 10,056 square feet is impervious in the form of the existing storage building and 677 square feet is pervious in the form of an existing stormwater planter. The watershed has a weighted complex number (CN) value of 97 and a calculated time of concentration (Tc) of 1.0 Minute (direct entry). The existing stormwater planter was sized to provide water quality treatment for the runoff from this watershed. The planter is designed with overflows to bypass larger storms. All runoff from the planter is conveyed via pipe the hydrodynamic separator and enters the village's drainage system where it is conveyed to the design point.

Watershed 3 is comprised of 22,343 square feet, of which 21,441 is impervious in the form of a portion of the driveway, and buildings and 902 square feet is pervious in the form of lawn and landscaping. The watershed has a weighted complex number (CN) value of 97 and a calculated time of concentration (Tc) of 1.4 Minutes. Stormwater from this tributary area flows overland from the center of the site in a northwesterly direction where it exits the site into the Fenimore Road right-of-way. The runoff then flows overland within the right-of-way to an existing catch basin where it enters the village's drainage system and is conveyed to the design point.

The rate off runoff at the design point are calculated as follows:

Pre-Developed Conditions				
Design 1-Year 10-Year 25-Year				
Point	cfs	cfs	Cfs	
DP	2.47	5.91	7.45	

F. POST-DEVELOPED CONDITION

In the post-developed condition, the project site has been modeled as eight (8) watersheds, Watershed 1A, 1B, 1C, 1D, 2, 3, 3A and 3B. All watersheds are tributary to the design point DP. Each watershed is analyzed as follows:

Watershed 1A is made up of the portion of the proposed parking area adjacent to the proposed building addition. This watershed contains 4,579-square feet of tributary area, which consists of 4,546-square feet of impervious area, with the remaining 33-square feet of area in the form of lawn and landscaping. This watershed has a weighted complex number (CN) value of 98 and a calculated Time of Concentration (Tc) of 0.8 minutes. Stormwater from this area flows overland to an existing catch basin. From here the runoff is captured and conveyed to an existing hydrodynamic separator, where it meets with the runoff from Watersheds 1B, 1C, 1D and 2. The hydrodynamic separator is capable of treating the entire water quality volume from the tributary area. The treated runoff is then conveyed to an existing catch basin located at the corner of Waverly Avenue and Fenimore Road where it enters the village's drainage system and is conveyed to the design point.

Watershed 1B is made up of the portion of the proposed parking area adjacent to the entrance to the existing storage building. This watershed contains 3,079-square feet of tributary area, which consists of 3,008-square feet of impervious area, with the remaining 71-square feet of area in the form of lawn and landscaping. This watershed has a weighted complex number (CN) value of 97 and a calculated Time of Concentration (Tc) of 0.8 minutes. Stormwater from this area flows overland to a relocated catch basin located adjacent to a proposed loading area. From here the runoff is captured and conveyed to an existing hydrodynamic separator, where it meets with the runoff from Watersheds 1A, 1C, 1D and 2. As previously mentioned, the hydrodynamic separator is capable of treating the entire water quality volume from the tributary area. The treated runoff is then conveyed to an existing catch basin located at the corner of Waverly Avenue and Fenimore Road where it enters the village's drainage system and is conveyed to the design point.

Watershed 1C is made up of the portion of the proposed parking area adjacent to the existing stucco building to remain. This watershed contains 3,283-square feet of tributary area, which consists of 3,039-square feet of impervious area, with the remaining 244-square feet of area in the form of lawn and landscaping. This watershed has a weighted complex number (CN) value of 96 and a calculated Time of Concentration (Tc) of 0.9 minutes. Stormwater from this area flows overland to an existing catch basin located just upstream of the existing hydrodynamic separator. From here the runoff is captured and conveyed to the existing hydrodynamic separator, where it meets with the runoff from Watersheds 1A, 1B, 1D and 2. As previously mentioned, the hydrodynamic separator is capable of treating the entire water quality volume from the tributary area. The treated runoff is then conveyed to an existing catch basin located at the corner of

Waverly Avenue and Fenimore Road where it enters the village's drainage system and is conveyed to the design point.

Watershed 1D is made up of the portion of the proposed parking area adjacent to the main driveway entrance. This watershed contains 1,428-square feet of tributary area, which consists of 1,402-square feet of impervious area, with the remaining 26-square feet of area in the form of lawn and landscaping. This watershed has a weighted complex number (CN) value of 98 and a calculated Time of Concentration (Tc) of 0.7 minutes. Stormwater from this area flows overland to a proposed trench drain located across the driveway entrance. From here the runoff is captured and conveyed to an existing hydrodynamic separator, where it meets with the runoff from Watersheds 1A, 1B, 1C and 2. As previously mentioned, the hydrodynamic separator is capable of treating the entire water quality volume from the tributary area. The treated runoff is then conveyed to an existing catch basin located at the corner of Waverly Avenue and Fenimore Road where it enters the village's drainage system and is conveyed to the design point.

Watershed 2 is made up of the existing roof area and associated stormwater planter. This watershed contains 10,733-square feet of tributary area, which consists of 10,056-square feet of impervious area, with the remaining 677-square feet of area in the form of an existing stormwater planter. This watershed has a weighted complex number (CN) value of 97 and a direct entry Time of Concentration (Tc) of 1.0 minute. Stormwater from this area is collected via a series of roof drains and is conveyed directly to an existing stormwater planter located adjacent to the existing building. The stormwater planter is sized to treat the entire water quality volume from the watershed, as well as bypass storm events up to and including the 25-year storm. From here the treated runoff is conveyed to an existing hydrodynamic separator, where it meets with the runoff from Watersheds 1A, 1B, 1C and 1D. The treated runoff is then conveyed to an existing catch basin located at the corner of Waverly Avenue and Fenimore Road where it enters the village's drainage system and is conveyed to the design point.

Watershed 3 is made up of a portion of the existing 2-story building, and sidewalk and landscaped area encompassing the property. This watershed contains 2,952 square feet of tributary area, which consists of 1,297 square feet of impervious area, with the remaining 1,655 square feet pervious area. The watershed has a weighted complex number (CN) value of 85 and a calculated time of concentration (Tc) of 0.5 minutes (direct entry). The runoff flows overland within the right-of-way to an existing catch basin where it enters the village's drainage system and is conveyed to the design point.

Watershed 3A is made up of the proposed roof area and associated stormwater planter. This watershed contains 14,755-square feet of tributary area, which consists of 14,082-square feet of impervious area, with the remaining 673-square feet of area in the form of a proposed stormwater planter. This watershed has a weighted complex number (CN) value of 97 and a direct entry Time of Concentration (Tc) of 1.0 minute. Stormwater from this area is collected via a

series of roof drains and is conveyed directly to a proposed stormwater planter, which has been sized to treat the entire water quality volume from watershed 3A and 3B, as well as bypass storm events up to and including the 25-year storm. From here the treated runoff is conveyed to an existing catch basin located approximately 90 feet from the intersection of Fenimore road and Waverly Avenue where it enters the village's drainage system and is conveyed to the design point.

Watershed 3B is made up of a portion of the driveway area, existing 2 story building and landscaped area located along Fenimore Road. This watershed contains 3,347-square feet of tributary area, which consists of 3,245-square feet of impervious area, with the remaining 102-square feet of area in the form of a proposed stormwater planter. This watershed has a weighted complex number (CN) value of 97 and a Time of Concentration (Tc) of 1.0 minute. Stormwater from this area originates adjacent to the existing two story building and flows in a easterly direction where it flows into the proposed stormwater planter. The stormwater planter has been sized to treat the entire water quality volume from watershed 3A and 3B, as well as bypass storm events up to and including the 25-year storm. From here the treated runoff is conveyed to an existing catch basin located approximately 90 feet from the intersection of Fenimore road and Waverly Avenue where it enters the village's drainage system and is conveyed to the design point.

The rate off runoff at the design point are calculated as follows:

Post-Developed Conditions				
Design 1-Year 10-Year 25-Year				
Point	cfs	cfs	Cfs	
DP	2.38	5.83	7.10	

G. SUMMARY OF FLOWS

Pre- and Post-Developed Conditions					
Design 1-Year 10-Year					
Point	cfs	cfs	Cfs		
Pre-	2.47	5.91	7.45		
Post-	2.38	5.83	7.10		

Post developed flows at the design point are less than those in the predeveloped conditions.

H. WATER QUALITY VOLUME

The Water Quality Volume (WQv) calculations were performed for each watershed as follows:

WATERSHEDS 1A, 1B, 1C & 1D

P= 90% Rainfall 1.5 -inches

A_i = Impervious Area = 11,995 -square feet

 $A_i = 0.2754$ -acres

 $A_t = Tributary Area = 12,369$ -square feet

 $A_t = 0.2840 - acres$

I = % Impervious = 96.98%

 R_v = 0.05+0.009(I); where I = Percent Impervious written as a percent

 $R_v = 0.923$ (0.20 minimum)

 $R_v = 0.923$

 $WQ_v = \frac{(P \times R_v \times A_t)}{12} = 0.03275$ acre-feet = 1426.74 cubic feet

Rainfall = 1.69 -inches \rightarrow 1435 cubic feet OKAY

The Water Quality Volume (WQv) from the proposed parking area comprises of approximately 41.15% of the overall WQv for the entire property. This volume is equal to a 1.69-inch storm event from the watershed, which produces a flow rate of approximately 0.53-cfs*. The entire volume is treated via an existing AquaSwirl AS-2 hydrodynamic device, which is capable of treating up to 1.10-cfs. The existing device is also capable of bypassing the 25-year storm event from the watershed. Water Quality routing calculations are contained within Section 8 of this report. The AquaSwirl Sizing Chart is contained within Section 9 of this report.

*Note, the existing hydrodynamic separator also receives flows from watershed 2. For the water quality storm event the peak flow is 0.56 cfs.

WATERSHED 2

$$A_i$$
 = Impervious Area = 10,056 -square feet

$$A_i = 0.2309$$
 -acres

$$A_t = Tributary Area = 10,733$$
 -square feet

$$A_t = 0.2464$$
 -acres

 R_v = 0.05+0.009(I); where I = Percent Impervious written as a percent

$$R_v = 0.893$$
 (0.20 minimum)

$$R_v = 0.893$$

$$WQ_v = \frac{(P \times R_v \times A_t)}{12} = 0.02751 \text{ acre-feet} = 1198.38 \text{ cubic feet}$$

The Water Quality Volume (WQv) from the existing roof area comprises of approximately 24.94% of the overall WQv for the entire property. This volume is equal to a 1.67-inch storm event. The entire volume is treated via an existing Stormwater Planter, which was previously approved by the Village and was designed to treat the entire WQV from this watershed. The existing planter is also capable of bypassing the 25-year storm event from the watershed without overflow. Water Quality routing calculations are contained within Section 8 of this report.

WATERSHED 3A & 3B

$$A_i$$
 = Impervious Area = 17,327 -square feet

$$A_i = 0.3978$$
 -acres

$$A_t = Tributary Area = 18,102$$
 -square feet

$$A_t = 0.4156$$
 -acres

 R_v = 0.05+0.009(I); where I = Percent Impervious written as a percent

$$R_v = 0.911$$
 (0.20 minimum)

$$R_v = 0.911$$

$$WQ_v = \frac{(P \times R_v \times A_t)}{12} = 0.04735 \text{ acre-feet} = 2062.43 \text{ cubic feet}$$

The Water Quality Volume (WQv) from the proposed roof area comprises of approximately 33.91% of the overall WQv for the entire property. This volume is equal to a 1.69-inch storm event. The entire volume is treated via a proposed Stormwater Planter with a Focal Point biofilter. The proposed planter is also capable of bypassing the 25-year storm event from the watershed without overflow. The Focal Point bio filter system is approved as a proprietary practice for redevelopment under the NYSDEC guidelines. Additional information for this practice has been provided in Section 10 of this report. Water Quality routing calculations are contained within Section 8 of this report.

100% of the Water Quality Volume is treated with a combination of a proposed stormwater planter for all new roof area, an existing stormwater planter for the existing roof area, and an AquaSwirl AS-2 hydrodynamic device for the existing/revised parking area. All practices have also been sized to bypass the 25-year storm event. Each practice is an approved Alternate SMP, as outlined in Section 9.4 of the NYSDEC Stormwater Management Design Manual.

I. NYSDEC TABLE 3.1 DESIGN REGULATIONS:

Each mitigation practice is contained in Table 3.1 of the NYSDEC design regulations and is discussed below.

- Preservation of Undisturbed Areas: Permanent conservation easements of undisturbed areas are not proposed for this site
- Preservation of Buffers. See above.
- Reduction of Clearing and Grading: All construction is occurring in areas previously disturbed.
- Locating Development in Less Sensitive Areas: No development is planned within sensitive areas.
- Open Space Design: Not applicable to this application.
- Soil Restoration: As required, all disturbed soil areas will be "deep tilled" prior to the establishment of ground cover. Deep tilling restores the absorptive quality of the soil.
- Roadway Reduction: No roadways are being proposed as part of this application.
- Sidewalk Reduction: All sidewalks have been designed to the minimum extent possible per the Village of Mamaroneck requirements, in order meet the required pedestrian traffic on and off-site.
- Driveway Reduction: All driveways have been designed to the minimum extent possible to provide adequate access for the proposed use.
- Cul-de-sac Reduction: No Cul-de-sacs are being proposed as part of this application.
- Building Footprint Reduction: The proposed building footprint is considered the minimum footprint desired for this use.
- Parking Reduction: Parking for the proposed use has been provided to the maximum extent possible.
- Conservation of Natural Areas: Not applicable to this application.
- Sheet Flow to riparian buffers or filter strips: Not applicable to this application.
- Vegetated Open Swale: An "O-Type Swale" is not applicable to this site.
- Tree Planting/Tree Boxes: Landscaped Islands have been provided wherever possible.
- Disconnection of Rooftop Runoff: Not applicable to this application.
- Stream Daylighting for Redevelopment Projects: Not applicable to this application.
- Rain Gardens: Due to the location of the property within the existing 100year flood zone, standard exfiltration practices were determined to be ineffective for this application.
- Green Roof: Green roof technology could be incorporated into the design if desired, however, 100% of the water quality volume is already being

- treated via existing and proposed stormwater planters and an existing hydrodynamic separator.
- Stormwater Planters: Stormwater Planters have been incorporated into the design to treat the runoff from both existing and proposed roof areas.
- Rain tank/Cistern: Rain tanks/Cisterns could be incorporated if desired.
- Porous Pavement: Porous Pavement could be incorporated into the design, however, due to the location of the property within the existing 100-year flood zone, standard exfiltration practices were determined to be ineffective for this application.

J. CONSTRUCTION PHASE

During the construction phase of the project, a sediment and erosion control plan shall be implemented in accordance with the New York State Department of Environmental Conservation's Best Management Practices (BMP). The primary goals of the sediment and erosion control plan are to prevent the tracking of dirt and mud onto adjacent roads, to prevent mud and silt from entering into existing and proposed drainage facilities, and to protect the receiving waters from contamination during the construction.

<u>During construction, the party responsible for implementing the temporary (during construction) Stormwater Management facilities Maintenance Program will be the owner.</u> Contact information will be filed with the Village.

A New York State Professional Engineer or Certified Professional In Erosion and Sediment Control (P.E. or CPESC) shall conduct an assessment of the site prior to the commencement of construction and certify in an inspection report that the appropriate erosion and sediment controls shown on the plan have been adequately installed and/or implemented to ensure overall preparedness of the site for construction. Following the commencement of construction, site inspections shall be conducted by the P.E. or CPESC at least every 7 calendar days and within 24 hours of the end of a storm event of 0.5 inches or greater.

During each inspection, the representative shall record the following:

- On a site map, indicate the extent of all disturbed site areas and drainage pathways. Indicate site areas that are expected to undergo initial disturbance or significant site work within the next 14-day period;
- 2. Indicate on a site map all areas of the site that have undergone temporary or permanent stabilization;
- 3. Indicate all disturbed site areas that have not undergone active site work during the previous 14-day period;
- 4. Inspect all sediment control practices and record approximate degree of sediment accumulation as a percentage of the sediment storage volume;

- 5. Inspect all erosion and sediment control practices and record all maintenance requirements. Identify any evidence of rill or gully erosion occurring on slopes and any loss of stabilizing vegetation or seeding/mulching. Document any excessive deposition of sediment or ponding water along the barrier. Record the depth of sediment within containment structures and any erosion near outlet and overflow structures.
- 6. All identified deficiencies.

The construction manager shall maintain a record of all inspection reports in a site logbook. The site logbook shall be maintained on-site and be made available to the Village of Mamaroneck. A summary of the site inspection activities shall be posted on a monthly basis in a public accessible location at the site.

The projects anticipated start date is Fall 2018 and the anticipated completed date is Fall of 2019.

K. CONSTRUCTION SEQUENCING

The following erosion control schedule shall be utilized:

- 1. Install construction entrance to the development area.
- 2. Establish construction staging area.
- 3. Install tree protection on trees as noted on plans.
- 4. Selective vegetation removal for silt fence installation.
- 5. Install silt fence down slope of all areas to be disturbed as shown on the plan.
- 6. Remove trees where necessary (clear & grub) for the proposed construction.
- 7. Strip topsoil and stockpile at the locations specified on the plans (up gradient of erosion control measures). Temporarily stabilize topsoil stockpiles (hydroseed during may 1st through october 31st planting season or by covering with a tarpaulin(s) november 1st through april 30th. Install silt fence around toe of slope.
- 8. Demolish any existing site features and/or structures noted as being removed on the construction documents, and dispose of off-site.
- 9. Rough grade site.

- 10. Install additional silt fencing as necessary.
- 11. Rough grade parking lot and install trench drains and drain inlets, as well as all associated onsite piping.
- 12. Obtain street opening permit for drainage connection to existing catch basin in Fenimore Road, as well as proposed curb cut widenings.
- 13. Install drainage work tributary to existing municipal catch basin in Fenimore Road up to location of proposed stormwater planter.
- 14. Excavate and construct foundations for new building.
- 15. Construct stormwater planter adjacent to building addition.
- 16. Construct building. Install and connect all roof drain leaders to previously installed stormwater planter.
- 17. Install curbing, and sub-base courses. Fine grade and seed all disturbed areas. Spread salt hay over seeded areas.
- 18. Install bituminous concrete top course.
- 19. Clean pavement, drain lines, catch basins and pretreatment devices. Clean exfiltration/attenuation galleries.
- 20. Remove all temporary soil erosion and sediment control measures after the site is stabilized with vegetation.
- * Soil erosion and sediment control maintenance must occur weekly and prior to and after every ½" or greater rainfall event.

L. EROSION AND SEDIMENT CONTROL COMPONENTS

The primary aim of the soil and sediment control measures is to reduce soil erosion from areas stripped of vegetation during and after construction and to prevent silt from reaching the off-site drainage structures and downstream properties. As outlined in the Construction Sequencing schedule, the Sediment and Erosion Control Components are an integral component of the construction sequencing and will be implemented to control sedimentation and re-establish vegetation as soon as practicable.

Planned erosion and sedimentation control practices during construction include the installation, inspection and maintenance of the inlet protection, soil stockpile areas, diversion swales, sediment traps and silt fencing. General land grading practices, including land stabilization and construction sequencing are also integrated into the Sediment and Erosion Control Plan. Dust control is not expected to be a problem due to the relatively limited area of exposure, the

undisturbed perimeter of trees around the project area and the relatively short time of exposure. Should excessive dust be generated, it will be controlled by sprinkling.

All proposed soil erosion and sediment control practices have been designed in accordance with the following publications:

- New York State standards and Specifications for Urban Erosion and Sediment Control, latest edition.
- New York State General Permit for Stormwater Discharges, GP-0-15-002 (General permit).
- "Reducing the Impacts of Stormwater Runoff from New Development", as published by the New York State Department of Environmental Conservation (NYSDEC), second edition, April, 1993.

The proposed soil erosion and sediment control devices include the planned erosion control practices outlined below. Maintenance procedures for each erosion control practice have also been outlined below.

SILT FENCE

Silt fence (geo-textile filter cloth) shall be placed in locations depicted on the approved plans. The purpose of the silt fence is to reduce the velocity of sediment laden stormwater from small drainage areas and to intercept the transported sediment load. In general, silt fence shall be used at the toe of slopes or intermediately within slopes where obvious channel concentration of stormwater is not present.

Maintenance

Silt fencing shall be inspected at a minimum of once per week and prior to and within 48 hours following a rain event ½" or greater. Inspections shall include ensuring that the fence material is tightly secured to the woven wire and the wire is secured to the wood posts. In addition, overlapping filter fabric shall be secure and the fabric shall be maintained a minimum of six (6) inches below grade. In the event that any "bulges" develop in the fence, that section of fence shall be replaced within 48 hours with new fence section. Any sediment build-up against the fence shall be removed within 48 hours and deposited on-site a minimum of 100 feet outside of any wetland or watercourse.

INLET PROTECTION

After driveway catch basins and surface inlets have been installed, these drain inlets will receive stormwater from the driveway, Temporary Diversion Swales and surrounding overland watersheds. In order to protect the

receiving waters from sedimentation, the contractor shall install ¾ inch stone aggregate around the perimeter of all catch basins and surface inlets as illustrated on the approved plans. This barrier will allow stormwater to be filtered prior to reaching the basin inlet grate.

Maintenance

The stone aggregate shall be inspected weekly prior to and within 48 hours following a rain event ½" or greater. Care shall be taken to ensure that all stone aggregate are properly located and secure and do not become displaced. The stone aggregate shall be inspected for accumulated sediments and any accumulated sediment shall be removed from the device and deposited not less than 100 feet from wetland or watercourse.

TREE PROTECTION

All significant trees to be preserved located within the limits of disturbance and on the perimeter of the disturbance limits shall be protected from harm by erecting a 3' high (minimum) snow fence completely surrounding the tree. Snow fence should extend to the drip-line of the tree to be preserved. Trees designated to be protected shall be identified during the staking of the limits of disturbance for each construction phase.

Maintenance

The snow fence shall be inspected daily to ensure that the perimeter of the fence remains at the drip-line of the tree to be preserved. Any damaged portions of the fence shall be repaired or replaced within 48 hours. Care shall also be taken to ensure that no construction equipment is driven or parked within the drip-line of the tree to be preserved.

SOIL/SHOT ROCK STOCKPILING

All soil and shot rock stripped from the construction area during grubbing and mass grading shall be stockpiled in locations approved by the Town/Village's representative, but in no case shall they be placed within 100' of a wetland or watercourse. The stockpiled soils shall be re-used during finish-grading to provide a suitable growing medium for plant establishment. Soil stockpiles shall be protected from erosion by vegetating the stockpile with rapidly – germinating grass seed or covering the stockpile with tarpaulin and surrounding it with either silt fence.

Maintenance

Sediment controls (silt fence) surrounding the stockpiles shall be inspected according to the recommended maintenance outline above. All stockpiles shall be inspected for signs of erosion or problems with seed establishment weekly and prior to and within 48 hours following a rain event ½" or greater.

GENERAL LAND GRADING

The intent of the Erosion & Sediment Control Plan is to control disturbed areas such that soils are protected from erosion by temporary methods and, ultimately, by permanent vegetation. Where practicable, all cut and fill slopes shall be kept to a maximum slope of 2:1. In the event that a slope must exceed a 2:1 slope, it will be stabilized with stone riprap. On fill slopes, all material will be placed in layers not to exceed 12 inches in depth and adequately compacted. Where practicable, diversion swales shall be constructed on the top of all fill embankments to divert any overland flows away from the fill slopes.

SURFACE STABILIZATION

All disturbed will be protected from erosion with the use of vegetative measures (i.e., grass seed mix, sod) hydromulch netting or hay. When activities temporarily cease during construction, soil stockpiles and exposed soil should be stabilized by seed, mulch or other appropriate measures as soon as possible, but in no case more than 14 days after construction activity has ceased. All seeded areas will be re-seeded areas as necessary and mulch according to the site plan to maintain a vigorous, dense vegetative cover,

Erosion control barriers consisting of silt fencing shall be placed around exposed areas during construction. Where exposed areas are immediately uphill from a wetland or watercourse, the erosion control barrier will consist of double rows of silt fencing. Any areas stripped of vegetation during construction will be vegetated and/or mulch as soon as possible, but in no case more than 14 days to prevent erosion of the exposed soils. And topsoil removed during construction will be temporarily stockpiled for future use in grading and landscaping.

As mentioned above, temporary vegetation will be established to protect exposed soil areas during construction. If growing conditions are not suitable for the temporary vegetation, mulch will be used to the satisfaction of the Commissioner of Public Works. Materials that may be used for mulching include straw, hay, salt hay, wood fiber, synthetic soil stabilizers, mulch netting, sod or hydromulch. In site areas where significant erosion potential exists (steep slopes) and where specifically directed by the Town/Village's representative, Curlex Excelsior erosion control blankets (manufactured by American Excelsior, or approved equal) shall be installed. A permanent vegetative cover will be established upon completion of construction of those areas that have been brought to finish-grade and to remain undisturbed.

DEWATERING

Prevent surface water and subsurface or ground water from flowing into excavations and trenches. Pump out any accumulated water.

Do not allow water to accumulate in excavations or trenches. Remove water from all excavations immediately to prevent softening of foundation bottoms, undercutting footings, and soil changes detrimental to the stability of subgrades and foundations. Furnish and maintain pumps, sumps, suction and discharge piping systems, and other system components necessary to convey the water away from the Site.

Convey water removed from excavations, and rain water, to collecting or runoff area. Cut and maintain temporary drainage ditches and provide other necessary diversions outside excavation limits for each structure. Do not use trench excavations as temporary drainage ditches.

Provide temporary controls to restrict the velocity of discharged water as necessary to prevent erosion and siltation of receiving areas.

M. CONSTRUCTION PRACTICES TO MINIMIZE STORMWATER CONTAMINATION

General:

Adequate measures shall be taken to minimize contaminant particles arising from the discharge of solid materials, including building materials, grading operations, and the reclamation and placement of pavement, during project construction, including but not limited to:

- Building materials, garbage, and debris shall be cleaned up daily and deposited into dumpsters, which will be periodically removed from the site and appropriately disposed of. All dumpsters and containers left on-site shall be covered and surrounded with silt fence in order to prevent contaminants from leaving the site. Silt fencing shall be inspected on a weekly basis.
- Dump trucks hauling material from the construction site will be covered with a tarpaulin.
- The paved street adjacent to the site entrance will be swept daily to remove excess mud, dirt, or rock tracked from the site.
- Petroleum products will be stored in tightly sealed containers that are clearly labeled.
- All vehicles on site will be monitored for leaks and receive regular preventive maintenance to reduce the chance of leakage.

- All spills will be cleaned up immediately upon discovery. Spills large enough to reach the storm system will be reported to the National Response Center at 1-800-424-8802.
- Materials and equipment necessary for spill cleanup will be kept in the temporary material storage trailer onsite. Equipment will include, but not be limited to, brooms, dust pans, mops, rags, gloves, goggles, kitty litter, sand, saw dust, and plastic and metal trash containers.
- All paint containers and curing compounds will be tightly sealed and stored when not required for use. Excess paint will not be discharged to the storm system, but will be properly disposed according to the manufacturer's instructions.
- Sanitary waste will be collected from portable units a minimum of two times a week to avoid overfilling. All sanitary waste units shall be surrounded by silt fence to prevent contaminants from leaving the site. Silt fencing shall be inspected on a weekly basis.
- Any asphalt substances used on-site will be applied according to the manufacturer's recommendation.
- Fertilizers will be stored in a covered shed and partially used bags will be transferred to a sealable bin to avoid spills and will be applied only in the minimum amounts recommended by the manufacturer and worked into the soil to limit exposure to stormwater.
- No disturbed area shall be left un-stabilized for longer than 14 days during the growing season.
- When erosion is likely to be a problem, grubbing operations shall be scheduled and performed such that grading operations and permanent erosion control features can follow within 24 hours thereafter.
- As work progresses, patch seeding shall be done as required on areas previously treated to maintain or establish protective cover.
- Drainage pipes and swales/ditches shall generally be constructed in a sequence from outlet to inlet in order to stabilize outlet areas and ditches before water is directed to the new installation or any portion thereof, unless conditions unique to the location warrant an alternative method.

Spill Control & Spill Response:

 For all hazardous materials stored on site, the manufacturer's recommended methods for spill clean up will be clearly posted. Site

- personnel will be made aware of the procedures, and the locations of the information and cleanup supplies.
- Appropriate cleanup materials and equipment will be maintained by the Contractor in the materials storage area on-site. As appropriate, equipment and materials may include items such as booms, dust pans, mops, rags, gloves, goggles, kitty litter, sand, sawdust, and plastic and metal trash containers specifically for clean up purposes.
- All spills will be cleaned immediately after discovery and the materials disposed of properly.
- The spill area will be kept well ventilated and personnel will wear appropriate protective clothing to prevent injury from contact with a hazardous substance.
- After a spill, a report will be prepared describing the spill, what caused it, and the cleanup measures taken. The spill prevention plan will be adjusted to include measures to prevent this type of spill from reoccurring, as well as clean up instructions in the event of reoccurrences.
- The Contractor's site superintendent, responsible for day-to-day operations, will be the spill prevention and cleanup coordinator. The Contractor is responsible for ensuring that the site superintendent has had appropriate training for hazardous materials handling, spill management, and cleanup.
- The Contractor's site superintendent will be notified immediately when a spill or the threat of a spill is observed. The superintendent will assess the situation and determine the appropriate response.
- If spills represent an imminent threat of escaping erosion and sediment controls and entering receiving waters, personnel will be directed to respond immediately to contain the release and notify the superintendent after the situation has been stabilized.
- Spill kits containing appropriate materials and equipment for spill response and cleanup will be maintained by the Contractor at the site.
- If oil sheen is observed on surface water, action will be taken immediately
 to remove the material causing the sheen. The Contractor will use
 appropriate materials to contain and absorb the spill. The source of the oil
 sheen will also be identified and removed or repaired as necessary to
 prevent further releases.
- If a spill occurs the superintendent or the superintendent's designee will be responsible for completing the spill reporting form and for reporting the spill to the contacts listed below.
- Personnel with primary responsibility for spill response and clean up will receive training by the Contractor's site superintendent or designee. The

- training must include identifying the location of the spill kits and other spill response equipment and the use of spill response materials.
- Spill response equipment will be inspected and maintained as necessary to replace any materials used in spill response activities.

Spill Control Notification:

- A reportable spill is a quantity of five (5) gallons or more or any spill of oil which: (1) violates water quality standards, (2) produces a "sheen" on a surface water, or (3) causes a sludge or emulsion. This spill must be reported immediately to the agencies listed below.
- Any spill of oil or hazardous substance to waters of the state must be reported immediately by telephone to the following agencies:
 - 911 Police, Fire and EMS
 - Village of Mamaroneck Engineering Department
 169 Mount Pleasant Avenue
 Phone: (914) 777-7731
 - Mamaroneck Fire Department
 123 Mamaroneck Avenue
 Phone: (914) 825-8777
 - NYS Department of Environmental Conservation (NYSDEC)
 Spill Reporting Hotline
 (1800) 457–7362
 - National Response Center: (1800) 424-8802
 - Local Emergency Planning Committee (LEPC)
 Westchester County Office of Emergency Management
 200 Bradhurst Avenue
 Hawthorne, NY 10532
 (914) 864–5450
 - Westchester County Department of Health (WCDOH)
 Spill Reporting Hotline
 (914) 813-5000
 - U.S. Environmental Protection Agency (USEPA)
 EPCRA Information Hotline
 1(800) 535–0202
 - U.S. Department of Labor and Occupational Safety and Health Administration (OSHA)

N. STORMWATER MANAGEMENT FACILITIES MAINTENANCE PROGRAM

The following maintenance plan has been developed to maintain the proper function of all drainage and erosion and sediment control facilities:

Erosion & Sediment Control Maintenance:

During the construction of the project, the site erosion and sediment control measures as well as basin embankments and outlet structures will be inspected by the project superintendent once a week and/or within 24 hours following a rainstorm ½" or greater. Any repairs required shall be performed in a timely manner. All sediment removal and/or repairs will be followed within 24 hours by re-vegetation. Remove sediment and correct erosion by re-seed eroded areas and gullies within 7 days.

General Stormwater Facilities Maintenance (Storm Sewer, Catch Basins/Drain Inlets, Manholes, Pre-treatment Device and Subsurface Infiltration System)

All stormwater facilities shall be inspected immediately after completion of construction, and then monthly for the first three (3) months following the completion of the Project. Within the first three (3) months, inspections shall immediately be performed following a large storm event (i.e. producing 1/2" (one-half inch) of rain or greater. Thereafter, these facilities shall be inspected as described as follows. Upon inspection, facilities shall be immediately maintained and/or cleaned as may be required. Any site areas exhibiting soil erosion of any kind shall be immediately restored and stabilized with vegetation, mulch or stone, depending on the area to be stabilized.

Upon each inspection, all visible debris including, but not limited to, twigs, leaf and forest litter shall be removed from the swales, overflow discharge points and frames and grates of drainage structures.

Sumps – Catch Basin/Drain Inlets and Drain Manholes

All catch basin/drain inlets and drain manholes with sumps have been designed to trap sediment prior to its transport to the infiltration practice and, ultimately, downstream. These sumps will require periodic inspection and maintenance to ensure that adequate depth is maintained within the sumps.

All sumps shall be inspected once per month for the first three (3) months (after drainage system has been put into service). Thereafter, all sumps

shall be inspected every four (4) months. The Owner, or their duly authorized representative, shall take measurements of the sump depth.

If sediment has accumulated to 1/2 (one-half) the depth of the sump, all sediment shall be removed from the sump. Sediments can be removed with hand-labor or with a vacuum truck.

The use of road salt shall be minimized for maintenance of roadway and driveway areas.

Hydrodynamic Separator:

The hydrodynamic separator (Aquaswirl unit) shall be inspected every six (6) months (Spring and Fall) for excess sediment accumulation. During dry weather conditions, accumulated sediments shall be vacuumed out when sediment has reached 1/2 (one-half) the capacity of the isolated sump, or when an appreciable level of hydrocarbons and trash has accumulated, whichever occurs first.

Upon completion of construction, the Aquaswirl Unit should be inspected quarterly during the first year in order to develop an appropriate schedule of maintenance. When the sediment pile is within 30 to 36 inches of the water surface, the system should be maintained. A vacuum truck shall be used to remove the accumulated sediment and debris. Refer to manufacturer's literature for detailed maintenance instructions.

Stormwater Planter:

The stormwater planters shall be inspected twice within the first six (6) months, and after each storm event greater than 0.5-inches (Spring and Fall) for excess sediment accumulation and for surface ponding. After the first year, the planter shall be inspected every four (4) months and after storm events greater than the 1-year storm.

During dry weather conditions, all accumulated sediment shall be removed from the planter, and the existing topsoil shall be retiled to promote exfiltration of the stormwater thought the practice.

Routine maintenance activities shall be performed weekly, and shall include running and replacing dead or dying vegetation, plant thinning, and erosion repair.

• FocalPoint Biofilter System:

The Focalpoint Biofilter System shall be inspected twice within the first six (6) months, and after each storm event greater than 1.0-inches (Spring and Fall) for excess sediment accumulation and for surface ponding. After the first year, the planter shall be inspected every six (6) months and after storm events greater than the 1-year storm.

During dry weather conditions, all accumulated sediment shall be removed from the planter, and the existing topsoil shall be retiled to promote exfiltration of the stormwater thought the practice.

Routine maintenance activities shall be performed weekly and shall include running and replacing dead or dying vegetation, plant thinning, and erosion repair.

All maintenance shall be completed in accordance with the manufacturer's guidelines outlined in the Operations & Maintenance manual located in Section 8 of this report.

O. CONCLUSION:

The stormwater management plan proposed meets and exceeds all the requirements set forth by the Village of Mamaroneck and the New York State Department of Environmental Conservation (NYSDEC) for redevelopment projects. Design modification requirements that may occur during the approval process, will be performed and submitted for review to the Village of Mamaroneck.

3.) Extreme Precipitation Table

Extreme Precipitation Tables

Northeast Regional Climate Center

Data represents point estimates calculated from partial duration series. All precipitation amounts are displayed in inches.

Smoothing Yes

State New York

Location

Longitude 73.743 degrees West **Latitude** 40.950 degrees North

Elevation 0 feet

Date/Time Fri, 19 Jan 2018 11:31:10 -0500

Extreme Precipitation Estimates

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.34	0.51	0.64	0.84	1.05	1.31	1yr	0.90	1.23	1.50	1.86	2.31	2.86	3.22	1yr	2.53	3.10	3.58	4.31	4.94	1yr
2yr	0.41	0.63	0.78	1.02	1.28	1.59	2yr	1.11	1.50	1.83	2.26	2.80	3.45	3.87	2yr	3.05	3.72	4.27	5.07	5.75	2yr
5yr	0.47	0.74	0.92	1.24	1.58	2.00	5yr	1.37	1.85	2.31	2.86	3.52	4.31	4.89	5yr	3.82	4.70	5.45	6.38	7.13	5yr
10yr	0.53	0.84	1.06	1.43	1.86	2.37	10yr	1.61	2.18	2.75	3.41	4.19	5.11	5.84	10yr	4.53	5.62	6.56	7.59	8.38	10yr
25yr	0.62	0.98	1.25	1.73	2.31	2.97	25yr	1.99	2.69	3.45	4.30	5.28	6.41	7.40	25yr	5.67	7.11	8.37	9.56	10.39	25yr
50yr	0.70	1.13	1.45	2.02	2.72	3.53	50yr	2.35	3.17	4.11	5.11	6.27	7.60	8.85	50yr	6.73	8.51	10.08	11.38	12.23	50yr
100yr	0.80	1.29	1.66	2.36	3.21	4.19	100yr	2.77	3.73	4.89	6.09	7.46	9.02	10.58	100yr	7.99	10.18	12.13	13.55	14.41	100yr
200yr	0.91	1.48	1.91	2.75	3.79	4.98	200yr	3.27	4.40	5.82	7.26	8.88	10.72	12.66	200yr	9.48	12.18	14.62	16.13	16.97	200yr
500yr	1.09	1.79	2.33	3.38	4.73	6.24	500yr	4.08	5.48	7.32	9.14	11.18	13.47	16.06	500yr	11.92	15.45	18.71	20.33	21.08	500yr

Lower Confidence Limits

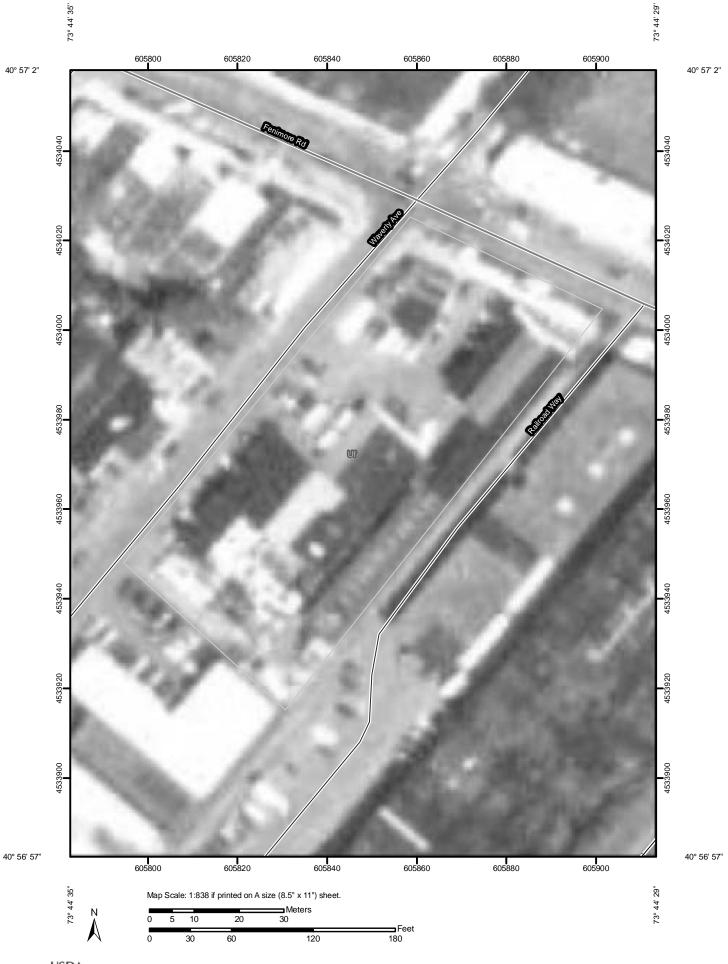
	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.25	0.39	0.47	0.63	0.78	0.88	1yr	0.67	0.86	1.27	1.54	1.96	2.58	2.97	1yr	2.29	2.86	3.31	3.97	4.58	1yr
2yr	0.39	0.61	0.75	1.01	1.25	1.50	2yr	1.08	1.47	1.71	2.19	2.73	3.35	3.76	2yr	2.97	3.61	4.14	4.93	5.61	2yr
5yr	0.44	0.68	0.84	1.16	1.47	1.79	5yr	1.27	1.75	2.02	2.57	3.20	4.03	4.54	5yr	3.56	4.37	5.06	5.95	6.70	5yr
10yr	0.49	0.75	0.93	1.31	1.69	2.04	10yr	1.46	1.99	2.29	2.91	3.58	4.62	5.21	10yr	4.09	5.01	5.90	6.82	7.63	10yr
25yr	0.56	0.85	1.06	1.52	1.99	2.42	25yr	1.72	2.36	2.71	3.42	4.15	5.53	6.22	25yr	4.90	5.98	7.22	8.17	9.07	25yr
50yr	0.62	0.94	1.17	1.69	2.27	2.73	50yr	1.96	2.67	3.09	3.89	4.59	6.32	7.11	50yr	5.60	6.83	8.44	9.34	10.35	50yr
100yr	0.69	1.05	1.31	1.90	2.60	3.09	100yr	2.24	3.02	3.54	4.43	5.12	7.23	8.11	100yr	6.40	7.80	9.85	10.69	11.80	100yr
200yr	0.78	1.17	1.48	2.15	3.00	3.52	200yr	2.59	3.44	4.06	5.05	5.68	8.27	9.27	200yr	7.32	8.91	11.52	12.23	13.47	200yr
500yr	0.91	1.36	1.75	2.54	3.62	4.22	500yr	3.12	4.12	4.88	6.08	8.37	9.87	11.05	500yr	8.73	10.63	14.20	14.60	16.05	500yr

Upper Confidence Limits

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.37	0.58	0.71	0.95	1.17	1.38	1yr	1.01	1.35	1.63	2.14	2.61	3.13	3.48	1yr	2.77	3.35	3.85	4.63	5.26	1yr
2yr	0.42	0.65	0.80	1.08	1.33	1.63	2yr	1.15	1.59	1.90	2.38	3.01	3.55	4.03	2yr	3.15	3.87	4.40	5.25	5.93	2yr
5yr	0.51	0.78	0.97	1.33	1.70	1.99	5yr	1.46	1.95	2.32	3.03	3.75	4.61	5.23	5yr	4.08	5.03	5.85	6.83	7.56	5yr
10yr	0.60	0.92	1.14	1.59	2.05	2.38	10yr	1.77	2.33	2.81	3.67	4.53	5.63	6.42	10yr	4.98	6.17	7.25	8.37	9.12	10yr
25yr	0.74	1.12	1.40	2.00	2.63	3.01	25yr	2.27	2.94	3.64	4.74	5.83	7.31	8.41	25yr	6.47	8.09	9.64	10.99	11.68	25yr
50yr	0.86	1.32	1.64	2.35	3.17	3.61	50yr	2.73	3.52	4.42	5.76	7.06	8.95	10.32	50yr	7.92	9.92	11.95	13.50	14.09	50yr
100yr	1.02	1.54	1.93	2.79	3.82	4.31	100yr	3.30	4.21	5.36	7.00	8.55	10.93	12.68	100yr	9.68	12.20	14.82	16.57	17.01	100yr
200yr	1.20	1.80	2.29	3.31	4.62	5.16	200yr	3.98	5.04	6.49	8.49	10.36	13.35	15.61	200yr	11.82	15.01	18.37	20.38	20.52	200yr
500yr	1.50	2.23	2.87	4.16	5.92	6.52	500yr	5.11	6.37	8.38	10.97	13.30	17.43	20.55	500yr	15.42	19.76	24.41	26.80	26.31	500yr



4.) Soils Maps & Soils Data



MAP LEGEND

Area of Interest (AOI)

Area of Interest (AOI)

Soils

Soil Map Units

Special Point Features

 \odot Blowout

X Borrow Pit

Ж Clay Spot

Closed Depression

Gravel Pit ×

Gravelly Spot ٨

Ճ Landfill

Lava Flow

Marsh or swamp

Mine or Quarry 52

Miscellaneous Water ⊚

Rock Outcrop

◉ Perennial Water

Saline Spot

Sandy Spot

Severely Eroded Spot

Sinkhole ٥

=

Slide or Slip

Sodic Spot

3 Spoil Area

Stony Spot

Wet Spot

Other

Special Line Features

2

Gully

Short Steep Slope

Very Stony Spot

11 Other

Political Features

0 Cities

Water Features

Oceans

Streams and Canals

Transportation

+++

Rails

-

Interstate Highways

~~

US Routes



Major Roads



Local Roads

MAP INFORMATION

Map Scale: 1:838 if printed on A size (8.5" × 11") sheet.

The soil surveys that comprise your AOI were mapped at 1:12,000.

Please rely on the bar scale on each map sheet for accurate map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL: http://websoilsurvey.nrcs.usda.gov

Coordinate System: UTM Zone 18N NAD83

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Westchester County, New York Survey Area Data: Version 4, Dec 14, 2006

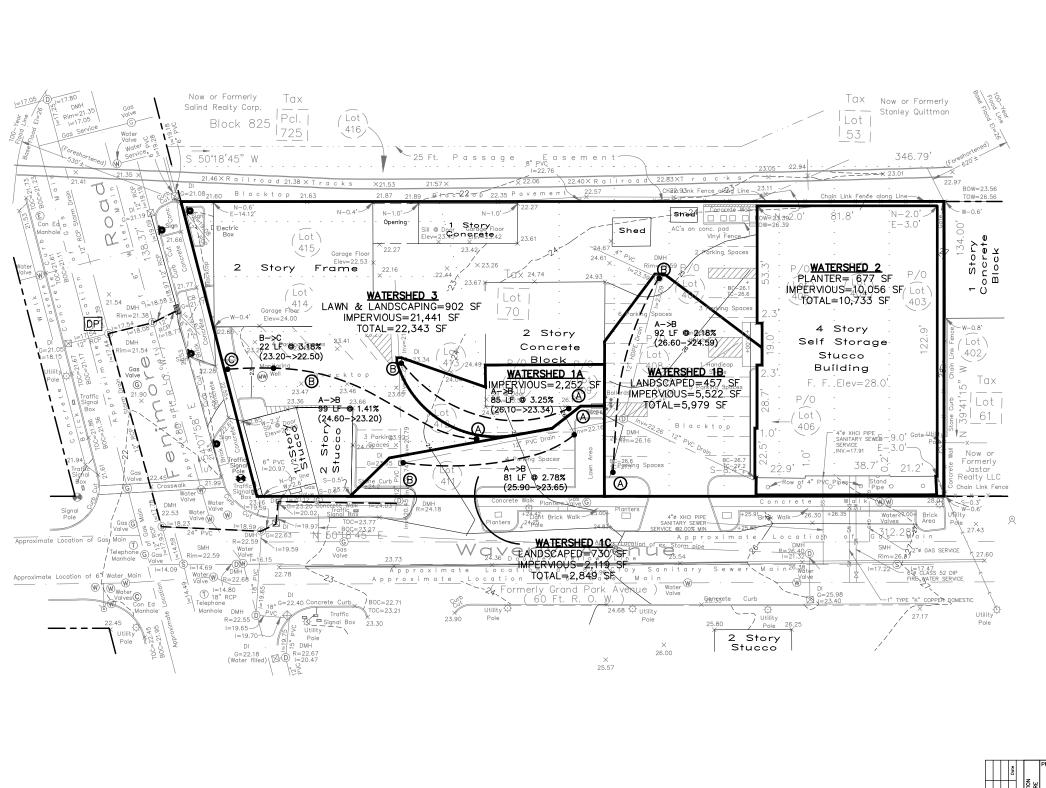
Date(s) aerial images were photographed: 7/31/2006

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Westchester County, New York (NY119)								
Map Unit Symbol Map Unit Name Acres in AOI Percent of AOI								
Uf	Urban land	1.3	100.0%					
Totals for Area of Interest		1.3	100.0%					

	5.) Watershed Maps	
Hudson Engineering & Con	nsulting, P.C.	



WATERSHE SEAL WIND FOR WITHOUT ENGINEERS SEAL WIND THE PLAN NOT WHATERS SEAL WIND THE PLAN NOT WELL WIND THE PLAN NOT WHATERS SEAL WIND THE PLAN NOT WELL WIND T

GRAPHIC SCALE

(IN FEET) 1 inch = 20 ft. SELF STORAGE BUILDING ADDITION 560 FENIMORE ROAD VILLAGE OF MAMARONECK WESTCHESTER COUNTY — NEW YORK

WATERSHED MAP - EXISTING



ENGINEERING

8
CONSULTING, P.C.
45 Knollwood Road - Suite 201
Elmotord, New York 10523

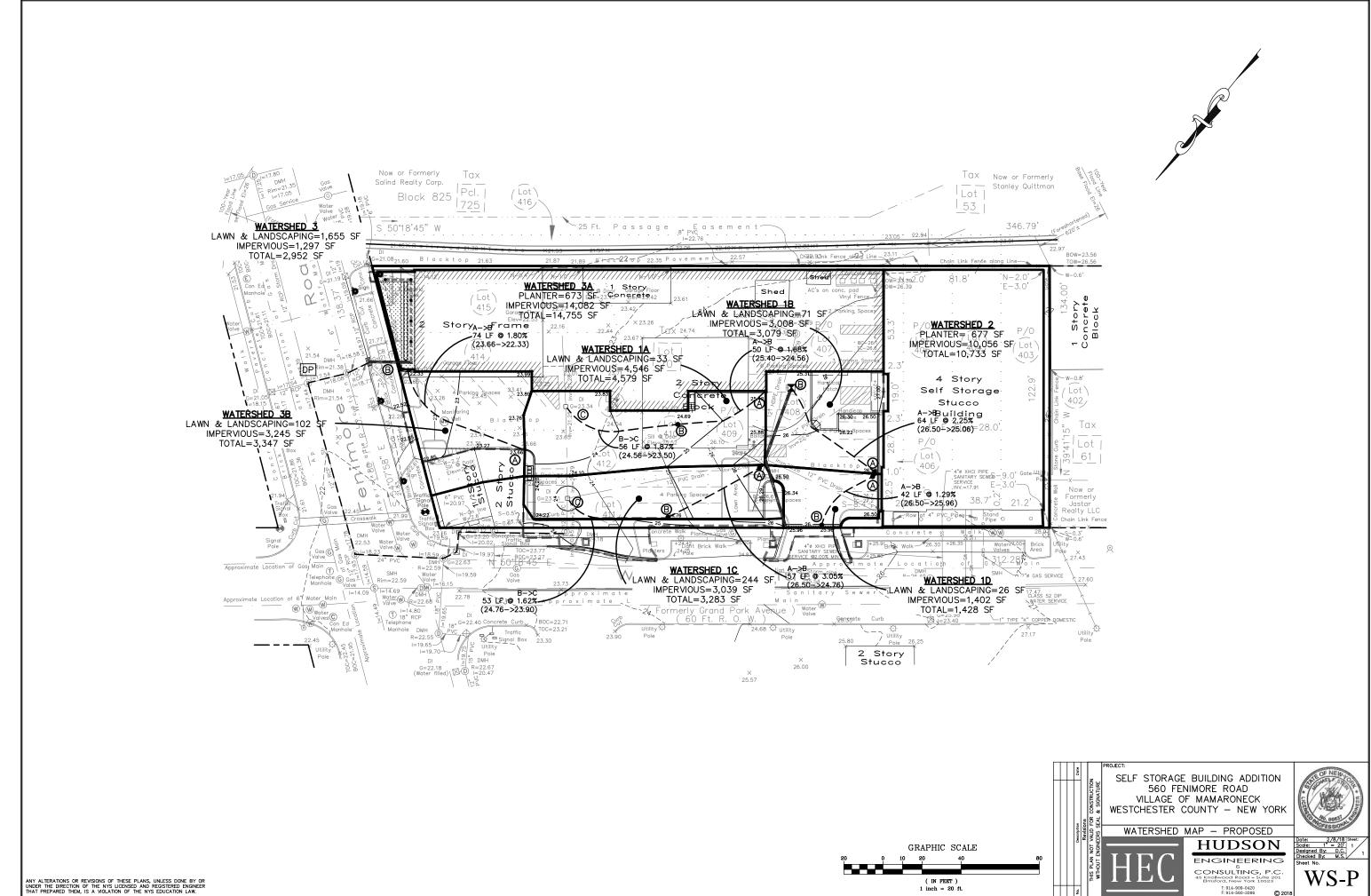
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F1914-550-2086

© 20

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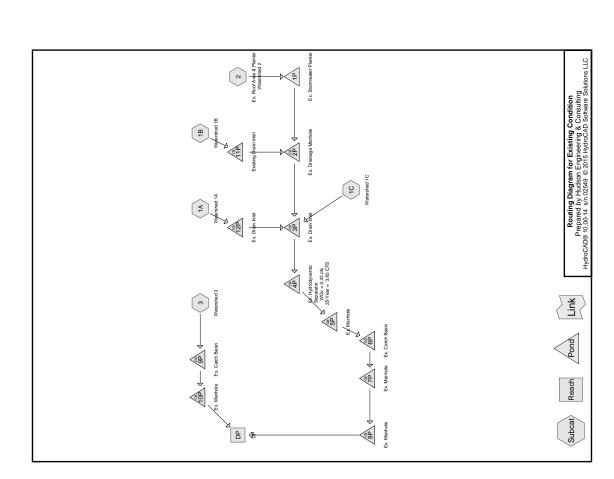
WS-E



1 inch = 20 ft.

ANY ALTERATIONS OR REVISIONS OF THESE PLANS, UNLESS DONE BY OR UNDER THE DIRECTION OF THE NYS LICENSED AND REGISTERED ENGINEER THAT PREPARED THEM, IS A VIOLATION OF THE NYS EDUCATION LAW.

6.) Pre-Developed Analysis of the 1-, 10-, and 25- year Extreme Storm Events



Page 2

Type Prepared by Hudson Engineering & Consulting HydroCAD® 10.00-14 s/n 02549 © 2015 HydroCAD Software Solutions LLC

Summary for Subcatchment 1A: Watershed 1A

493 cf, Depth= 2.63" 0.17 dfs @ 12.01 hrs, Volume= Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 1-Year Rainfall=2.86"

				P2= 3.45"		
				n= 0.011		
	uilding	rea	Tc Length Slope Velocity Capacity Description in) (feet) (ft/ft) (ft/sec) (cfs)	Sheet Flow, A-B Smooth surfaces n= 0.011 P2= 3.45"		
& part of bu	2,252 98 Parking Lot & part of building 2,252 100.00% Impervious Area	& part of bu pervious Ar	& part of bu pervious Ar	pervious A	Capacity (cfs)	
Area (sf) CN Description	arking Lot	ml %00.00	Velocity (ft/sec)	85 0.0325 1.68		
CN	98 P	1	Slope (ft/ft)	0.0325		
ea (sf)	2,252	2,252	Length (feet)	82		
Ā	*		Tc (min)	0.8		

Summary for Subcatchment 1B: Watershed 1B

1,255 cf, Depth= 2.52" 0.44 cfs @ 12.02 hrs, Volume= Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 1-Year Rainfall=2.86"

	79 50-75% Grass cover, Fair, HSG C				Area	y Description	iin) (feet) (ft/ft) (ft/sec) (cfs)	Sheet Flow, A-B
	ass cover		verage	ons Alec	ervious /	Capacit	(cfs	
Area (sf) CN Description	0-75% Gra	Parking Lot	Weighted Average	V 10 10 10 10 10 10 10 10 10 10 10 10 10	92.36% Impervious Area	Velocity	(t/sec)	1.45
CN	2 6/	98 F	97 V	•	တ	Slope	(ft/ft)	92 0.0218
rea (sf)	457	5,522	5,979	5	5,522	Length	(feet)	92
Ā		*				L C	(min)	1.

Summary for Subcatchment 1C: Watershed 1C

Smooth surfaces n= 0.011 P2= 3.45"

503 cf, Depth= 2.12" 0.19 dfs @ 12.01 hrs, Volume= Runoff Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 1-Year Rainfall=2.86"

CN Description	79 50-75% Grass cover, Fair, HSG C	Parking Lot	Weighted Average	25.62% Pervious Area	74.38% Impervious Area
S	79	98	93		
Area (st)	730	2,119	2,849	730	2.119
		*			

Type III 24-hr 1-Year Rainfall=2.86"

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Sheet Flow, A-B Smooth surfaces n= 0.011 P2= 3.45" Description Capacity (cfs) Velocity (ft/sec) Slope (ft/ft) 0.0277 Length (feet) 8 (min) 0.9

Summary for Subcatchment 2: Ex. Roof Area & Planter Watershed 2

2,254 cf, Depth= 2.52" 0.80 cfs @ 12.01 hrs, Volume= П Runoff

hrs Runoff by SCS TR-20 method, UH-SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 Type III 24-hr 1-Year Rainfall=2.86"

Direct Entry, Capacity Description (cfs) 93.69% Impervious Area Weighted Average 6.31% Pervious Area Slope Velocity (ft/ft) (ft/sec) CN Description Planter Roof 98 79 97 Area (sf) 10,056 677 Tc Length (feet) 10,733 677 10,056 (min) 1.0

Summary for Subcatchment 3: Watershed 3

4,691 cf, Depth= 2.52" 1.64 cfs @ 12.02 hrs, Volume= Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 1-Year Rainfall=2.86"

Sheet Flow, A-B Smooth surfaces n= 0.011 P2= 3.45" Shallow Concentrated Flow, B->C Paved Kv= 20.3 fps Capacity Description (cfs) 50-75% Grass cover, Fair, HSG C Parking Lot & Buildings Weighted Average 4.04% Pervious Area 95.96% Impervious Area Description Velocity 1.24 (ft/sec) Slope (ft/ft) 0.0318 0.0141 S 29 79 97 97 Length 66 22 Area (sf) 902 21,441 22,343 902 21,441 (feet) (min) <u>ს</u> 0.1

Total 121 4.

Existing Condition

Type III 24-hr 1-Year Rainfall=2.86"

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Summary for Reach DP: DP

44,156 sf, 93.74% Impervious, Inflow Depth = 2.50" for 1-Year event 2.47 ds @ 12.02 hrs, Volume= 9,197 cf 2.47 ds @ 12.02 hrs, Volume= 9,197 cf, Atten=0%, Lag=0.0 min nflow Area = II Outflow

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs

Summary for Pond 1P: Ex. Stormwater Planter

10,733 sf, 93.69% Impervious, Inflow Depth = 2.52" for 1-Year event 80 cfs @ 12.01 hrs, Volume= 2,224 cf, Atten=75%, Lag=18.7 min 20 cfs @ 12.33 hrs, Volume= 2,254 cf, Atten=75%, Lag=18.7 min 20 cfs @ 12.33 hrs, Volume= 0.80 cfs @ 12.01 hrs, Volume= 0.20 cfs @ 12.33 hrs, Volume= 0.20 cfs @ 12.33 hrs, Volume= nflow Area = II II Inflow Outflow Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 27.77' @ 12.33 hrs Surf.Area= 677 sf Storage= 861 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 209.2 min (973.5 - 764.3)

	ow (Recalc)	
	1,016 cf Custom Stage Data (Prismatic)Listed below (Recalc)	ore
Avail.Storage Storage Description	Sustom Stage Dat	tore Cum.Store eet) (cubic-feet)
I.Storage S	1,016 cf C	Inc.Store (cubic-feet)
Avai		Surf.Area (sq-ft)
Invert	26.50'	0,
Volume	#	Elevation (feet)

				= 64.0' CPP, projecting, no headwall, Ke= 0.900	nlet / Outlet Invert= 23.50' / 21.33' S= 0.0339 '/ Cc= 0.900	n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf	6.0" Horiz. Orifice/Grate X 10.00 C= 0.600	spe	Surface area
0	1,016		ulvert	projecting, no	ert= 23.50' / 2	gated PE, sm	ice/Grate X 1	low at low hea	Itration over
0	1,016	Invert Outlet Devices	23.50' 12.0" Round Culvert	L= 64.0' CPP,	Inlet / Outlet Inv	n= 0.013 Corru	6.0" Horiz. Orif	Limited to weir flow at low heads	2.000 in/hr Exfiltration over Surface area
677	229	Invert	23.50				27.75		26.50′
50	00	Device Routing	Primary	•			Device 1		#3 Device 1
26.50	28.00	Device	#				4		¥

Primary OutFlow Max=0.20 cfs @ 12.33 hrs HW=27.77′ TW=22.47′ (Dynamic Tailwater)
—1=culvert (Passes 0.20 cfs of 5.80 cfs potential flow)
—2=Orifice/Grate (Weir Controls 0.17 cfs @ 0.48 fps)
—3=Exilitration (Exilitration Controls 0.33 cfs)

Summary for Pond 2P: Ex. Drainage Manhole

16,712 sf, 93.21% Impervious, Inflow Depth = 2.52" for 1-Year event 0.47 ds @ 12.02 hrs, Volume= 3,509 cf 0.47 ds @ 12.02 hrs, Volume= 3,509 cf, Atten= 0%, Lag= 0.0 min 0.47 ds @ 1.02 hrs, Volume= 3,509 cf, Atten= 0%, Lag= 0.0 min	rvious, Inflow Depth = 2.52" for 1-Year event	lume= 3,509 cf	lume= 3,509 cf, Atten= 0%, Lag= 0.0 min	1 2 500 of
	3,712 sf, 93.21% Impe	cfs @ 12.02 hrs, Vo	cfs @ 12.02 hrs, Vo	ofe @ 1202 hrs Vo

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs

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Peak Elev= 22.55' @ 12.02 hrs Flood Elev= 26.50'

Device #1	Device Routing #1 Primary	22.16	Invert Outlet Devices 22.16' 12.0" Round 12" PVC L= 101.5' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 22.16' / 20.74' S= 0.0140' / Cc= 0.900
			THE U.C. I OVER STRUCTURE INTERPRETATION OF THE U.C. OF STRUCTURE INTERPRETATION OF TH

Primary OutFlow Max=0.47 dts @ 12.02 hrs HW=22.55' TW=21.27' (Dynamic Tailwater) -1=12" PVG (Inlet Controls 0.47 cfs @ 1.67 fps)

Summary for Pond 3P: Ex. Drain Inlet

Inflow Depth = 2.48" for 1-Year event	4,506 cf	0.84 cfs @ 12.01 hrs, Volume= 4,506 cf, Atten= 0%, Lag= 0.0 min	4.506 cf
21,813 sf, 91.45% Impervious,	0.84 cfs @ 12.01 hrs, Volume=	0.84 cfs @ 12.01 hrs, Volume=	0.84 cfs @ 12.01 hrs. Volume=
Inflow Area =		Outflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 21.27' @ 12.01 hrs Flood Elev= 23.90'

Invert Outlet Devices	20.74' 12.0" Round 12" PVC	L= 14.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 20.74' / 20.45' S= 0.0207' / Cc= 0.900	n= 0.010 PVC smooth interior Flow Area = 0.79 ef
Invert	20.74			
Device Routing	#1 Primary			
Device	#1			

WQv = 0.43 cfs 25-Year = 3.65 CFS Summary for Pond 4P: Ex. Hydrodynamic Separator

Inflow D	4,506 cf	4,506 cf, Atten= 0%, Lag= 0.0 min	4,506 cf
21,813 sf, 91.45% Impervious, I	0.84 cfs @ 12.01 hrs, Volume=	0.84 cfs @ 12.01 hrs, Volume=	0.84 cfs @ 12.01 hrs, Volume=
Inflow Area =	= lutlow =	Ontflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 20.98' @ 12.02 hrs Flood Elev= 24.12'

Outlet Devices Invert 20.45 Routing Primary Device #1

15.0" Round Ex. 15" RCPL= 54.0' CPP, projecting, no headwall, Ke= 0.900
Inlet / Outlet Invert= 20.45' / 20.12' S= 0.0061'/ Cc= 0.900
n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf

Type III 24-hr 1-Year Rainfall=2.86"

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Summary for Pond 5P: Ex. Manhole

: 21,813 sf, 91.45% Impervious, Inflow Depth = 2.48" for 1-Year event	4,506 cf	4,506 cf, Atten= 0%, Lag= 0.0 min	4,506 cf
21,813 sf, 91.45% Impervious, Ir	0.84 cfs @ 12.01 hrs, Volume=	0.84 cfs @ 12.01 hrs, Volume=	0.84 cfs @ 12.01 hrs, Volume=
Inflow Area =	II	Outflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 20.61' @ 12.02 hrs Flood Elev= 24.12'

Invert Outlet Devices	20.02' 15.0" Round Ex. 15" HDPE	L= 8.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 20.02' / 19.97' S= 0.0063 '/ Cc= 0.900	n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf
Invert	20.02			
Routing	Primary			
Device Routing	#			

Summary for Pond 6P: Ex. Catch Basin

21,813 sf, 91.45% Impervious, Inflow Depth = 2.48" for 1-Year event	ਹ	cf, Atten= 0%, Lag= 0.0 min	cf
Inflow Depth =		4,506 cf, A	
, 91.45% Impervious,	12.01 hrs, Volume=	0.84 dfs @ 12.01 hrs, Volume=	12.01 hrs, Volume=
21,813 sf	0.84 cfs @	0.84 cfs @	0.84 cfs @
ea =	II	II	II
Inflow Area	Inflow	Outflow	Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 20.46' @ 12.01 hrs Flood Elev= 24.12'

Invert Outlet Devices	19.97' 15.0" Round Ex. 15" HDPE	L= 4.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 19.97' / 19.59' S= 0.0950 '/' Cc= 0.900	n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf
Invert	19.97			
Device Routing	#1 Primary			
Device	¥			

Summary for Pond 7P: Ex. Manhole

21,813 sf, 91.45% Impervious, Inflow Depth = 2.48" for 1-Year event	4,506 cf	4,506 cf, Atten= 0%, Lag= 0.0 min	4,506 cf
21,813 sf, 91.45% Impervious, Infl	0.84 cfs @ 12.01 hrs, Volume=	0.84 cfs @ 12.01 hrs, Volume=	0.84 cfs @ 12.01 hrs, Volume=
Inflow Area =	= luflow =	Ontflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 19.01° @ 12.01 hrs Flood Elev= 24.12°

Type III 24-hr 1-Year Rainfall=2.86"

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Invert Outlet Devices	18.59' 24.0" Round Ex. 24" PVC L= 42.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 18.59 / 18.23' S= 0.0086 '/ Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 3.14 sf
Invert	18.59'
Device Routing	Primary
Device	#

Summary for Pond 8P: Ex. Manhole

for 1-Year event		4,506 cf, Atten= 0%, Lag= 0.0 min	
2.48"		, Atte	
Inflow Depth = 2.48"	4,506 cf	4,506 cf	4,506 cf
npervious,	Volume=	Volume=	Volume=
21,813 sf, 91.45% Impervious, I	12.01 hrs,	12.01 hrs,	12.01 hrs,
21,813 sf,	0.84 cfs @	0.84 cfs @ 12.01 hrs, Volume=	0.84 cfs @
	II	II	II
Inflow Area	Inflow	Outflow	Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 18.33' @ 12.01 hrs Flood Elev= 24.12'

Invert Outlet Devices	17.78' 12.0" Round Ex. 12" RCP	L= 87.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 17.78' / 17.44' S= 0.0039 '/ Cc= 0.900	n= 0.011 Concrete nine straight & clean Flow Area= 0.79 sf
Invert	17.78'			
Device Routing	#1 Primary			
Device	#1			

Summary for Pond 9P: Ex. Catch Basin

Inflow Depth = 2.52" for 1-Year event	4,691 cf	4,691 cf, Atten= 0%, Lag= 0.0 min	.64 cfs @ 12.02 hrs, Volume= 4,691 cf
22,343 sf, 95.96% Impervious,	1.64 cfs @ 12.02 hrs, Volume=	1.64 cfs @ 12.02 hrs, Volume=	1.64 cfs @ 12.02 hrs, Volume=
Inflow Area =	= luflow =	Outflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 19.58' @ 12.02 hrs Flood Elev= 24.12'

Invert Outlet Devices	18.77' 12.0" Round Ex. 12" RCP	L= 10.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 18.77' / 18.58' S= 0.0190 '/ Cc= 0.900	n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf
Invert	18.77			
Device Routing	#1 Primary	•		
Device	#1			

Type III 24-hr 1-Year Rainfall=2.86"

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Inflow Depth = 2.52" for 1-Year event	4,691 cf	4,691 cf, Atten= 0%, Lag= 0.0 min	4,691 cf
22,343 sf, 95.96% Impervious, Inflow Depth =	12.02 hrs, Volume=	1.64 cfs @ 12.02 hrs, Volume=	12.02 hrs, Volume=
22,343 sf,	1.64 cfs @	1.64 cfs @	1.64 cfs @
Inflow Area =	= luflow =	Outflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= $18.89' \ @ 12.02$ hrs Flood Elev= 24.12'

invert Outlet Devices	18.08' 12.0" Round Ex. 12" RCP	L= 17.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 18.08 / 17.54 S= 0.0318 // Cc= 0.900	n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf
Invert	18.08′			
Device Routing	Primary			
Device	#			

Primary OutFlow Max=1.64 cfs @ 12.02 hrs HW=18.89' TW=0.00' (Dynamic Tailwater) -1=Ex.12" RCP (Inlet Controls 1.64 cfs @ 2.41 fps)

Summary for Pond 11P: Existing Drain Inlet

Inflow Depth = 2.52" for 1-Year event	1,255 cf	1,255 cf, Atten= 0%, Lag= 0.0 min	1.255 cf
5,979 sf, 92.36% Impervious, Int	0.44 cfs @ 12.02 hrs, Volume=	0.44 cfs @ 12.02 hrs, Volume=	0.44 cfs @ 12.02 hrs. Volume=
Inflow Area =	= moljul	Ontflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 23.47' @ 12.02 hrs Flood Elev= 24.90'

Invert Outlet Devices	23.09' 12.0" Round 12" HDPE	L= 65.3' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 23.09' / 22.26' S= 0.0127 '/ Cc= 0.900	n= 0.013 Corrugated PE. smooth interior. Flow Area= 0.79 sf
Invert	23.09′			
Device Routing	#1 Primary			
Device	#			

Primary OutFlow Max=0.44 cfs @ 12.02 hrs HW=23.46' TW=22.55' (Dynamic Tailwater) -1=12" HDPE (Inlet Controls 0.44 cfs @ 1.64 fps)

Summary for Pond 12P: Ex. Drain Inlet

2,252 sf,100.00% Impervious, Inflow Depth = 2.63" for 1-Year event	493 cf	493 cf, Atten= 0%, Lag= 0.0 min	493 cf
2,252 sf,100.00% Impervious,	0.17 cfs @ 12.01 hrs, Volume=	0.17 cfs @ 12.01 hrs, Volume=	0.17 cfs @ 12.01 hrs, Volume=
Inflow Area =	= molJul	Ontflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 21.49' @ 12.02 hrs Flood Elev= 23.50'

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Invert Outlet Devices	21.25' 12.0" Round 12" PVC	L= 45.0' CPP, projecting, no headwall, Ke= 0.900	nlet / Outlet Invert= 21.25' / 20.79' S= 0.0102 '/ Cc= 0.900	n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf
Outlet	12.0"	L= 45.	Inlet /	n = 0.0
Invert	21.25'			
Device Routing	#1 Primary			
Device	#1			

Primary OutFlow Max=0.17 ofs @ 12.01 hrs HW=21.49′ TW=21.27′ (Dynamic Tailwater) 1.12″ PVC (Outlet Controls 0.17 ofs @ 1.76 fps)

Type III 24-hr 10-Year Rainfall=5.11"

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Summary for Subcatchment 1A: Watershed 1A

914 cf, Depth= 4.87" 0.31 cfs @ 12.01 hrs, Volume= II Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.11"

				P2= 3.45"
				n= 0.011
	nilding	геа	Tc Length Slope Velocity Capacity Description in) (feet) (ft/ft) (ft/sec) (cfs)	Sheet Flow, A-B Smooth surfaces n= 0.011 P2= 3.45"
	2,252 98 Parking Lot & part of building	100.00% Impervious Area	Capacity (cfs)	
Area (sf) CN Description	arking Lot	00.00% Im	Velocity (ft/sec)	1.68
CN	98 P	1	Slope (ft/ft)	85 0.0325
ea (sf)	2,252	2,252	Length (feet)	82
Ā	*		Tc (min)	0.8

Summary for Subcatchment 1B: Watershed 1B

2,370 cf, Depth= 4.76" 0.81 cfs @ 12.02 hrs, Volume= II Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.11"

	ription	50-75% Grass cover, Fair, HSG C
	Description	50-75% Grass cove
	CN	42
	Area (sf)	457
;		

						P2= 3.45"
						n= 0.011
	457 79 50-75% Grass cover, Fair, HSG C			a	To Length Slope Velocity Capacity Description iii) (feet) (ft/ft) (ft/sec) (cfs)	Sheet Flow, A-B Smooth surfaces n= 0.011 P2= 3.45"
	ss cover, F		/erage	92.36% Impervious Area	Capacity (cfs)	
(::)	J-75% Gra	98 Parking Lot	Weighted Average	2.36% Imp	Velocity (ft/sec)	1.45
	79 50	98 P	M 76	6	Slope (ft/ft)	92 0.0218
(10)	457	5,522	5,979 457	5,522	Length (feet)	92
		*			Tc (min)	1.1

Summary for Subcatchment 1C: Watershed 1C

1,022 cf, Depth= 4.31" 0.37 cfs @ 12.01 hrs, Volume= Runoff Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.11"

CN Description	79 50-75% Grass cover, Fair, HSG C	Parking Lot	Weighted Average	25.62% Pervious Area	74.38% Impervious Area
2	79	98	93		
Area (st)	730	2,119	2,849	730	2.119
	1				

Type III 24-hr 10-Year Rainfall=5.11"

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Sheet Flow, A-B Smooth surfaces n= 0.011 P2= 3.45" Description Capacity (cfs) Velocity (ft/sec) Slope (ft/ft) 0.0277 Length (feet) 8 Tc (min) 0.9

Summary for Subcatchment 2: Ex. Roof Area & Planter Watershed 2

4,254 cf, Depth= 4.76" 1.46 cfs @ 12.01 hrs, Volume= П Runoff

hrs Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 Type III 24-hr 10-Year Rainfall=5.11"

Direct Entry, Capacity Description (cfs) 93.69% Impervious Area Weighted Average 6.31% Pervious Area CN Description Slope Velocity (ft/ft) (ft/sec) Planter Roof 98 79 97 Tc Length (feet) 10,056 677 10,733 677 10,056 Area (sf) (min) 1.0

Summary for Subcatchment 3: Watershed 3

8,857 cf, Depth= 4.76" 3.00 cfs @ 12.02 hrs, Volume= Runoff Runoff by SCS TR-20 method, UH-SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.11"

Sheet Flow, A-B Smooth surfaces n= 0.011 P2= 3.45" Shallow Concentrated Flow, B->C Paved Kv= 20.3 fps Capacity Description (cfs) 50-75% Grass cover, Fair, HSG C Parking Lot & Buildings Weighted Average 4.04% Pervious Area 95.96% Impervious Area Description Velocity 1.24 (ft/sec) Slope (ft/ft) 0.0318 0.0141 S 29 79 97 97 Length 66 22 (feet) 22,343 902 21,441 Area (sf) 902 21,441 (min) 1.3 0.1

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4.

Existing Condition

Type III 24-hr 10-Year Rainfall=5.11"

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Summary for Reach DP: DP

17,418 cf, Atten= 0%, Lag= 0.0 min 4.73" for 10-Year event 44,156 sf, 93.74% Impervious, Inflow Depth = 4 5.91 ds @ 12.02 hrs, Volume= 17,418 cf, 5.91 ds @ 12.02 hrs, Volume= 17,418 cf, Inflow = Outflow = nflow Area =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs

Summary for Pond 1P: Ex. Stormwater Planter

4,254 cf 4,255 cf, Atten= 2%, Lag= 0.5 min 4,255 cf 10,733 sf, 93.69% Impervious, Inflow Depth = 4.76" for 10-Year event 1.46 ds @ 12.01 hrs, Volume= 1.43 ds @ 12.02 hrs, Volume= 1.43 ds @ 12.02 hrs, Volume= nflow Area = II Ш Inflow Outflow Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 27.84' @ 12.02 hrs Surf.Area= 677 sf Storage= 908 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 150.0 min (900.7 - 750.7)

Volume Invert Avail.Storage Storage Description #1 26.50' 1,016 cf Custom Stage Data (Prismatic)Listed below (Recalc) Elevation Surf.Area Inc. Store Cum.Store (feet) (sq-ft) (cubic-feet) 0 26.50 677 0 0 28.00 677 1,016 1,016						
Invert		rismatic)Listed below (Recalc)				
Invert	e Description	m Stage Data (P	Cum.Store	(cubic-feet)	0	1,016
26.50' 26.50' on Surf.A et) (sc	Storag	Custo	Store.	c-feet)	0	1,016
26.50' 26.50' on Surf.A et) (sc	I.Storage	1,016 cf	ln	(cubi		
26.5 26.5 30 50	Avai		rf.Area	(sd-ft)	229	219
Volume #1 Elevation (feet) 26.50 28.00	Invert	26.50'	Su			
	Volume	#	Elevation	(feet)	26.50	28.00

Invert Outlet Devices	23.50' 12.0" Round Culvert	L= 64.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 23.50 / 21.33' S= 0.0339 '/ Cc= 0.900	n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf	_	Limited to weir flow at low heads	26.50' 2.000 in/hr Exfiltration over Surface area
Invert	23.50				27.75		26.50
Device Routing	#1 Primary				#2 Device 1		#3 Device 1
Device	#				¥		#3

Primary OutFlow Max=1.43 cfs @ 12.02 hrs HW=27.84" TW=23.22" (Dynamic Tailwater)
—_culvert (Passes 1.43 dfs of 5.85 dfs potential flow)
—_2=Orifice/Grate (Weir Controls 1.40 dfs @ 0.98 fps)
—_3=Exiltration (Exiltration Controls 0.03 dfs)

Summary for Pond 2P: Ex. Drainage Manhole

16,712 sf, 93.21% Impervious, Inflow Depth = 4.76" for 10-Year event 2.24 ds @ 12.02 hrs, Volume= 6,625 cf 6.224 ds @ 12.02 hrs, Volume= 6,625 cf Atten= 0%, Lag= 0.0 min 2.24 ds @ 12.02 hrs, Volume= 6,625 cf Inflow Area = II П II Outflow Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs

Type III 24-hr 10-Year Rainfall=5.11"

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Peak Elev= 23.22' @ 12.02 hrs Flood Elev= 26.50'

12.0" Round **12"** PVC L= 101.5 CPP; projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 22.16', 20.74' S= 0.0140', Cc= 0.900 Inlet / Outlet Smooth interior, Flow Area= 0.79 sf Outlet Devices Invert 22.16' Routing Primary Device #1

Primary OutFlow Max=2.24 cfs @ 12.02 hrs HW=23.22' TW=22.59' (Dynamic Tailwater) —1=12" PVC (Inlet Controls 2.24 cfs @ 2.85 fps)

Summary for Pond 3P: Ex. Drain Inlet

21,813 sf, 91,45% Impervious, Inflow Depth = 4.71" for 10-Year event 2.91 ds @ 12.02 hrs, Volume= 8,562 df, Atten= 0%, Lag= 0.0 min 2.91 ds @ 12.02 hrs, Volume= 8,562 df, Atten= 0%, Lag= 0.0 min 2.91 ds @ 12.02 hrs, Volume= Inflow Area = Inflow = = П Outflow Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 22.60' @ 12.03 hrs Flood Elev= 23.90'

Invert Outlet Devices	20.74' 12.0" Round 12" PVC	L= 14.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 20.74 / 20.45' S= 0.0207 '/ Cc= 0.900	n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf
Invert	20.74			
Device Routing	#1 Primary			
Device	#1			

WQv = 0.43 cfs 25-Year = 3.65 CFS Summary for Pond 4P: Ex. Hydrodynamic Separator

s, Inflow Depth = 4.71" for 10-Year event	= 8,562 cf	2.91 cfs @ 12.02 hrs, Volume= 8,562 cf, Atten= 0%, Lag= 0.0 min	= 8.562 cf
21,813 sf, 91.45% Impervious	2.91 cfs @ 12.02 hrs, Volume=	2.91 cfs @ 12.02 hrs, Volume=	2 91 cfs @ 12 02 hrs Volume=
Inflow Area =	= luflow =	Outflow =	Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 21.73 @ 12.03 hrs Flood Elev= 24.12'

15.0" Round Ex. 15" RCPL= 54.0' CPP, projecting, no headwall, Ke= 0.900
Inlet / Outlet Invert= 20.45' / 20.12' S= 0.0061'/ Cc= 0.900
n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf Outlet Devices Invert 20.45 Routing Primary Device #1

Existing Condition

Type III 24-hr 10-Year Rainfall=5.11"

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Summary for Pond 5P: Ex. Manhole

Inflow Depth = 4.71" for 10-Year event	8,562 cf	8,562 cf, Atten= 0%, Lag= 0.0 min	
21,813 sf, 91.45% Impervious,	2.91 cfs @ 12.02 hrs, Volume=	2.91 cfs @ 12.02 hrs, Volume=	2.91 cfs @ 12.02 hrs, Volume=
Inflow Area =	= luflow =	Outflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 21.37 @ 12.02 hrs Flood Elev= 24.12

Invert Outlet Devices 20.02 Device Routing Primary

¥

Summary for Pond 6P: Ex. Catch Basin

th = 4.71" for 10-Year event	362 cf	2.91 cfs @ 12.02 hrs, Volume= 8,562 cf, Atten= 0%, Lag= 0.0 min	562 cf
Inflow Depi	8,8	8,6	8.8
91.45% Impervious,	2.02 hrs, Volume=	2.02 hrs, Volume=	2.02 hrs. Volume=
21,813 sf,	2.91 cfs @ 1	2.91 cfs @ 1	2.91 cfs @ 1
ea =	II	II	II
Inflow Are	Inflow	Outflow =	Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 20.99' @ 12.02 hrs Flood Elev= 24.12'

Invert Outlet Devices	19.97' 15.0" Round Ex. 15" HDPE	L= 4.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 19.97' / 19.59' S= 0.0950 '/ Cc= 0.900	n= 0.013 Corrugated PE. smooth interior. Flow Area= 1.23 sf
Inve	19.6			
Device Routing	#1 Primary			
Device	¥			

Primary OutFlow Max=2.30 cfs @ 12.02 hrs HW=20.99' TW=19.53' (Dynamic Tailwater) -1=Ex.15" HDPE (Inlet Controls 2.90 cfs @ 2.71 fps)

Summary for Pond 7P: Ex. Manhole

Inflow Depth = 4.71" for 10-Year event	2.91 cfs @ 12.02 hrs, Volume= 8,562 cf	8,562 cf, Atten= 0%, Lag= 0.0 min	8,562 cf
.45% Impervious,	02 hrs, Volume=	.02 hrs, Volume=	.02 hrs, Volume=
21,813 sf, 91	2.91 cfs @ 12.	2.91 cfs @ 12.	2.91 cfs @ 12.
Inflow Area =	= luflow =	Outflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 19.55' @ 12.03 hrs Flood Elev= 24.12'

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Device	Device Routing	Invert	Invert Outlet Devices
#1		18.59'	18.59' 24.0" Round Ex. 24" PVC
			L= 42.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 18.59 / 18.23 S= 0.0086 // Cc= 0.900
			n= 0.010 PVC, smooth interior. Flow Area= 3.14 sf

Summary for Pond 8P: Ex. Manhole

21,813 sf, 91.45% Impervious, Inflow Depth = 4.71" for 10-Year event		8,562 cf, Atten= 0%, Lag= 0.0 min	
4.71"		, Atte	
Inflow Depth = ,	8,562 cf	8,562 cf	8.562 cf
npervious,	Volume=	Volume=	Volume=
91.45% In	12.02 hrs,	12.02 hrs,	12.02 hrs.
21,813 sf,	2.91 cfs @	2.91 cfs @	2.91 cfs @
:a =	II	II	II
Inflow Area =	Inflow	Outflow	Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 19.26' @ 12.02 hrs Flood Elev= 24.12'

Routing Device

lliveit Outliet Devices	17.78' 12.0" Round Ex. 12" RCP	L= 87.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 17.78' / 17.44' S= 0.0039 '/ Cc= 0.900	n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf
IIIVEI	17.78			
Device Rouling	Primary			
200	#1			

Primary OutFlow Max=2.90 cfs @ 12.02 hrs HW=19.26' TW=0.00' (Dynamic Tailwater) —1=Ex.12" RCP (Barrel Controls 2.90 cfs @ 3.69 fps)

Summary for Pond 9P: Ex. Catch Basin

		_	
for 10-Year event		3,857 cf, Atten= 0%, Lag= 0.0 min	
4.76"		, Atten	
Inflow Depth = 4.76 "	8,857 cf	w	8,857 cf
npervious,	Volume=	, Volume=	Volume=
22,343 sf, 95.96% Impervious, 1	12.02 hrs,	12.02 hrs,	12.02 hrs,
22,343 sf,	3.00 cfs @	3.00 cfs @ 12.02 hrs, Volume=	3.00 cfs @
ea =	II	II	II
Inflow Area	Inflow	Outflow	Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 20.57 @ 12.03 hrs Flood Elev= 24.12'

Invert Outlet Devices	18.77' 12.0" Round Ex. 12" RCP	L= 10.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 18.77' / 18.58' S= 0.0190'/ Cc= 0.900	n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf
Invert	18.77			
Device Routing	#1 Primary			
Device	#1			

Type III 24-hr 10-Year Rainfall=5.11"

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Existing Condition

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Summary for Pond 10P: Ex. Manhole

= 22,343 sf, 95.96% Impervious, Inflow Depth = 4.76" for 10-Year event	8,857 cf	8,857 cf, Atten= 0%, Lag= 0.0 min	8.857 cf
22,343 sf, 95.96% Impervious,	3.00 cfs @ 12.02 hrs, Volume=	3.00 cfs @ 12.02 hrs, Volume=	3.00 cfs @ 12.02 hrs. Volume=
Area =	= lutlow =	Outflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 19.59' @ 12.02 hrs Flood Elev= 24.12'

¥

12.0" Round Ex. 12" RCP L= 17.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 18.08' / 17.54' S= 0.0318 /' $C \approx 0.900$ n= 0.011 Concrete pipe, straight & dean, Flow Area= 0.79 sf Invert Outlet Devices 18.08′ Device Routing Primary

Summary for Pond 11P: Existing Drain Inlet

Inflow Depth = 4.76" for 10-Year event	5	2,370 cf, Atten= 0%, Lag= 0.0 min	*
Inflow Depth =	2,370 c	2,370 c	2,370 c
5,979 sf, 92.36% Impervious, 1	0.81 cfs @ 12.02 hrs, Volume=	0.81 cfs @ 12.02 hrs, Volume=	0.81 cfs @ 12.02 hrs, Volume=
Inflow Area =	= molJul	Outflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 23.65' @ 12.02 hrs Flood Elev= 24.90'

Invert Outlet Devices	23.09' 12.0" Round 12" HDPE	L= 65.3' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 23.09 / 22.26 S= 0.0127 // Cc= 0.900	n= 0.013 Corrugated PE. smooth interior. Flow Area= 0.79 sf
Inve	23.0			
Device Routing	#1 Primary	•		
Device	#			

Primary OutFlow Max=0.77 cfs @ 12.02 hrs HW=23.64′ TW=23.21′ (Dynamic Tailwater) **1=12″ HDPE** (Outlet Controls 0.77 dfs @ 2.52 fps)

Summary for Pond 12P: Ex. Drain Inlet

2,252 sf,100.00% Impervious, Inflow Depth = 4.87" for 10-Year event	914 cf	914 cf, Atten= 0%, Lag= 0.0 min	914 cf
2,252 sf,100.00% Impervious,	0.31 cfs @ 12.01 hrs, Volume=	0.31 cfs @ 12.01 hrs, Volume=	0.31 cfs @ 12.01 hrs, Volume=
Inflow Area =	= luflow =	Outflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 22.62° @ 12.03 hrs Flood Elev= 23.50°

Type III 24-hr 10-Year Rainfall=5.11" Type Prepared by Hudson Engineering & Consulting HydroCAD® 10.00-14 s/n 02549 © 2015 HydroCAD Software Solutions LLC

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Invert Outlet Devices	21.25' 12.0" Round 12" PVC	L= 45.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 21.25 / 20.79' S= 0.0102 '/ Cc= 0.900	n=0.010 PVC smooth interior Flow Area= 0.79 sf
	21.25			
Device Routing	Primary			
Device	#1			

Type III 24-hr 25-Year Rainfall=6.41"

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Summary for Subcatchment 1A: Watershed 1A

1,158 cf, Depth= 6.17" 0.39 cfs @ 12.01 hrs, Volume= II Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=6.41"

Area (sf) CN Description 2,252 98 Parking Lot & part of building 2,252 100.00% Impervious Area TC Length Slope Velocity Capacity Description	В	Smooth surfaces n= 0.011 P2= 3.45"
ist) CN Description 52 98 Parking Lot & part of b 52 100.00% Impervious A 100.00% Impervious A 100.00% Impervious A	Sheet Flow, A-B	Smooth surface
St	(CTS)	
Sf) CN D S52 98 P S52 1	(TVSeC)	
sf) 552 552 19th	et) (п/п) 85 0.0325	
2,2 2,2 Ler	(Teet)	
¥ C	(min)	

Summary for Subcatchment 1B: Watershed 1B

3,016 cf, Depth= 6.05" 1.02 dfs @ 12.02 hrs, Volume= II Runoff Runoff by SCS TR-20 method, UH-SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=6.41"

									011 P2= 3.45"
	29					iption		Sheet Flow, A-B	Smooth surfaces n= 0.011 P2= 3.45"
	79 50-75% Grass cover, Fair, HSG C		verage	ious Area	92.36% Impervious Area	Capacity Descr	in) (feet) (ft/ft) (ft/sec) (cfs)	Sheet	Smoo
Area (sf) CN Description	50-75% Gra	98 Parking Lot	Weighted Average	7.64% Pervious Area	32.36% Imp	Velocity	(ft/sec)	1.45	
CN	79 5	98 F	97 ا	7	0)	Slope	(ft/ft)	92 0.0218	
rea (st)	457	5,522	5,979	457	5,522	Length	(teet)	92	
V		*				J L	(min)	1.1	

Summary for Subcatchment 1C: Watershed 1C

1,327 cf, Depth= 5.59" 0.47 dfs @ 12.01 hrs, Volume= Runoff Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=6.41"

	298				
CN Description	79 50-75% Grass cover, Fair, HSG C	Parking Lot	Weighted Average	25.62% Pervious Area	74.38% Impervious Area
S	79	86	93		
Area (st)	730	2,119	2,849	730	2,119
		*			

Type III 24-hr 25-Year Rainfall=6.41"

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Sheet Flow, A-B Smooth surfaces n= 0.011 P2= 3.45" Description Capacity (cfs) Velocity (ft/sec) Slope (ft/ft) 0.0277 Length (feet) 8 Tc (min) 0.9

Summary for Subcatchment 2: Ex. Roof Area & Planter Watershed 2

5,414 cf, Depth= 6.05" 1.84 cfs @ 12.01 hrs, Volume= П Runoff Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, d= 0.01 hrs Type III 24-hr 25-Year Rainfall=6.41"

					sa.	Slope Velocity Capacity Description		Direct Futry
			verage	ious Area	93.69% Impervious Area	Capacity	(cts)	
Area (sf) CN Description	oof	lanter	Weighted Average	6.31% Pervious Area	3.69% Imp	Velocity	(t/sec)	
CN	98 Roof	79 Planter	97		o	Slope	(ft/ft)	
rea (sf)	10,056		10,733	229	10,056	Tc Length	(feet)	
A	*	*				ည	(min)	1.0

Summary for Subcatchment 3: Watershed 3

11,271 cf, Depth= 6.05" 3.78 cfs @ 12.02 hrs, Volume= Runoff Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=6.41"

	79 50-75% Grass cover, Fair, HSG C	ngs		ia ia	Area		C Let gai Stope Vehical Capacity Description Capacity Capacit	9	Sheet Flow, A-B	Smooth surfaces n= 0.011 P2= 3.45"	Shallow Concentrated Flow, B->C	Paved Kv= 20.3 fps
	ess cove	& Buildi	verage	ious Are	ervious		Capacity (ofo)	3				
Area (sf) CN Description	0-75% Gra	98 Parking Lot & Buildings	Weighted Average	4.04% Pervious Area	95.96% Impervious Area	. 4:00	velocity (#/coo)	(neer)	1.24		3.62	
CN	2 62	98 P	97 W	4	Õ	Č	olope (#/#/	(IIVII)	99 0.0141		0.0318	
ea (sf)	905	21,441	22,343	902	21,441	44000	rengin (foot)	(leer)	66		22	
Ā		*			•	ŕ	2 (4		1.3		0.1	
		- 1						٠				

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Type III 24-hr 25-Year Rainfall=6.41"

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Summary for Reach DP: DP

 44,156 sf, 93.74% Impervious, Inflow Depth = 6.03" for 25-Year event

 7.45 ds @ 12.02 hrs, Volume=
 22,186 cf

 7.45 ds @ 12.02 hrs, Volume=
 22,186 cf, Atten=0%, Lag=0.0 min

 Inflow = Outflow = Inflow Area =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs

Summary for Pond 1P: Ex. Stormwater Planter

Inflow Area =	ii II	10,733 sf,	93.69% Im	pervious,	10,733 sf, 93.69% Impervious, Inflow Depth = 6.05" for 25-Year event
Inflow	II	1.84 cfs @	12.01 hrs, '	Volume=	5,414 cf
Outflow	II	1.81 cfs @ 12.02 hrs, Volume=	12.02 hrs, \	Volume=	5,414 cf, Atten= 1%, Lag= 0.5 min
Primary	II	1.81 cfs @ 12.02 hrs, Volume=	12.02 hrs, '	Volume=	5,414 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= $27.86' \ @ 12.02$ hrs Surf.Area= 677 sf Storage= 918 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 133.3 min (879.6 - 746.3)

	1,016 of Custom Stage Data (Prismatic)Listed below (Recalc)		
Avail.Storage Storage Description	n Stage Data (Pri	Cum.Store (cubic-feet)	1,016
Storage	Custor	Inc.Store ubic-feet)	1,016
.Storage	1,016 cf	u gho)	
Avail		Surf.Area (sq-ft)	677
Invert	26.50'	Sul	
Volume	#	Elevation (feet)	26.50 28.00

Invert Outlet Devices	23.50' 12.0" Round Culvert	L= 64.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 23.50' / 21.33' S= 0.0339 '/' Cc= 0.900	n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf	6.0" Horiz. Orifice/Grate X 10.00 C= 0.600	Limited to weir flow at low heads	2.000 in/hr Exfiltration over Surface area	
Invert	23.50				27.75		26.50	
Device Routing	#1 Primary				#2 Device 1		#3 Device 1	
Device	#				4		¥	

Primary OutFlow Max=1.80 cfs @ 12.02 hrs HW=27.86' TW=24.40' (Dynamic Tailwater)
—1=Culvert (Passes 1.80 fs of 5.55 dfs potential flow)
—2=Orifice@rate (Weir Controls 1.77 dfs @ 1.06 fps)
—3=Exfiltration (Exfiltration Controls 0.03 dfs)

Summary for Pond 2P: Ex. Drainage Manhole

Inflow Area =	ll l	16,712 sf,	93.21% Impervious	16,712 st, 93.21% Impervious, Inflow Depth = 6.05" for 25-Year event
M S	II	2.02 CIS @	12.02 ms, volume	0,430 CI
Outflow	II	2.82 cfs @	12.02 hrs, Volume=	8,430 ct, Atten= 0%, Lag= 0.0 min
Primary	II	2.82 cfs @	12.02 hrs. Volume=	8.430 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs

Type III 24-hr 25-Year Rainfall=6.41"

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Peak Elev= 24.57' @ 12.03 hrs Flood Elev= 26.50'

Invert Outlet Devices	22.16' 12.0" Round 12" PVC	L= 101.5' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 22.16 / 20.74 S= 0.0140 / Cc= 0.900	n=0.010 PVC smooth interior Flow Area=0.79 ef
Invert	22.16'			
Device Routing	Primary			
Device	#1			

Primary OutFlow Max=2.41 cfs @ 12.02 hrs HW=24.35' TW=23.70' (Dynamic Tailwater) —1=12" PVC (Inlet Controls 2.41 cfs @ 3.06 fps)

Summary for Pond 3P: Ex. Drain Inlet

pervious, Inf Volume= Volume=	0 0
21,813 sf, 91.45% Impervious, Inflow Depth = 6.00" for 25-Year event 3.68 cfs @ 12.02 hrs, Volume= 10,915 cf	3.68 CIS (# 17.02 hrs. volume=
Inflow Area = Inflow Outflow =	בבב

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 23.77' @ 12.03 hrs Flood Elev= 23.90'

Device Kouting invert	Invert Outlet Devices	20.74' 12.0" Round 12" PVC	L= 14.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert = 20.74 / 20.45' S = 0.0207 '/ Cc = 0.900	n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf
Device Routing #1 Primary	Invert	20.74			
Device #1	Routing	Primary			
	Device	#1			

WQv = 0.43 cfs 25-Year = 3.65 CFS Summary for Pond 4P: Ex. Hydrodynamic Separator

Inflow Depth = 6.00" for 25-Year event	10,915 cf	10,915 cf, Atten= 0%, Lag= 0.0 min	10,915 of
91.45% Impervious,	2.02 hrs, Volume=	3.68 cfs @ 12.02 hrs, Volume=	3.68 cfs @ 12.02 hrs, Volume=
Inflow Area =	= lutlow =	Ontflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 22.39' @ 12.03 hrs Flood Elev= 24.12'

15.0" Round Ex. 15" RCPL= 54.0' CPP, projecting, no headwall, Ke= 0.900
Inlet / Outlet Invert= 20.45' / 20.12' S= 0.0061'/ Cc= 0.900
n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf Outlet Devices Invert 20.45 Routing Primary Device #1

Type III 24-hr 25-Year Rainfall=6.41"

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Existing Condition

Type
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Summary for Pond 5P: Ex. Manhole

Inflow Depth = 6.00" for 25-Year event	10,915 cf	10,915 cf, Atten= 0%, Lag= 0.0 min	10,915 cf
		3.68 cfs @ 12.02 hrs, Volume=	
Inflow Area =	= lutlow =	Ontflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 21.82' @ 12.02 hrs Flood Elev= 24.12'

Invert Outlet Devices	20.02' 15.0" Round Ex. 15" HDPE	L= 8.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 20.02 / 19.97 S= 0.0063 // Cc= 0.900	n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf
Invert	20.02			
Device Routing	Primary			
Device	#			

Summary for Pond 6P: Ex. Catch Basin

1 = 6.00" for 25-Year event	15 cf	10,915 cf, Atten= 0%, Lag= 0.0 min	15 cf
Inflow Dept	10,9	10,9	10,9
11.45% Impervious,	3.68 cfs @ 12.02 hrs, Volume= 10,915 cf	2.02 hrs, Volume=	2.02 hrs, Volume=
21,813 St, 3	3.68 cfs @ 1	3.68 cfs @ 1	3.68 cfs @ 1
9a 11	II	II	II
Inflow Area	Inflow	Outflow	Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 21.21' @ 12.02 hrs Flood Elev= 24.12'

Invert Outlet Devices	19.97' 15.0" Round Ex. 15" HDPE	L= 4.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 19.97' / 19.59' S= 0.0950 '/' Cc= 0.900	n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf
Invert	19.97			
Device Routing	#1 Primary			
Device	#			

Summary for Pond 7P: Ex. Manhole

of of	cf, Atten= 0%, Lag= 0.0 min	of
10,915	10,915	10,915
12.02 hrs, Volume=	12.02 hrs, Volume=	12.02 hrs, Volume=
3.68 cfs @	3.68 cfs @	3.68 cfs @
uflow =	Outflow =	rimary =
	11	Inflow = 3.68 ds @ 12.02 hrs, Volume= 10,915 cf Atten= 0%, Lag= 0.0 min 0.015 or Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 19.96' @ 12.03 hrs Flood Elev= 24.12'

Type III 24-hr 25-Year Rainfall=6.41"

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Invert Outlet Devices	18.59' 24.0" Round Ex. 24" PVC	L= 42.0' CPP, projecting, no headwall, Ke= 0.900	nlet / Outlet Invert= 18.59' / 18.23' S= 0.0086 '/ Cc= 0.900	n= 0.010 PVC, smooth interior, Flow Area= 3.14 sf
Invert	18.59'			
Device Routing	Primary			
Device	#1			

Summary for Pond 8P: Ex. Manhole

21,813 sf, 91.45% Impervious, Inflow Depth = 6.00" for 25-Year event		n= 0%, Lag= 0.0 min	
6.00"		, Atte	
Inflow Depth =	10,915 cf	10,915 cf	10.915 of
pervious,	Volume=	Volume=	Volume=
91.45% In	12.02 hrs,	12.02 hrs,	12.02 hrs.
21,813 sf,	3.68 cfs @	3.68 cfs @	3.68 cfs @
a II	II	II	II
Inflow Area =	Inflow	Outflow	Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 19.80' @ 12.02 hrs Flood Elev= 24.12'

Invert Outlet Devices	17.78' 12.0" Round Ex. 12" RCP	L= 87.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 17.78 / 17.44 S= 0.0039 // Cc= 0.900	n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf
Invert	17.78			
Device Routing	#1 Primary			
Device	#1			

Primary OutFlow Max=3.66 cfs @ 12.02 hrs HW=19.79' TW=0.00' (Dynamic Tailwater) —1=Ex.12" RCP (Inlet Controls 3.66 cfs @ 4.66 fps)

Summary for Pond 9P: Ex. Catch Basin

22,343 sf, 95.96% Impervious, Inflow Depth = 6.05" for 25-Year event	11,271 of	11,271 cf, Atten= 0%, Lag= 0.0 min	11 271 cf
95.96% Impervious,	12.02 hrs, Volume=	3.78 cfs @ 12.02 hrs, Volume=	12.02 hrs Volume=
22,343 sf,	3.78 cfs @	3.78 cfs @	3.78 cfs @
rea =	II	II	11
Inflow Area =	Inflow	Outflow	Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 21.74 @ 12.03 hrs Flood Elev= 24.12'

Invert Outlet Devices	18.77' 12.0" Round Ex. 12" RCP	L= 10.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 18.77' / 18.58' S= 0.0190 '/ Cc= 0.900	n=0.011 Concrete pipe, straight & clean, Flow Area=0.79 sf
Invert	18.77			
Device Routing	#1 Primary			
Device	#1			

Type III 24-hr 25-Year Rainfall=6.41"

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Inflow Depth = 6.05" for 25-Year event	11,271 cf	11,271 cf, Atten= 0%, Lag= 0.0 min	11,271 of
22,343 sf, 95.96% Impervious, Inflow Depth = 1	3.78 cfs @ 12.02 hrs, Volume=	3.78 cfs @ 12.02 hrs, Volume=	3.78 cfs @ 12.02 hrs, Volume=
Inflow Area =	= luflow =	Ontflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 20.18 @ 12.02 hrs Flood Elev= 24.12'

Device Routing Primary

¥

12.0" Round Ex. 12" RCP L= 17.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 18.08' / 17.54' S= 0.0318 /' $C \approx 0.900$ n= 0.011 Concrete pipe, straight & dean, Flow Area= 0.79 sf Invert Outlet Devices 18.08'

Primary OutFlow Max=3.78 cfs @ 12.02 hrs HW=20.18' TW=0.00' (Dynamic Tailwater) —1=Ex.12" RCP (Inlet Controls 3.78 cfs @ 4.81 fps)

Summary for Pond 11P: Existing Drain Inlet

Inflow Depth = 6.05" for 25-Year event		3,016 cf, Atten= 0%, Lag= 0.0 min	
nflow D	3,016 cf	3,016 cf, ,	3,016 cf
5,979 sf, 92.36% Impervious, 1	1.02 dfs @ 12.02 hrs, Volume=	1.02 cfs @ 12.02 hrs, Volume=	1.02 cfs @ 12.02 hrs, Volume=
Inflow Area =	= molJul	Outflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 24.66' @ 12.04 hrs Flood Elev= 24.90'

Primary OutFlow Max=0.00 cfs @ 12.02 hrs HW=23.99' TW=24.20' (Dynamic Tailwater) -1=12" HDPE (Controls 0.00 cfs)

Summary for Pond 12P: Ex. Drain Inlet

2,252 sf,100.00% Impervious, Inflow Depth = 6.17" for 25-Year event	1,158 cf	1,158 cf, Atten= 0%, Lag= 0.0 min	1,158 cf
2,252 sf,100.00% Impervious,	0.39 cfs @ 12.01 hrs, Volume=	0.39 cfs @ 12.01 hrs, Volume=	0.39 cfs @ 12.01 hrs, Volume=
Inflow Area =	= lutlow =	Outflow =	Primary =

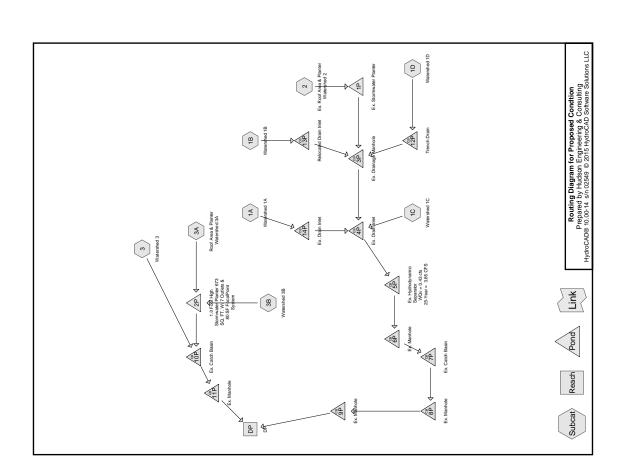
Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 23.78' @ 12.04 hrs Flood Elev= 23.50'

Type III 24-hr 25-Year Rainfall=6.41"

Existing ConditionPrepared by Hudson Engineering & Consulting
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Page 25 Invert Outlet Devices
21.25' 12.0" Round 12" PVC
L = 45.0' CPP, projecting, no headwall, Ke= 0.900
Inlet / Outlet Invert= 21.25' / 20.79' S= 0.0102' / Cc= 0.900
n = 0.010 PVC, smooth interior, Flow Area = 0.79 sf Device Routing #1 Primary

7.) Post-Developed Analysis of the 1-, 10-, and 25- year Extreme Storm Events



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Summary for Subcatchment 1A: Watershed 1A

1,003 cf, Depth= 2.63" 0.35 cfs @ 12.01 hrs, Volume= Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 1-Year Rainfall=2.86"

									P2= 3.45"
									n = 0.011
	33 74 >75% Grass cover, Good, HSG C				ag.	Tc Length Slope Velocity Capacity Description		Sheet Flow, A-B	Smooth surfaces n= 0.011 P2= 3.45"
	s cover, Go	,	verage	ious Area	99.28% Impervious Area	Capacity	(cts)		
Area (sf) CN Description	75% Grass	98 Parking Lot	Weighted Average	0.72% Pervious Area	9.28% Imp	Velocity	(t/sec)	1.66	
CND	74 >	98 P	W 86	0	Ö	Slope	(ft/ft)	79 0.0330	
rea (sf)	33	4,546	4,579	33	4,546	Length	(teet)	79	
Ā		*				ပ	(min)	0.8	

Summary for Subcatchment 1B: Watershed 1B

646 cf, Depth= 2.52" 0.23 dfs @ 12.01 hrs, Volume= Runoff Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 1-Year Rainfall=2.86"

	74 >75% Grass cover, Good, HSG C		erage	ous Area	97.69% Impervious Area	Capacity Description	iin) (feet) (ft/ft) (ft/sec) (cfs)	Sheet Flow, A-B
Area (sf) CN Description	75% Grass	98 Parking Lot	Weighted Average	2.31% Pervious Area	7.69% Imp	Velocity	(ft/sec)	1.37
CN	74 >	98 P	97 W	2	6	Slope	(ft/ft)	64 0.0225
ea (st)	71	3,008	3,079	71	3,008	Length	(feet)	64
An		*				Tc	(min)	0.8

Smooth surfaces n= 0.011 P2= 3.45"

Summary for Subcatchment 1C: Watershed 1C

661 cf, Depth= 2.41" 0.24 dfs @ 12.01 hrs, Volume= Runoff

Runoff by SCS TR-20 method, UH–SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 1-Year Rainfall=2.86"

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HydroCAD® 10.00-14 s/n 02549 © 2015 HydroCAD Software Solutions LLC		74 >75% Grass cover, Good, HSG C			33	Area	Slope Velocity Capacity Description	(cfs)	Sheet Flow, A->B	Smooth surfaces n= 0.011 P2= 3.45"	Shallow Concentrated Flow, B->C	Paved Kv= 20.3 fps		
5 Hydro(s cover,		verage	ious Are	ervious	Capac	ပ						
549 © 201	Area (sf) CN Description	75% Gras	Parking Lot	Weighted Average	7.43% Pervious Area	92.57% Impervious Area	Velocity	(ft/sec)	1.51		2.58			
14 s/n 02	CN	74 >	98 P	W 96	7.	6	Slope	(ft/ft)	57 0.0305		53 0.0162		110 Total	
00 10.00-	ea (sf)	244	3,039	3,283	244	3,039	Tc Length	(feet)	22		23		110	
HydroCAI	Ā		*				T _C	(min)	9.0		0.3		6.0	

Summary for Subcatchment 1D: Watershed 1D

313 cf, Depth= 2.63" 0.11 cfs @ 12.01 hrs, Volume= Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 1-Year Rainfall=2.86"

								В	Smooth surfaces n= 0.011 P2= 3.45"
	74 >75% Grass cover, Good, HSG C			a	Area	ty Description	nin) (feet) (ft/ft) (ft/sec) (cfs)	Sheet Flow, A-B	Smooth surface
ر	ss cover,	ı	Average	1.82% Pervious Area	98.18% Impervious Area	Capaci	(ct		
Area (sf) CN Description	.75% Gra	98 Parking Lot	98 Weighted Average	.82% Per	8.18% Irr	Velocity	(tt/sec)	1.01	
S	74 >	98 F	۸ 86	_	0)	Slope	(ft/ft)	42 0.0129	
rea (sf)	56	1,402	1,428	56	1,402	Length	(feet)	42	
Ā		*				٦ ۲	(min)	0.7	

Summary for Subcatchment 2: Ex. Roof Area & Planter Watershed 2

2,254 cf, Depth= 2.52"
52
Volume=
hrs
12.01 hrs,
(3)
0.80 cfs @
II
Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 1-Year Rainfall=2.86"

CN Description	Roof	Planter	Weighted Average	6.31% Pervious Ārea	03 60% Impervious Area
CN	86	79	97		
Area (st)	10,056	229	10,733	229	10.056
	*	*			

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Type III 24-hr 1-Year Rainfall=2.86"

Description	Direct Entry,
Capacity (cfs)	
Velocity (ft/sec)	
Slope (ft/ft)	
Length (feet)	
Tc (min)	1.0

Summary for Subcatchment 3: Watershed 3

362 cf, Depth= 1.47" 0.14 cfs @ 12.01 hrs, Volume= Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 1-Year Rainfall=2.86"

⋖	۱rea (sf)	CN	Area (sf) CN Description			
	1,655	74	>75% Grass cover, Good, HSG C	over, God	od, HSG C	
*	1,297	98	98 Building/sidewalks	alks		
	2,952	85	Weighted Average	rage		
	1,655		56.06% Pervious Area	us Area		
	1,297	•	43.94% Impervious Area	vious Are	98	
٦ ۲	Tc Length	Slope	Slope Velocity Capacity Description	apacity	Description	
(min)	(feet)	(ft/ft)	(ft/sec)	(cts)		ı
0.5					Direct Entry,	

Summary for Subcatchment 3A: Roof Area & Planter Watershed 3A

3,098 cf, Depth= 2.52" 1.10 cfs @ 12.01 hrs, Volume= Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 1-Year Rainfall=2.86"

* 14,082 98 Roof * 673 79 Planter 14,755 97 Weighted Average 673 4.56% Pervious Area 14,082 95.44% Impervious Area TC Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)
--

Summary for Subcatchment 3B: Watershed 3B

0.25 dfs @ 12.01 hrs, Volume=

703 cf, Depth= 2.52" Runoff Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 1-Year Rainfall=2.86"

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									=-
									P2 = 3.45
									n = 0.011
	74 >75% Grass cover, Good, HSG C				aa	Description	iin) (feet) (ft/ft) (ft/sec) (cfs)	Sheet Flow, A-B	Smooth surfaces n= 0.011 P2= 3.45"
	s cover, Go		verage	ious Area	96.95% Impervious Area	Capacity	(cts)		
Area (sf) CN Description	•75% Gras	Parking Lot	Weighted Average	3.05% Pervious Area	96.95% Imp	Velocity	(ft/sec)	1.29	
CN	74 >	98 F	97 ۷	ניי	0)	Slope	(ft/ft)	74 0.0180	
rea (sf)	102	3,245	3,347	102	3,245	Length	(feet)	74	
Ā		*				<u>۲</u>	(min)	1.0	

Summary for Reach DP: DP

Inflow Depth = 2.46" for 1-Year event	2.34 cfs @ 12.02 hrs, Volume= 9,042 cf	9,042 cf, Atten= 0%, Lag= 0.0 min
44,156 sf, 92.12% Impervious,	2.34 cfs @ 12.02 hrs, Volume=	2.34 cfs @ 12.02 hrs. Volume=
Inflow Area =	= lutlow =	Outflow =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3

Summary for Pond 1P: Ex. Stormwater Planter

Inflow Depth = 2.52" for 1-Year event	-	f, Atten= 74%, Lag= 17.7 min	-
Inflow Depth =	2,254 c	2,254 c	2,254 c
10,733 sf, 93.69% Impervious, II	12.01 hrs, Volume=	0.21 cfs @ 12.31 hrs, Volume=	12.31 hrs, Volume=
10,733 sf,	0.80 cfs @	0.21 cfs @	0.21 cfs @
Inflow Area =	lnflow =	Outflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= $27.77' \otimes 12.31$ hrs Surf.Area= 669 sf Storage= 852 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 208.0 min (972.3 - 764.3)

Avail. Storage Storage Description	1,004 cf Custom Stage Data (Prismatic)Listed below (Recalc)	Inc.Store Cum.Store (cubic-feet) (cubic-feet)		1,004	Invert Outlet Devices	23.50' 12.0" Round Culvert	L= 64.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 23.50' / 22.26' S= 0.0194 '/ Cc= 0.900	n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf	6.0" Horiz. Orifice/Grate X 10.00 C= 0.600	imited to weir flow at low heads	2.000 in/hr Exfiltration over Surface area
torage	004 cf	u lo			t Our	12.		lule	۵		Ë	
	1,	Surf.Area (sq-ft)	699	699	Inver	23.50				27.75		26.50
Invert	26.50'			_	Routing	Primary				Device 1		Device 1
Volume	#1	Elevation (feet)	26.50	28.00	Device Routing	#				#2		#3

Type III 24-hr 1-Year Rainfall=2.86"

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Primary OutFlow Max=0.21 cfs @ 12.31 hrs HW=27.77′ TW=22.46′ (Dynamic Tailwater)

—1=Culvert (Passes 0.21 cfs of 5.80 cfs potential flow)

—2=Orifice/Grate (Weir Controls 0.18 cfs @ 0.50 fps)

—3=Exfiltration (Exfiltration Controls 0.03 cfs)

ummary for Pond 2P: 1.0 Foot High Stormwater Planter 673 SQ. FT. W/ 7 Outlets & 80 SF FocalPoint Sys

18,102 sf, 95.72% Impervious, Inflow Depth = 2.52" for 1-Year event		3,803 cf, Atten= 4%, Lag= 0.9 min	3,803 cf
95.72% Impervious,	1.35 cfs @ 12.01 hrs, Volume=	12.03 hrs, Volume=	12.03 hrs, Volume=
18,102 sf,	1.35 dfs @ 1	1.29 cfs @ 1	1.29 cfs @ `
Inflow Area =	Inflow =	Ontflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 22.17' @ 12.03 hrs Suff.Area= 80 sf Storage= 433 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 7.8 min (772.2 - 764.3)

Avail.Storage Storage Description	4.00'W × 20.00'L × 2.25'H FocalPoint 180 of Overall × 20.0% Voids	Stormwater Planter (Prismatic) Listed below (Recalc) -Impervious	541 of Total Available Storage	Cum.Store	(cubic-feet)	0	337	505	Ces	12.0" Round Culvert	L= 19.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 19.00' / 18.77' S= 0.0121 '/' Cc= 0.900	n= 0.013, Flow Area= 0.79 sf	100.000 in/hr Exfiltration over Surface area	8.0" Horiz. Orifice/Grate X 6.00 C= 0.600 Limited to weir flow at low heads
ge Storaç	36 of 4.00'V 180 of		cf Total,	Inc.Store	(cubic-feet)	0	337	168	Outlet Devices	2.0" Rour	= 19.0' C	i= 0.013, F	00.000 in/	3.0" Horiz. Imited to w
		505 cf	541	Surf.Area	(sq-ft) (c	673	673	673	Invert	19.00′ 1			•	22.08' 8
Invert	19.33	21.58				3	æ	3	Routing	Primary			Device 1	Device 1
Volume	#	#2		Elevation	(feet)	21.58	22.08	22.33	Device Routing	#			#2	¥

Primary OutFlow Max=1.29 cfs @ 12.03 hrs HW=22.17' TW=19.50' (Dynamic Tailwater)

—1=Culvert (Passes 1.29 cfs of 4.88 cfs potential flow)

—2=Exfiltration (Exfiltration Controls 0.19 cfs)

—3=Orifice/Grate (Weir Controls 1.10 cfs @ 0.98 fps)

Summary for Pond 3P: Ex. Drainage Manhole

, Inflow Depth = 2.53" for 1-Year event	3,213 cf	3,213 cf, Atten= 0%, Lag= 0.0 min	3,213 cf
		0.37 cfs @ 12.01 hrs, Volume=	
Inflow Area =	= luflow =	Outflow =	Primary =

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 22.50 @ 12.01 hrs Flood Elev= 26.50

			_	
Invert Outlet Devices	22.16' 12.0" Round 12" PVC	L= 101.5' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 22.16 / 20.74 S= 0.0140 // Cc= 0.900	n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf
Invert	22.16'			
Device Routing	Primary			
Device	#1			

Summary for Pond 4P: Ex. Drain Inlet

23,102 sf, 95.45% Impervious, Inflow Depth = 2.53" for 1-Year event		4,877 cf, Atten= 0%, Lag= 0.0 min	4,877 cf
95.45% Impervious,	12.01 hrs, Volume=	0.96 cfs @ 12.01 hrs, Volume=	12.01 hrs, Volume=
23,102 sf,	0.96 cfs @	0.96 cfs @	0.96 cfs @
Inflow Area =	lnflow =	Outflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 21.45' @ 12.01 hrs Flood Elev= 23.90'

Device Routing Invert	Invert Outlet Devices	20.74' 12.0" Round 12" PVC	L= 14.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 20.74 / 20.45 S= 0.0207 Cc= 0.90	n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf
Device Routing #1 Primary	Invert	20.74			
Device #1	Routing	Primary			
	Device	#1			

00

Primary OutFlow Max=0.95 cfs @ 12.01 hrs HW=21.45' TW=21.27' (Dynamic Tailwater) —1=12" PVC (Inlet Controls 0.95 cfs @ 1.61 fps)

WQv = 0.43 cfs 25-Year = 3.65 CFS Summary for Pond 5P: Ex. Hydrodynamic Separator

23,102 sf, 95.45% Impervious, Inflow Depth = 2.53" for 1-Year event		4,877 cf, Atten= 0%, Lag= 0.0 min	
23,102 sf, 95.45% Impervious,	0.96 cfs @ 12.01 hrs, Volume=	0.96 cfs @ 12.01 hrs, Volume=	0.96 cfs @ 12.01 hrs, Volume=
Inflow Area =	= luflow =	Outflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 21.27' @ 12.01 hrs Flood Elev= 24.12'

Invert Outlet Devices	20.74' 15.0" Round Ex. 15" RCP	L= 52.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 20.74' / 20.12' S= 0.0119'/ Cc= 0.900	n= 0.011 Concrete pipe, straight & clean, Flow Area= 1.23 sf
Invert	20.74			
Device Routing	Primary			
Device	#1			

Type III 24-hr 1-Year Rainfall=2.86"

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Summary for Pond 6P: Ex. Manhole

23,102 sf, 95.45% Impervious, Inflow Depth = 2.53" for 1-Year event	4,877 cf	4,877 cf, Atten= 0%, Lag= 0.0 min	4,877 cf	
23,102 sf, 95.45% Impervious,	0.96 cfs @ 12.01 hrs, Volume=	0.96 cfs @ 12.01 hrs, Volume=	0.96 cfs @ 12.01 hrs, Volume=	
Inflow Area =	= lutlow =	Ontflow =	Primary =	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 20.66 @ 12.01 hrs Flood Elev= 24.12'

Invert Outlet Devices	20.02' 15.0" Round Ex. 15" HDPE	L= 8.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 20.02 / 19.97 S= 0.0063 // Cc= 0.900	n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf
Invert	20.02			
Device Routing	Primary			
Device	#			

Primary OutFlow Max=0.95 cfs @ 12.01 hrs HW=20.66' TW=20.50' (Dynamic Tailwater) $^+$ 1=Ex.15" HDPE (Outlet Controls 0.95 cfs @ 2.21 fps)

Summary for Pond 7P: Ex. Catch Basin

23,102 sf, 95.45% Impervious, Inflow Depth = 2.53" for 1-Year event	4,877 cf	4,877 cf, Atten= 0%, Lag= 0.0 min	
95.45% Impervious,	12.01 hrs, Volume=	12.01 hrs, Volume=	12.01 hrs, Volume=
23,102 sf,	0.96 cfs @ \	0.96 cfs @ 12.01 hrs, V	0.96 cfs @ 1
Inflow Area =	= lutlow =	Ontflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 20.50' @ 12.01 hrs Flood Elev= 24.12'

Invert Outlet Devices	19.97' 15.0" Round Ex. 15" HDPE	L= 4.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 19.97 / 19.59 S= 0.0950 // Cc= 0.900	n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf	
Invert	19.97				
Device Routing	#1 Primary				
Device	#1				

Primary OutFlow Max=0.95 cfs @ 12.01 hrs HW=20.50′ TW=19.04′ (Dynamic Tailwater) **1=Ex.15″ HDPE** (Inlet Controls 0.95 cfs @ 1.95 fps)

Summary for Pond 8P: Ex. Manhole

Inflow Depth = 2.53" for 1-Year event	4,877 cf	4,877 cf, Atten= 0%, Lag= 0.0 min	4,877 cf
23,102 sf, 95.45% Impervious,	12.01 hrs, Volume=	0.96 cfs @ 12.01 hrs, Volume=	12.01 hrs, Volume=
23,102 sf,	0.96 cfs @	0.96 cfs @	0.96 cfs @
Inflow Area =	= ntlow =	Outflow =	Primary =

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 19.04' @ 12.01 hrs Flood Elev= 24.12'

Invert Outlet Devices	18.59' 24.0" Round Ex. 24" PVC	-= 42.0' CPP, projecting, no headwall, Ke= 0.900	nlet / Outlet Invert= 18.59' / 18.23' S= 0.0086 '/ Cc= 0.900	n= 0.010 PVC, smooth interior, Flow Area= 3.14 sf
0	2	ت	_	2
Inver	18.59			
Device Routing	Primary			
Device	#1			

Summary for Pond 9P: Ex. Manhole

Inflow Depth = 2.53" for 1-Year event	4,877 cf	4,877 cf, Atten= 0%, Lag= 0.0 min	
23,102 sf, 95.45% Impervious, Inflow Depth = 2	0.96 cfs @ 12.01 hrs, Volume=	0.96 cfs @ 12.01 hrs, Volume=	0.96 cfs @ 12.01 hrs, Volume=
Inflow Area =	= moljul	Ontflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 18.38 @ 12.01 hrs Flood Elev= 24.12'

Invert Outlet Devices	17.78' 12.0" Round Ex. 12" RCP	L= 87.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 17.78 / 17.44 S= 0.0039 / Cc= 0.900	n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf
Invert	17.78'			
Device Routing	#1 Primary			
Device	#1			

Primary OutFlow Max=0.95 ofs @ 12.01 hrs HW=18.38' TW=0.00' (Dynamic Tailwater) **1=Ex. 12" RCP** (Barrel Controls 0.95 ofs @ 2.79 fps)

Summary for Pond 10P: Ex. Catch Basin

Inflow Depth = 2.37" for 1-Year event	4,165 cf	1.42 cfs @ 12.03 hrs, Volume= 4,165 cf, Atten= 0%, Lag= 0.0 min	4,165 cf
21,054 sf, 88.46% Impervious,	1.42 cfs @ 12.03 hrs, Volume=	1.42 cfs @ 12.03 hrs, Volume=	1.42 cfs @ 12.03 hrs, Volume=
Inflow Area =	= lutlow =	Outflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 19.50' @ 12.03 hrs Flood Elev= 24.12'

Invert Outlet Devices	18.77' 12.0" Round Ex. 12" RCP	L= 10.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 18.77' / 18.58' S= 0.0190'/ Cc= 0.900	n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf
Invert	18.77			
Device Routing	#1 Primary			
Device	#1			

Type III 24-hr 1-Year Rainfall=2.86"

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Summary for Pond 11P: Ex. Manhole

Inflow Area =	21,054 sf, 88.46% Impervious,	Inflow Depth = 2.37" for 1-Year event
Inflow	1.42 cfs @ 12.03 hrs, Volume=	4,165 cf
Outflow =	1.42 cfs @ 12.03 hrs, Volume=	4,165 cf, Atten= 0%, Lag= 0.0 min
Primary =	1.42 cfs @ 12.03 hrs, Volume=	1.42 cfs @ 12.03 hrs, Volume= 4,165 cf
Routing by Dyn-	Bouting by Dyn-Stor-Ind method Time Span= 0.00-60.00 hrs /3	00 brs dt= 0.01 brs / 3

Routing by Dyn-Stor-Ind method, Peak Elev= 18.81' @ 12.03 hrs Flood Elev= 24.12'

Invert Outlet Devices	18.08' 12.0" Round Ex. 12" RCP	L= 17.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 18.08 / 17.54 S= 0.0318 // Cc= 0.900	n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf
Invert	18.08			
Device Routing	Primary			
Device	#			

Primary OutFlow Max=1.41 cfs @ 12.03 hrs HW=18.81' TW=0.00' (Dynamic Tailwater) = 1=Ex.12" RCP (Inlet Controls 1.41 cfs @ 2.30 fps)

Summary for Pond 12P: Trench Drain

nflow Dep	313 cf	313 cf, Atten= 0%, Lag= 0.0 min	313 cf
1,428 sf, 98.18% Impervious, In	0.11 cfs @ 12.01 hrs, Volume=	0.11 cfs @ 12.01 hrs, Volume=	0.11 cfs @ 12.01 hrs, Volume=
Inflow Area =	= luflow =	Outflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, d= 0.01 hrs / 3 Peak Elev= 23.53 @ 12.01 hrs Flood Elev= 25.96'

Invert Outlet Devices	23.35' 12.0 " Round 12" HDPE	L= 31.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 23.35' / 22.26' S= 0.0352 '/ Cc= 0.900	n= 0.013 Corrugated PE. smooth interior. Flow Area= 0.79 sf
Invert	23.35			
Device Routing	#1 Primary			
Device	#			

Summary for Pond 13P: Relocated Drain Inlet

Inflow Depth = 2.52" for 1-Year event		646 cf, Atten= 0%, Lag= 0.0 min	
3,079 sf, 97.69% Impervious, I	0.23 cfs @ 12.01 hrs, Volume=	0.23 dfs @ 12.01 hrs, Volume=	0.23 cfs @ 12.01 hrs, Volume=
Inflow Area =	= luflow =	Outflow =	Primary =

Type III 24-hr 1-Year Rainfall=2.86" Proposed Condtion
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Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 22.74' @ 12.01 hrs Flood Elev= 25.05'

Invert Outlet Devices	22.45' 12.0" Round 12" HDPE	L= 35.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 22.45' / 22.26' S= 0.0054' / Cc= 0.900	n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
Invert	22.45			
Device Routing	Primary			
Device	#1			

Primary OutFlow Max=0.23 cfs @ 12.01 hrs HW=22.74' TW=22.50' (Dynamic Tailwater) —1=12" HDPE (Outlet Controls 0.23 cfs @ 1.84 fps)

Summary for Pond 14P: Ex. Drain Inlet

Inflow Depth = 2.63" for 1-Year event	1,003 cf	1,003 cf, Atten= 0%, Lag= 0.0 min	1,003 cf
4,579 sf, 99.28% Impervious, Inflow Depth = 2.63" for 1-	0.35 cfs @ 12.01 hrs, Volume=	0.35 cfs @ 12.01 hrs, Volume=	0.35 cfs @ 12.01 hrs, Volume=
Inflow Area =	= ntlow =	Outflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 21.61 (@ 12.01 hrs Flood Elev= 23.63'

Invert Outlet Devices	21.25' 1 5.0" Round 12" PVC	L= 45.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 21.25' / 20.79' S= 0.0102 '/ Cc= 0.900	n= 0.010 PVC, smooth interior, Flow Area= 1.23 sf
Invert	21.25'			
Device Routing	Primary			
Device	#1			

Primary OutFlow Max=0.35 cfs @ 12.01 hrs HW=21.61' TW=21.45' (Dynamic Tailwater) —1=12" PVC (Outlet Controls 0.35 cfs @ 1.77 fps)

Type III 24-hr 10-Year Rainfall=5.11"

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Summary for Subcatchment 1A: Watershed 1A

1,859 cf, Depth= 4.87" 0.63 dfs @ 12.01 hrs, Volume= II Runoff Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.11"

						P2= 3.45"
						n= 0.011
	>75% Grass cover, Good, HSG C			39	Slope Velocity Capacity Description (ft/ft) (ft/sec) (cfs)	Sheet Flow, A-B Smooth surfaces n= 0.011 P2= 3.45"
	s cover, Go		verage ious Area	99.28% Impervious Area	Capacity (cfs)	
Area (sf) CN Description	.75% Grass	Parking Lot	Weighted Average 0.72% Pervious Area	9.28% Imp	Velocity (ft/sec)	1.66
CN	< 42	98 F	۸ 86 0	0)	Slope (ft/ft)	79 0.0330
rea (sf)	33	4,546	4,579 33	4,546	Tc Length	79
Ā		*			Tc (min)	0.8

Summary for Subcatchment 1B: Watershed 1B

1,220 cf, Depth= 4.76" 0.42 cfs @ 12.01 hrs, Volume= Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.11"

-							-		
									= 0.011 P2= 3.45"
	74 >75% Grass cover, Good, HSG C				ee	Tc Length Slope Velocity Capacity Description		Sheet Flow, A-B	Smooth surfaces n= 0.011 P2= 3.45"
	s cover, Go		verage	ious Area	97.69% Impervious Area	Capacity	(cts)		
Area (sf) CN Description	.75% Gras	98 Parking Lot	Weighted Average	2.31% Pervious Area	17.69% Imp	Velocity	(ft/sec)	1.37	
CS	74 >	98 F	97 V	0	0)	Slope	(ft/ft)	64 0.0225	
rea (sf)	71	3,008	3,079	71	3,008	Length	(feet)	64	
4		*				٦ ۲	(min)	0.8	

Summary for Subcatchment 1C: Watershed 1C

1,270 cf, Depth= 4.64" 0.44 cfs @ 12.01 hrs, Volume= II Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.11"

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nyarocade 10.00-14 s/ii 02349 € 2013 nyarocad soriware sorinions llo		d, HSG C			or.	Description		Sheet Flow, A->B	Smooth surfaces n= 0.011 P2= 3.45"	Snallow Concentrated Flow, B->C Paved Kv= 20.3 fps	
349 © ∠UI5 ⊓yc	Area (sf) CN Description	74 >75% Grass cover, Good, HSG C	Parking Lot	Weighted Average 7 43% Pervious Area	92.57% Impervious Area	Slope Velocity Capacity Description	(ft/sec)	1.51	C	7.58	
4 5/11 02	CN	74 >	98 P	7 V 96	. თ	Slope	(ft/ft)	57 0.0305	2	53 0.0162	Total
-0.00-	ea (sf)	244	3,039	3,283	3,039		(feet)	22	Ç	53	110 Total
JydroCAD	Are					J.	(min)	9.0	ć	0.3	6.0

Summary for Subcatchment 1D: Watershed 1D

4
Depth=
ç,
580 cf,
22
Volume=
Ś,
Ξ
6
12.01 hrs,
(9)
ş
0.20 cfs
0.2
II
Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.11"

									Smooth surfaces n= 0.011 P2= 3.45"
ood, HSG C				ea		Description	,	Sheet Flow, A-B	Smooth surfaces
s cover, Go		verage	ious Area	ervious Ar		Capacity	(cts)		
75% Grass	arking Lot	Veighted A	.82% Perv	8.18% Imp		Velocity	(t/sec)	1.01	
74 >	98 P	Λ 86	_	6		Slope	(ft/ft)	0.0129	
56	1,402	1,428	56	1,402		Length	(feet)	42	
	*					С	(min)	0.7	
	26 74 >75% Grass cover, Good, HSG C	26 74 >75% Grass cover, Good, HSG C * 1,402 98 Parking Lot	26 74 >75% Grass cover, Good, HSG C * 1,402 98 Parking Lot 1,428 98 Weighted Average	26 74 >75% Grass cover, Good, HSG C 1,402 98 Parking Lot 1,428 98 Weighted Average 26 1.82% Pervious Area	26 74 >75% Grass cover, Good, HSG C 1,402 98 Parking Lot 1,428 98 Weighted Average 26 1.82% Pervious Area 1,402 98.18% Impervious Area	* 1,402 98 Parking Lot 1,428 98 Weighted Average 26 1.82% Pervious Area 1,402 98.18% Impervious Area	26 74 >75% Grass cover, Good, HSG C 1,402 98 Parking Lot 1,428 98 Weighted Average 26 1.82% Pervious Area 1,402 98.18% Impervious Area Tc Length Slope Velocity Capacity Description	26 1,402 1,428 26 1,402 Length (feet)	26 74 >75% Grass cover, Good, HSG C 1,402 98 Parking Lot 1,402 98 Velighted Average 26 1,82% Pervious Area 1,402 98.18% Impervious Area TC Length Slope Velocity Capacity Description (min) (feet) (tf/ft) (f/sec) (ds) 0.7 42 0.0129 1.01 Sheet Flow, A-B

Summary for Subcatchment 2: Ex. Roof Area & Planter Watershed 2

4.76"	
4,254 cf, Depth= 4.76"	
4,254 cf,	
me=	
Volume=	
12.01 hrs,	
1.46 cfs @	
II	
Runoff	

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.11"

Area (sf) CN Description	Roof	Planter	Weighted Average	6.31% Pervious Area	93.69% Impervious Area
S	86	79	6		
Area (sf)	10,056	229	10,733	229	10.056
	*	*			

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Type III 24-hr 10-Year Rainfall=5.11"

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/ Description	Direct Entry,
Capacity (cfs)	
Velocity (ft/sec)	
Slope (ft/ft)	
Length (feet)	
Tc (min)	1.0

Summary for Subcatchment 3: Watershed 3

854 cf, Depth= 3.47" 0.33 cfs @ 12.01 hrs, Volume= Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.11"

f) CN Description	74	7 98 Building/sidewalks	85	5 56.06% Pervious Area	7 43.94% Impervious Area	jth Slope Velocity Capacity Description		Direct Entry,
S	74	86				Slope	(ft/ft	
Area (sf)	1,655	1,297	2,952	1,655	1,297	Tc Length	(min) (feet)	0.5
							ت	

Summary for Subcatchment 3A: Roof Area & Planter Watershed 3A

5,849 cf, Depth= 4.76" 2.01 cfs @ 12.01 hrs, Volume= Runoff Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.11"

						on		ntrv.
					ا ان	Descripti		Direct Entry.
			verage	ons Area	dividus Air	Capacity	(cfs)	
Area (sf) CN Description	Soof	Planter	Weighted Average	7.70 /8 51 /6	90.44 % IIIIpervious Area	Slope Velocity Capacity Description	(ft/sec)	
CN	98 Roof	79 Planter	۸ / کا	, ,	,,	Slope	(ft/ft)	
rea (sf)	14,082	673	14,755	2,00		Tc Length	(feet)	
⋖	*	*				JC	(min)	1.0

Summary for Subcatchment 3B: Watershed 3B

1,327 cf, Depth= 4.76" 0.45 dfs @ 12.01 hrs, Volume=

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.11" Runoff

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								P2= 3.45"
								n = 0.011
	74 >75% Grass cover, Good, HSG C			23	Tc Length Slope Velocity Capacity Description	-	Sheet Flow, A-B	Smooth surfaces n= 0.011 P2= 3.45"
	s cover, Go		verage ious Area	96.95% Impervious Area	Capacity	(cfs)		
Area (sf) CN Description	75% Gras	Parking Lot	Weighted Average 3.05% Pervious Area	6.95% Imp	Velocity	(ft/sec)	1.29	
CN	< 42	98 P	97 V 3	6	Slope	(ft/ft)	74 0.0180	
rea (sf)	102	3,245	3,347	3,245	Lenath	(feet)	74	
A		*			J _C	(min)	1.0	

Summary for Reach DP: DP

s, Inflow Depth = 4.68" for 10-Year event	5.82 cfs @ 12.02 hrs, Volume= 17,214 cf	= 17.214 cf. Atten= 0%. Lag= 0.0 mir
92.12% Impervious	12.02 hrs, Volume=	12 02 hrs Volume=
44,156 sf,	5.82 cfs @	5 82 cfs @
ow Area =	lnflow =	#low =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3

Summary for Pond 1P: Ex. Stormwater Planter

Inflow Depth = 4.76" for 10-Year event	4,254 cf	4,255 cf, Atten= 2%, Lag= 0.5 min	4,255 cf
10,733 sf, 93.69% Impervious, Inflow Depth = 4.76"	1.46 cfs @ 12.01 hrs, Volume=	1.43 cfs @ 12.02 hrs, Volume=	1.43 cfs @ 12.02 hrs, Volume=
Inflow Area =	lnflow =	Outflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 27.84 @ 12.02 hrs Surf.Area= 669 sf Storage= 897 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 149.2 min (899.8 - 750.7)

Invert Avail.Storage Storage Description	1,004 cf Custom Stage Data (Prismatic)Listed below (Recalc)	Inc.Store Cum.Store (aubic-feet) (aubic-feet)	0 0	1,004 1,004	Invert Outlet Devices	23.50' 12.0" Round Culvert	L= 64.0 CPP, projecting, no neadwall, "Re= 0.900 Inlet / Outlet Invert= 23.50 / 22.26	n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf	6.0" Horiz. Orifice/Grate X 10.00 C= 0.600	Limited to weir flow at low heads	2.000 in/hr Exfiltration over Surface area
Avail.Stor	1,00	Surf.Area (sq-ft)	699	699	Invert	23.50'			27.75		26.50'
Invert	26.50'				Routing	Primary			Device 1		Device 1
Volume	#1	Elevation (feet)	26.50	28.00	Device Routing	#			#5		#3

Type III 24-hr 10-Year Rainfall=5.11"

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Primary OutFlow Max=1.43 cfs @ 12.02 hrs HW=27.84 TW=23.43' (Dynamic Tailwater)

—1=Culvert (Passes 1.43 cfs of 5.85 cfs potential flow)

—2=Orifice/Grate (Weir Controls 1.40 cfs @ 0.98 fps)

—3=Exfiltration (Exfiltration Controls 0.03 cfs)

ummary for Pond 2P: 1.0 Foot High Stormwater Planter 673 SQ. FT. W/ 7 Outlets & 80 SF FocalPoint Sy:

nflow Depth = 4.76" for 10-Year event	7,176 cf	7,176 cf, Atten= 2%, Lag= 0.5 min	7,176 cf
18,102 sf, 95.72% Impervious, Inflow Depth = 4	2.46 cfs @ 12.01 hrs, Volume=	2.42 cfs @ 12.02 hrs, Volume=	2.42 cfs @ 12.02 hrs, Volume=
Inflow Area =	Inflow =	Outflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 22.22' @ 12.02 hrs Suff.Area= 80 sf Storage= 469 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= $7.3\,\mathrm{min}$ (757.9 - 750.7)

Avail.Storage Storage Description	4.00'W x 20.00'L x 2.25'H FocalPoint 180 cf Overall x 20.0% Voids	505 cf Stormwater Planter (Prismatic) Listed below (Recalc) -Impervious	541 cf Total Available Storage	Inc. Store Cum. Store	-feet) (cubic-feet)	0 0	337 337	168 505	rt Devices	19.00' 12.0" Round Culvert = 19.0' CPP. projecting no headwall. Ke= 0.900	Inlet / Outlet Invert= 19.00/ / 18.77' S= 0.0121 // Cc= 0.900	ll≡ 0.013, intow Area≡ 0.79 st 100.000 in/hr Exfiltration over Surface area	8.0" Horiz. Orifice/Grate X 6.00 C= 0.600
I.Storage	36 cf	505 cf	541 cf	Inc	(cubic-feet)				Invert Outlet Devices	.00' 12.0 '	Inlet	.0=0. 19.33′ 100. 0	
				Surf.Area	(sd-ft)	673	673	673	ľ	19		19	22
Invert	19.33	21.58							Souting	Primary		Device 1	Device 1
Volume	#	#2		Elevation	(feet)	21.58	22.08	22.33	Device Routing	#1		#	

Primary OutFlow Max=2.41 cfs @ 12.02 hrs HW=22.22′ TW=20.24′ (Dynamic Tailwater)

—1=Culvert (Passes 2.41 cfs of 4.20 cfs potential flow)

—2=Exfiltration (Exfiltration Controls 0.19 cfs)

—3=Orifice/Grate (Weir Controls 2.22 cfs @ 1.24 fps)

Limited to weir flow at low heads

Summary for Pond 3P: Ex. Drainage Manhole

, Inflow Depth = 4.77" for 10-Year event	6,055 cf	6,055 cf, Atten= 0%, Lag= 0.0 min	6,055 cf
15,240 sf, 94.92% Impervious,	2.04 cfs @ 12.02 hrs, Volume=	2.04 cfs @ 12.02 hrs, Volume=	2.04 cfs @ 12.02 hrs, Volume=
Inflow Area =	lnflow =	Outflow =	Primary =

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 23.46 @ 12.02 hrs Flood Elev= 26.50

ing Invert Outlet Devices	ary 22.16' 12.0" Round 12" PVC	L= 101.5' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 22.16 / 20.74 S= 0.0140 // Cc= 0.900	n= 0.010 PVC smooth interior Flow Area= 0.79 sf
Device Routing	#1 Primary			
Device	#1			

1

Summary for Pond 4P: Ex. Drain Inlet

Inflow Area =	Ш	23,102 sf,	, 95.45% Impervious,	Inflow Depth = 4.77" for 10-Year event
Inflow	II	3.10 cfs @	12.02 hrs, Volume=	3.10 cfs @ 12.02 hrs, Volume= 9,184 cf
Outflow	II	3.10 cfs @	3.10 cfs @ 12.02 hrs, Volume=	9,184 cf, Atten= 0%, Lag= 0.0 min
Primary	II	3.10 cfs @	3.10 cfs @ 12.02 hrs, Volume=	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 23.00 @ 12.02 hrs Flood Elev= 23.90'

Invert Outlet Devices	20.74' 12.0" Round 12" PVC	L= 14.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 20.74' / 20.45' S= 0.0207' / Cc= 0.900	n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf
Invert	20.74			
Device Routing	#1 Primary			
Device	#1			

WQv = 0.43 cfs 25-Year = 3.65 CFS Summary for Pond 5P: Ex. Hydrodynamic Separator

nflow D		9,184 cf, Atten= 0%, Lag= 0.0 min	9,184 cf
23,102 sf, 95.45% Impervious, 1	3.10 cfs @ 12.02 hrs, Volume=	3.10 cfs @ 12.02 hrs, Volume=	3.10 cfs @ 12.02 hrs, Volume=
Inflow Area =	= lutlow =	Outflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 21.93' @ 12.02 hrs Flood Elev= 24.12'

Invert Outlet Devices	20.74' 15.0" Round Ex. 15" RCP	L= 52.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 20.74' / 20.12' S= 0.0119' / Cc= 0.900	n= 0.011 Concrete pipe, straight & clean. Flow Area= 1.23 sf
Invert	20.74			
Device Routing	Primary			
Device	#1			

Type III 24-hr 10-Year Rainfall=5.11"

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Summary for Pond 6P: Ex. Manhole

23,102 sf, 95.45% Impervious, Inflow Depth = 4.77" for 10-Year event	9,184 cf	9,184 cf, Atten= 0%, Lag= 0.0 min	9,184 cf	
23,102 sf, 95.45% Impervious,	3.10 cfs @ 12.02 hrs, Volume=	3.10 cfs @ 12.02 hrs, Volume=	3.10 cfs @ 12.02 hrs, Volume=	
Inflow Area =		Outflow =	Primary =	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 21.48 @ 12.02 hrs Flood Elev= 24.12'

Invert Outlet Devices	20.02' 15.0" Round Ex. 15" HDPE	L= 8.0' CPP, projecting, no headwall, Ke= 0.900	nlet / Outlet Invert= 20.02' / 19.97' S= 0.0063 '/' Cc= 0.900	n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf
Outle	15.0	 8	Inlet	_ = 0
Invert	20.02			
Device Routing	Primary			
Device	#			

Primary OutFlow Max=3.08 cfs @ 12.02 hrs HW=21.47' TW=21.03' (Dynamic Tailwater) $^{-1}$ =Ex.15" HDPE (Inlet Controls 3.08 cfs @ 2.51 fps)

Summary for Pond 7P: Ex. Catch Basin

nflow Area = $\Pi = \Pi = \Pi$ Inflow Outflow Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 21.04 @ 12.02 hrs Flood Elev= 24.12'

Device Kouing Invert	Invert Outlet Devices	19.97' 15.0" Round Ex. 15" HDPE	L= 4.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 19.97' / 19.59' S= 0.0950 '/' Cc= 0.900	n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf	
Device Roung #1 Primary	Invert	19.97				
#1	Kouting	Primary				
	Device	#1				

Summary for Pond 8P: Ex. Manhole

Inflow [9,184 cf	9,184 cf, Atten= 0%, Lag= 0.0 min	9,184 cf
23,102 sf, 95.45% Impervious,	12.02 hrs, Volume=	3.10 cfs @ 12.02 hrs, Volume=	12.02 hrs, Volume=
23,102 sf,	3.10 cfs @	3.10 cfs @	3.10 cfs @
Inflow Area =	= wolJul	Outflow =	Primary =

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 19.63' @ 12.02 hrs Flood Elev= 24.12'

Device

#1

Invert Outlet Devices	18.59' 24.0 " Round Ex. 24" PVC	L= 42.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 18.59 / 18.23' S= 0.0086 '/ Cc= 0.900	n= 0.010 PVC, smooth interior, Flow Area= 3.14 sf
Invert	18.59			
Routing	Primary			

Primary OutFlow Max=3.08 cfs @ 12.02 hrs HW=19.63' TW=19.36' (Dynamic Tailwater) -1=Ex.24" PVC (Outlet Controls 3.08 cfs @ 2.73 fps)

Summary for Pond 9P: Ex. Manhole

Inflow Depth = 4.77" for 10-Year event	9,184 cf	.10 cfs @ 12.02 hrs, Volume= 9,184 cf, Atten= 0%, Lag= 0.0 min	9,184 cf
23,102 sf, 95.45% Impervious,	3.10 cfs @ 12.02 hrs, Volume=	3.10 cfs @ 12.02 hrs, Volume=	3.10 cfs @ 12.02 hrs, Volume=
Inflow Area =	= lutlow =	Outflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 19.37' @ 12.02 hrs Flood Elev= 24.12'

Invert Outlet Devices	17.78' 12.0" Round Ex. 12" RCP	L= 87.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 17.78 / 17.44 S= 0.0039 // Cc= 0.900	n= 0.011 Concrete pipe, straight & clean. Flow Area= 0.79 sf
Invert	17.78'			
Device Routing	Primary			
Device	#1			

Primary OutFlow Max=3.08 cfs @ 12.02 hrs HW=19.36' TW=0.00' (Dynamic Tailwater) —1=Ex.12" RCP (Barrel Controls 3.08 cfs @ 3.93 fps)

Summary for Pond 10P: Ex. Catch Basin

Inflow Depth = 4.58" for 10-Year event		8,030 cf, Atten= 0%, Lag= 0.0 min	
21,054 sf, 88.46% Impervious, Inflow Depth = 4.58"	2.73 cfs @ 12.02 hrs, Volume=	2.73 cfs @ 12.02 hrs, Volume=	2.73 cfs @ 12.02 hrs, Volume=
Inflow Area =	= luflow =	Outflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 20.26' @ 12.02 hrs Flood Elev= 24.12'

Routing Device #

18.77' 12.0" Round Ex. 12" RCP
L= 10.0' CPP-, projecting, no headwall, Ke= 0.900
Inlet / Outlet Invert= 18.77' / 18.58' S= 0.0190 '/ Cc= 0.900
n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf Primary

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Type III 24-hr 10-Year Rainfall=5.11"

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Summary for Pond 11P: Ex. Manhole

21,054 sf, 88.46% Impervious, Inflow Depth = 4.58" for 10-Year event	8,030 cf	8,030 cf, Atten= 0%, Lag= 0.0 min	8,030 cf	
21,054 sf, 88.46% Impervious,	2.73 dfs @ 12.02 hrs, Volume=	2.73 dfs @ 12.02 hrs, Volume=	2.73 cfs @ 12.02 hrs, Volume=	
Inflow Area =	Inflow =	Outflow =	Primary =	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 19.42 @ 12.02 hrs Flood Elev= 24.12'

Invert Outlet Devices	18.08' 12.0" Round Ex. 12" RCP	L= 17.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 18.08' / 17.54' S= 0.0318 '/' Cc= 0.900	n= 0.011 Concrete pipe, straight & clean. Flow Area= 0.79 sf
Invert	18.08			
Device Routing	Primary			
Device	#1			

Summary for Pond 12P: Trench Drain

nflow De	580 cf	580 cf, Atten= 0%, Lag= 0.0 min	580 cf
1,428 sf, 98.18% Impervious, Ir	0.20 cfs @ 12.01 hrs, Volume=	0.20 cfs @ 12.01 hrs, Volume=	0.20 cfs @ 12.01 hrs, Volume=
Inflow Area =	= moljul	Outflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 23.63' @ 12.02 hrs Flood Elev= 25.96'

Invert Outlet Devices	23.35' 12.0" Round 12" HDPE	L= 31.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 23.35' / 22.26' S= 0.0352 '/' Cc= 0.900	n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
Invert	23.35			
Device Routing	Primary			
Device	#			

Summary for Pond 13P: Relocated Drain Inlet

, Inflow Depth = 4.76" for 10-Year event	1,220 cf	0.42 ds @ 12.01 hrs, Volume= 1,220 cf, Atten= 0%, Lag= 0.0 min	1.220 cf
3,079 sf, 97.69% Impervious,	0.42 cfs @ 12.01 hrs, Volume=	0.42 cfs @ 12.01 hrs, Volume=	0.42 cfs @ 12.01 hrs. Volume=
Inflow Area =	Inflow	Outflow =	Primary =

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 23.47° @ 12.02 hrs Flood Elev= 25.05°

Invert Outlet Devices	22.45' 12.0" Round 12" HDPE	L= 35.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 22.45 / 22.26 S= 0.0054 // Cc= 0.900	n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
Invert	22.45'			
Device Routing	Primary			
Device	#1			

Summary for Pond 14P: Ex. Drain Inlet

Inflow Depth = 4.87" for 10-Year event		1,859 cf, Atten= 0%, Lag= 0.0 min	
Inflow Depth =	1,859 cf	1,859 cf	1,859 cf
4,579 sf, 99.28% Impervious,	12.01 hrs, Volume=	0.63 cfs @ 12.01 hrs, Volume=	12.01 hrs, Volume=
4,579 sf,	0.63 cfs @	0.63 cfs @	0.63 cfs @
nflow Area =	= MC	Outflow =	nary =
Inflo	Inflow	Out	Primar

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 23.01 @ 12.02 hrs Flood Elev= 23.63

Invert Outlet Devices	21.25' 1 5.0" Round 12" PVC	L= 45.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 21.25' / 20.79' S= 0.0102 '/ Cc= 0.900	n= 0.010 PVC, smooth interior, Flow Area= 1.23 sf
Invert	21.25'			
Device Routing	Primary			
Device	#1			

Type III 24-hr 25-Year Rainfall=6.41"

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Summary for Subcatchment 1A: Watershed 1A

2,355 cf, Depth= 6.17" 0.79 cfs @ 12.01 hrs, Volume= II Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=6.41"

						P2= 3.45"
						n= 0.011
	74 >75% Grass cover, Good, HSG C			ā	To Length Slope Velocity Capacity Description in) (feet) (ft/ft) (ft/sec) (cfs)	Sheet Flow, A-B Smooth surfaces n= 0.011 P2= 3.45"
	s cover, Go		verage ious Area	99.28% Impervious Area	Capacity (cfs)	
Area (sf) CN Description	75% Grass	98 Parking Lot	Weighted Average 0.72% Pervious Area	9.28% Imp	Velocity (ff/sec)	1.66
CN	74 >	98 P	0 86 0	6	Slope (ff/ft)	79 0.0330
ea (st)	33	4,546	4,579 33	4,546	Length (feet)	79
Ar		*			Tc (min)	0.8

Summary for Subcatchment 1B: Watershed 1B

1,553 cf, Depth= 6.05" 0.53 cfs @ 12.01 hrs, Volume= Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=6.41"

									i= 0.011 P2= 3.45"
	74 >75% Grass cover, Good, HSG C				ee	Tc Length Slope Velocity Capacity Description		Sheet Flow, A-B	Smooth surfaces n= 0.011 P2= 3.45"
	s cover, Go		verage	ious Area	97.69% Impervious Area	Capacity	(cts)		
Area (sf) CN Description	.75% Gras	98 Parking Lot	Weighted Average	2.31% Pervious Area	7.69% Imp	Velocity	(ft/sec)	1.37	
CN	< 4/	98 F	97 V	7	0	Slope	(ft/ft)	64 0.0225	
rea (st)	71	3,008	3,079	71	3,008	Length	(feet)	8	
∢		*				Tc	(min)	0.8	

Summary for Subcatchment 1C: Watershed 1C

1,624 cf, Depth= 5.94" 0.56 dfs @ 12.01 hrs, Volume= II Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=6.41"

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HydroCAD® 10:00-14 s/n 02549 © 2015 HydroCAD Software Solutions LLC		74 >75% Grass cover, Good, HSG C 98 Parking Lot		еа	Slope Velocity Capacity Description (ff/ft) (ff/sec) (ds)	Sheet Flow, A->B	Smooth surfaces n= 0.011 P2= 3.45" Shallow Concentrated Flow, B->C	Paved Kv= 20.3 fps
5 HydroCA		s cover, G	Weighted Average 7.43% Pervious Area	92.57% Impervious Area	Capacity (cfs)			
549 © 201	Area (sf) CN Description	>75% Grass Parking Lot	Weighted Average 7.43% Pervious Ar	2.57% Imp	Velocity (ff/sec)	1.51	2.58	
14 s/n 02	CN	74 × 98 P	7 96	6	Slope (ft/ft)	57 0.0305	53 0.0162	
J® 10.00-	rea (sf)	244 3,039	3,283	3,039	Tc Length in) (feet)	57	53	
HydroCA	Ā	*			T _C (min)	9.0	0.3	

Summary for Subcatchment 1D: Watershed 1D

110

0.9

734 cf, Depth= 6.17" 0.25 cfs @ 12.01 hrs, Volume= Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=6.41"

									Smooth surfaces n= 0.011 P2= 3.45"
od, HSG C				ee		Description		Sheet Flow, A-B	Smooth surfaces
s cover, Go		verage	ious Area	ervious Are		Capacity	(cts)		
75% Grass	arking Lot	Veighted A	.82% Perv	8.18% Imp		Velocity	(t/sec)	1.01	
74 >	98 F	98 V	_	6		Slope	(ft/ft)	0.0129	
56	1,402	1,428	56	1,402		Length	(feet)	42	
	*					J _C	(min)	0.7	
	26 74 >75% Grass cover, Good, HSG C	26 74 >75% Grass cover, Good, HSG C * 1,402 98 Parking Lot	26 74 >75% Grass cover, Good, HSG C 1,402 98 Parking Lot 1,428 98 Weighted Average	26 74 >75% Grass cover, Good, HSG C 1,402 98 Parking Lot 1,428 98 Weighted Average 26 1.82% Pervious Area	26 74 >75% Grass cover, Good, HSG C 1,402 98 Parking Lot 1,428 99 Welghted Average 26 1,82% Pervious Area 1,402 98.18% Impervious Area	26 74 >75% Grass cover, Good, HSG C 1,402 98 Parking Lot 1,428 98 Weighted Average 26 1.82% Pervious Area 1,402 98.18% Impervious Area	26 74 >75% Grass cover, Good, HSG C 1,402 98 Parking Lot 1,428 98 Weighted Average 26 1.82% Pervious Area 1,402 98.18% Impervious Area Tc Length Slope Velocity Capacity Description	26 74 >75% Grass cover, Good, HSG C 1,402 98 Parking Lot 1,428 99 Welghted Average 26 1.82% Pervious Area 1,402 98.18% Impervious Area TC Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (ds)	26 74 >75% Grass cover, Goc 1,402 98 Parking Lot 1,428 99 Weighted Average 26 1,82% Pervious Area 1,402 98.18% Impervious Area 1,402 98.18% Impervious Area Length Slope Velocity Capacity (feet) (ft/ft) (ft/sec) (ds) 42 0.0129 1.01

Summary for Subcatchment 2: Ex. Roof Area & Planter Watershed 2

6.05
Depth=
5,414 cf,
Volume=
12.01 hrs,
1.84 cfs @
II
Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=6.41"

Area (sf) CN Description	Roof	Planter	Weighted Average	6.31% Pervious Area	93.69% Impervious Area
S	86	79	6		
Area (sf)	10,056	229	10,733	229	10.056
	*	*			

Type III 24-hr 25-Year Rainfall=6.41"

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	Direct Entry,				1.0
	(cfs)	ft/sec)	(ft/ft) (f	(feet)	(min)
	acity Description	Slope Velocity Capacity [Slope Ve	Length	J _C
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Summary for Subcatchment 3: Watershed 3

1,154 cf, Depth= 4.69" 0.44 cfs @ 12.01 hrs, Volume= Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=6.41"

ui	74 >75% Grass cover, Good, HSG C	idewalks	Weighted Average	56.06% Pervious Area	43.94% Impervious Area	Tc Length Slope Velocity Capacity Description) (cfs)	Direct Entry.
Area (sf) CN Description	>75% Gra	Building/sidewalks	Weighted	56.06% P	43.94% Ir	e Velocit	t) (ft/sec)	
CN	74	86	82			Slop	(£/)	
rea (sf)	1,655	1,297	2,952	1,655	1,297	Length	(teet)	
Ā		*				T _C	(min)	0.5

Summary for Subcatchment 3A: Roof Area & Planter Watershed 3A

7,443 cf, Depth= 6.05" 2.53 dfs @ 12.01 hrs, Volume= Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=6.41"

Summary for Subcatchment 3B: Watershed 3B

1,688 cf, Depth= 6.05" 0.57 cfs @ 12.01 hrs, Volume= Runoff Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=6.41"

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									45"
									P2= 3.
									n = 0.011
	>75% Grass cover, Good, HSG C				aa	Tc Length Slope Velocity Capacity Description		Sheet Flow, A-B	Smooth surfaces n= 0.011 P2= 3.45"
	s cover, Gc		verage	ious Area	96.95% Impervious Area	Capacity	(cts)		
Area (sf) CN Description	-75% Gras	98 Parking Lot	Weighted Average	3.05% Pervious Area	96.95% Imp	Velocity	(ft/sec)	1.29	
CN	74	98 F	97	.,	0,	Slope	(ft/ft)	0.0180	
rea (sf)	102	3,245	3,347	102	3,245	Length	(feet)	74 0.0180	
∀		*				Tc	(min)	1.0	

Summary for Reach DP: DP

Inflow Depth = 5.97" for 25-Year event	7.30 cfs @ 12.02 hrs, Volume= 21,967 cf	21,967 cf, Atten= 0%, Laq= 0.0 min
44,156 sf, 92.12% Impervious,	7.30 cfs @ 12.02 hrs, Volume=	7.30 cfs @ 12.02 hrs, Volume=
Inflow Area =	= luflow =	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3

Summary for Pond 1P: Ex. Stormwater Planter

Inflow Depth = 6.05" for 25-Year event	.84 cfs @ 12.01 hrs, Volume= 5,414 cf	5,414 cf, Atten= 1%, Lag= 0.5 min	5,414 cf	Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 27.86' @ 12.02 hrs Surf.Area= 669 sf Storage= 907 d
93.69% Impervious,	1.84 cfs @ 12.01 hrs, Volume=	1.81 cfs @ 12.02 hrs, Volume=	1.81 cfs @ 12.02 hrs, Volume=	Time Span= 0.00-60 Surf.Area= 669 sf S
10,733 sf,	1.84 cfs @	1.81 cfs @	1.81 cfs @	-Stor-Ind method, 36' @ 12.02 hrs
Inflow Area =	= molful	Outflow =	Primary =	Routing by Dyn- Peak Elev= 27.8

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 132.6 min (878.9 - 746.3)

	1,004 cf Custom Stage Data (Prismatic)Listed below (Recalc				
Invert Avail. Storage Storage Description	ı Stage Data (Prisn	Cum.Store	(cubic-feet)	0	1,004
Storage	Custom	Inc.Store	cubic-feet)	0	1.004
.Storage	1,004 cf	<u>lu</u>	(cubi		
Avail.		Surf.Area	(sd-ft)	699	699
Invert	26.50'	Sur			
Volume	#1	Elevation	(feet)	26.50	28.00

Invert Outlet Devices	23.50' 12.0" Round Culvert	L= 64.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 23.50 / 22.26 S= 0.0194 / Cc= 0.900	n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf	_	Limited to weir flow at low heads	26.50' 2.000 in/hr Exfiltration over Surface area
Invert	23.50				27.75		26.50
Device Routing	#1 Primary	•			#2 Device 1		#3 Device 1
Device	#1				#2		#3

Type III 24-hr 25-Year Rainfall=6.41"

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Primary OutFlow Max=1.80 cfs @ 12.02 hrs HW=27.86' TW=25.08' (Dynamic Tailwater)

—1=Culvert (Passes 1.80 cfs of 4.98 cfs potential flow)

—2=Orifice/Grate (Weir Controls 1.77 cfs @ 1.06 fps)

—3=Exfiltration (Exfiltration Controls 0.03 cfs)

ummary for Pond 2P: 1.0 Foot High Stormwater Planter 673 SQ. FT. W/ 7 Outlets & 80 SF FocalPoint Sys

Inflow Area Inflow		18,102 sf, 95.72% Impervious, 3.10 cfs @ 12.01 hrs, Volume=	95.72% In 12.01 hrs,	pervious, Volume=	18,102 sf, 95.72% Impervious, Inflow Depth = 6.05" for 25-Year event 10 cfs @ 12.01 hrs, Volume= 9,131 cf	ar event
	II	2.99 cfs @	12.03 hrs,	Volume=	9,132 cf, Atten= 4%, La	g= 0.9 min
	II	2.99 cfs @	12.03 hrs,	Volume=	9,132 cf	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 22.25' @ 12.03 hrs Suff.Area= 80 sf Storage= 489 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 7.5 min (753.8 - 746.3)

Avail.Storage Storage Description	36 cf 4.00'W x 20.00'L x 2.25'H FocalPoint	180 of Overall x 20.0% Voids Stormwater Planter (Prismatic) isted below (Recalc) Impensions	Edd of Total Available Storage	Total Available Stotage	Inc.Store Cum.Store	cubic-feet) (cubic-feet)	0 0
il.Storage	36 cf	505 of	10 P	2 - 2	lnc)	
		_			Surf.Area	(sd-ft)	673
Invert	19.33	21 58'	2		S		
Volume	#1	¥	!		Elevation	(feet)	21.58

et)	10	37	505			L= 19.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 19.00' / 18.77' S= 0.0121 '/' Cc= 0.900	9 sf	100.000 in/hr Exfiltration over Surface area	Device 1 22.08 8.0" Horiz. Orifice/Grate X 6.00 C= 0.600 Limited to weir flow at low heads		
(cubic-feet)		က	2	S	Culvert	P, projecting	nvert= 19.00	w Area= 0.7	Exfiltration	rifice/Grate	ir flow at low	
(cubic-feet)	0	337	168	Invert Outlet Devices	19.00' 12.0" Round Culvert	L= 19.0' CPF	Inlet / Outlet I	n= 0.013, Flow Area= 0.79 sf	100.000 in/hr	8.0" Horiz. O	Limited to wei	
Sull.Alea (Sq-ft)	673	673	673	Invert	19.00′				19.33	22.08		
∓ ∓	88	80	83	Device Routing	Primary				Device 1	Device 1		
(feet)	21.58	22.08	22.33	Device	#				4	¥		

Primary OutFlow Max=3.07 cfs @ 12.03 hrs HW=22.25' TW=21.19' (Dynamic Tailwater)

—1=Culvert (Inlet Controls 3.07 cfs @ 3.91 fps)

—2=Exfiltration (Passes < 0.19 cfs potential flow)

—3=Orifice/Grate (Passes < 2.95 cfs potential flow)

Summary for Pond 3P: Ex. Drainage Manhole

Inflow Depth = 6.06" for 25-Year event		7,702 cf, Atten= 0%, Lag= 0.0 min	7,702 cf
15,240 sf, 94.92% Impervious, Inflow Depth = 6	2.57 cfs @ 12.02 hrs, Volume=	2.57 cfs @ 12.02 hrs, Volume=	2.57 cfs @ 12.02 hrs, Volume=
Inflow Area =	Inflow	Outflow =	Primary =

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 25.12° @ 12.02 hrs Flood Elev= 26.50°

Invert Outlet Devices	22.16' 12.0" Round 12" PVC	L= 101.5' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 22.16 / 20.74 S= 0.0140 / Cc= 0.900	n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf
Invert	22.16'			
Device Routing	Primary			
Device	#1			

Summary for Pond 4P: Ex. Drain Inlet

Inflow Depth = 6.07" for 25-Year event	11,681 cf	11,681 cf, Atten= 0%, Lag= 0.0 min	11,681 of
23,102 sf, 95.45% Impervious,	3.91 cfs @ 12.02 hrs, Volume=	3.91 cfs @ 12.02 hrs, Volume= 11,681 cf, Atter	3.91 cfs @ 12.02 hrs, Volume=
Inflow Area =	= luflow =	Outflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 24.39 @ 12.02 hrs Flood Elev= 23.90'

Invert Outlet Devices	20.74' 12.0" Round 12" PVC	L= 14.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 20.74' / 20.45' S= 0.0207' / Cc= 0.900	n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf
Invert	20.74			
Device Routing	#1 Primary			
Device	#1			

WQv = 0.43 cfs 25-Year = 3.65 CFS Summary for Pond 5P: Ex. Hydrodynamic Separator

event		Lag= 0.0 min	
or 25-Year event		0%, Lag= (
6.07" for		, Atten=	
23,102 sf, 95.45% Impervious, Inflow Depth = 1	11,681 cf	11,681 cf	11,681 of
pervious,	Volume=	Volume=	Volume=
95.45% In	12.02 hrs,	12.02 hrs,	12.02 hrs,
23,102 sf,	3.91 cfs @	3.91 cfs @ 12.02 hrs, Volume=	3.91 cfs @
ea =	II	II	II
Inflow Are	Inflow	Outflow	Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 22.70 @ 12.02 hrs Flood Elev= 24.12'

Invert Outlet Devices	20.74' 15.0" Round Ex. 15" RCP	L= 52.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert = 20.74 / 20.12' S = 0.0119 '/ Cc = 0.900	n= 0.011 Concrete pipe, straight & clean, Flow Area= 1.23 sf
Invert	20.74			
Device Routing	Primary			
Device	#1			

Type III 24-hr 25-Year Rainfall=6.41"

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Summary for Pond 6P: Ex. Manhole

Inflow Depth = 6.07" for 25-Year event	11,681 cf	11,681 cf, Atten= 0%, Lag= 0.0 min	11,681 cf
23,102 sf, 95.45% Impervious, Inflow Depth = 6.07"	3.91 cfs @ 12.02 hrs, Volume=	3.91 cfs @ 12.02 hrs, Volume=	3.91 cfs @ 12.02 hrs, Volume=
Inflow Area =	= lutlow =	Outflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, d= 0.01 hrs / 3 Peak Elev= 22.00 @ 12.02 hrs Flood Elev= 24.12'

Device ¥

Invert Outlet Devices	20.02' 15.0" Round Ex. 15" HDPE	L= 8.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 20.02' / 19.97' S= 0.0063 '/' Cc= 0.900	n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf
Invert	20.02			
Kouting	Primary			

Primary OutFlow Max=3.89 cfs @ 12.02 hrs HW=21.98' TW=21.29' (Dynamic Tailwater) $^+$ 1=Ex.15" HDPE (Inlet Controls 3.89 cfs @ 3.17 fps)

Summary for Pond 7P: Ex. Catch Basin

23,102 sf, 95.45% Impervious, Inflow Depth = 6.07" for 25-Year event	1,681 cf	11,681 cf, Atten= 0%, Lag= 0.0 min	1,681 cf
ervious, Inflow De	Volume= 1		
95.45% Imp	12.02 hrs, V	12.02 hrs, V	12.02 hrs, Volume
23,102 sf,	3.91 cfs @	3.91 cfs @ 12.02 hrs, \	3.91 cfs @
ea =	II	II	II
Inflow Area	Inflow	Outflow	Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 21.30' @ 12.02 hrs Flood Elev= 24.12'

Invert Outlet Devices	19.97' 15.0" Round Ex. 15" HDPE	L= 4.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 19.97' / 19.59' S= 0.0950 '/' Cc= 0.900	n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf
Invert	19.97			
Device Routing	Primary			
Device	#			

Primary OutFlow Max=3.89 cfs @ 12.02 hrs HW=21.29' TW=20.13' (Dynamic Tailwater) -1=Ex.15" HDPE (Inlet Controls 3.89 cfs @ 3.17 fps)

Summary for Pond 8P: Ex. Manhole

23,102 sf, 95.45% Impervious, Inflow Depth = 6.07" for 25-Year event	11,681 cf	11,681 cf, Atten= 0%, Lag= 0.0 min	11,681 cf
23,102 sf, 95.45% Impervious,	3.91 cfs @ 12.02 hrs, Volume=	3.91 cfs @ 12.02 hrs, Volume=	3.91 cfs @ 12.02 hrs, Volume=
Inflow Area =	II		Primary =

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Type III 24-hr 25-Year Rainfall=6.41"

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 20.15' @ 12.02 hrs Flood Elev= 24.12'

Invert Outlet Devices	18.59' 24.0" Round Ex. 24" PVC	L= 42.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 18.59 / 18.23 S= 0.0086 / Cc= 0.900	n= 0.010 PVC, smooth interior, Flow Area= 3.14 sf
Invert	18.59			
Device Routing	Primary			
Device	#1			

Summary for Pond 9P: Ex. Manhole

Inflow Depth = 6.07" for 25-Year event	11,681 of	91 cfs @ 12.02 hrs, Volume= 11,681 cf, Atten= 0%, Lag= 0.0 min	11,681 of
23,102 sf, 95.45% Impervious,	3.91 cfs @ 12.02 hrs, Volume=	3.91 cfs @ 12.02 hrs, Volume=	3.91 cfs @ 12.02 hrs, Volume=
Inflow Area =	= luflow =	Outflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 19.99 @ 12.02 hrs Flood Elev= 24.12'

Invert Outlet Devices	17.78' 12.0" Round Ex. 12" RCP	L= 87.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 17.78' / 17.44' S= 0.0039 '/ Cc= 0.900	n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf
Invert	17.78			
Device Routing	#1 Primary			
Device	#1			

Summary for Pond 10P: Ex. Catch Basin

Inflow Area = 21,054 st, 88.4% impervious, inflow Lepth = 5.86" inflow = 3.39 cfs @ 12.01 hrs, Volume= 10,286 cf Outflow = 3.39 cfs @ 12.01 hrs, Volume= 10,286 cf, Atter
II
<u>0</u>

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 21.20 @ 12.02 hrs Flood Elev= 24.12'

Invert Outlet Devices	18.77' 12.0" Round Ex. 12" RCP	L= 10.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 18.77' / 18.58' S= 0.0190 '/ Cc= 0.900	n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf
Invert	18.77			
Device Routing	#1 Primary			
Device	#1			

Type III 24-hr 25-Year Rainfall=6.41"

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Summary for Pond 11P: Ex. Manhole

Inflow Area =	21,054 sf, 88.46% Impervious,	Inflow Depth = 5.86" for 25-Year event
Inflow =	3.39 cfs @ 12.01 hrs, Volume=	10,286 cf
Outflow =	3.39 dfs @ 12.01 hrs, Volume=	10,286 cf, Atten= 0%, Lag= 0.0 min
Primary =	3.39 cfs @ 12.01 hrs, Volume=	3.39 cfs @ 12.01 hrs, Volume= 10,286 cf
		-

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 19.87' @ 12.01 hrs Flood Elev= 24.12'

Invert Outlet Devices	18.08' 12.0" Round Ex. 12" RCP	L= 17.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 18.08 / 17.54 S= 0.0318 // Cc= 0.900	n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf
Invert	18.08			
Device Routing	Primary			
Device	#			

Summary for Pond 12P: Trench Drain

,428 sf, 98.18% Impervious, Inflow Depth = 6.17" for 25-Year event	734 cf	734 cf, Atten= 0%, Lag= 0.0 min	734 cf
1,428 sf, 98.18% Impervious,	0.25 cfs @ 12.01 hrs, Volume=	0.25 cfs @ 12.01 hrs, Volume=	0.25 cfs @ 12.01 hrs, Volume=
Inflow Area =	= mllow =	Outflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 25.12' @ 12.02 hrs Flood Elev= 25.96'

Invert Outlet Devices	23.35' 12.0" Round 12" HDPE	L= 31.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 23.35 / 22.26 S= 0.0352 // Cc= 0.900	n= 0.013 Corrugated PE. smooth interior. Flow Area= 0.79 sf
Invert	23.35			
Routing	#1 Primary			
Device Routing	#			

Primary OutFlow Max=0.00 cfs @ 12.01 hrs HW=24.87' TW=24.93' (Dynamic Tailwater) -1=12" HDPE (Controls 0.00 ds)

Summary for Pond 13P: Relocated Drain Inlet

v Depth = 6.05" for 25-Year event	1,553 cf	1,553 cf, Atten= 0%, Lag= 0.0 min	1.553 cf
3,079 sf, 97.69% Impervious, Inflov	0.53 cfs @ 12.01 hrs, Volume=	0.53 cfs @ 12.01 hrs, Volume= 1,553 cf, Atten= 0%, Lag= 0.0 min	0.53 cfs @ 12.01 hrs. Volume=
Inflow Area =		Ontflow =	

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 25.14' @ 12.02 hrs Flood Elev= 25.05'

Invert Outlet Devices	22.45' 12.0" Round 12" HDPE	L= 35.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 22.45' / 22.26' S= 0.0054 '/ Cc= 0.900	n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
Invert	22.45'			
Device Routing	Primary			
Device	#1			

Primary OutFlow Max=0.00 cfs @ 12.01 hrs HW=24.93' TW=24.96' (Dynamic Tailwater) -1=12" HDPE (Controls 0.00 cfs)

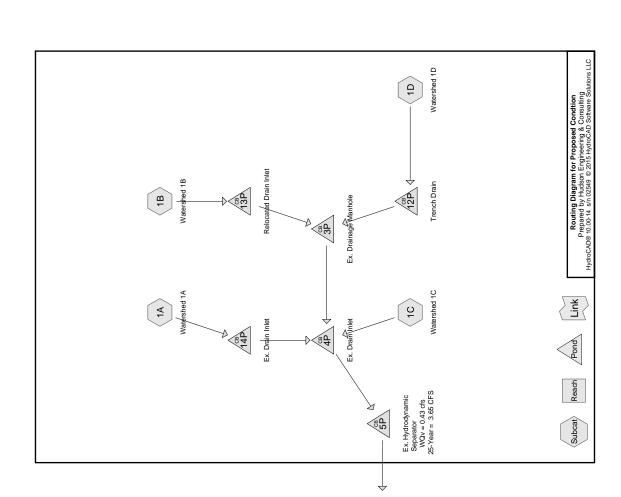
Summary for Pond 14P: Ex. Drain Inlet

4,579 sf, 99.28% Impervious, Inflow Depth = 6.17" for 25-Year event 0.79 cfs @ 12.01 hrs, Volume= 2,355 cf, Atten= 0%, Lag= 0.0 min 0.79 cfs @ 12.01 hrs, Volume= 2,355 cf	Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 24.40' @ 12.02 hrs Flood Elev= 23.63'
39.28% Impervious, 2.01 hrs, Volume= 2.01 hrs, Volume= 2.01 hrs, Volume=	Time Span= 0.00-60
4,579 sf, 9 0.79 cfs @ 1 0.79 cfs @ 1 0.79 cfs @ 1	-Stor-Ind method, 40' @ 12.02 hrs .63'
Inflow Area = Inflow = Outflow = Primary =	Routing by Dyn-Ste Peak Elev= 24.40' Flood Elev= 23.63'

Invert Outlet Devices	21.25' 15.0" Round 12" PVC	L= 45.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 21.25' / 20.79' S= 0.0102 '/ Cc= 0.900	n= 0.010 PVC, smooth interior. Flow Area= 1.23 sf
Invert	21.25'			
Device Routing	#1 Primary			
Device	#1			

Primary OutFlow Max=0.00 cfs @ 12.01 hrs HW=24.27' TW=24.30' (Dynamic Tailwater) __1=12" PVC (Controls 0.00 cfs)

	8). Water Quality Calculations
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Type III 24-hr WQv Parking Rainfall=1.69" Proposed Condtion
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Summary for Subcatchment 1A: Watershed 1A

560 cf, Depth= 1.47" 0.20 cfs @ 12.01 hrs, Volume= Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr WQv Parking Rainfall=1.69"

								l	
									P2= 3.45"
									n = 0.011
	74 >75% Grass cover, Good, HSG C				a	Tc Length Slope Velocity Capacity Description		Sheet Flow, A-B	Smooth surfaces n= 0.011 P2= 3.45"
	cover, Go	,	/erage	ous Area	99.28% Impervious Area	Capacity	(cts)		
CN Description	75% Grass	98 Parking Lot	Weighted Average	0.72% Pervious Area	9.28% Imp	Velocity	(ft/sec)	1.66	
C C C	74 >	98 P	N 86	0	0	Slope	(ft/ft)	79 0.0330	
Area (st)	33	4,546	4,579	33	4,546	Length	(feet)	79	
Ā		*				ည	(min)	0.8	

Summary for Subcatchment 1B: Watershed 1B

351 cf, Depth= 1.37" 0.13 cfs @ 12.01 hrs, Volume= Runoff Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr WQv Parking Rainfall=1.69"

									2= 3.45"
									n= 0.011
	74 >75% Grass cover, Good, HSG C				aa	Tc Length Slope Velocity Capacity Description		Sheet Flow, A-B	Smooth surfaces n= 0.011 P2= 3.45"
	cover, Go		/erage	ous Area	97.69% Impervious Area	Capacity	(cts)		
Area (sf) CN Description	75% Grass	98 Parking Lot	Weighted Average	2.31% Pervious Area	7.69% Imp	Velocity	(tt/sec)	1.37	
CN	74 >	98 P	97 W	2	6	Slope	(ft/ft)	64 0.0225	
ea (sf)	71	3,008	3,079	71	3,008	Length	(teet)	64	
Ā		*				Тc	(min)	0.8	

Summary for Subcatchment 1C: Watershed 1C

349 cf, Depth= 1.28" 0.13 dfs @ 12.01 hrs, Volume= Runoff Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr WQv Parking Rainfall=1.69"

Type III 24-hr WQv Parking Rainfall=1.69"

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Type III 24
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	>75% Grass cover, Good, HSG C			rea	s Area	Slone Velocity Canacity Description	(ds)	Sheet Flow, A->B	Smooth surfaces n= 0.011 P2= 3.45"	Shallow Concentrated Flow, B->C	Paved Kv= 20.3 fps	
	s cove		verage	ious A	ervio	, ac	5					
Area (sf) CN Description	75% Gras	Parking Lot	Weighted Average	7.43% Pervious Area	92.57% Impervious Area	Velocity	(ft/sec)	1.51		2.58		
N.		98 P	M 96	7	60	Slope	(#/#)	57 0.0305		53 0.0162		110 Total
U						_		0		0		T (
rea (sf)	244	3,039	3,283	24	3,039	To I enoth	(feet)			55		110
۷						Ľ	(min)	9.0		0.3		6.0
		*						ı				

Summary for Subcatchment 1D: Watershed 1D

175 cf, Depth= 1.47"
Volume=
12.01 hrs,
0.06 cfs @
II
Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr WQv Parking Rainfall=1.69"

					- 1		
							P2= 3.45"
							n = 0.011
CN Description 74 >75% Grass cover Good HSG C	000000000000000000000000000000000000000		39	To Length Slope Velocity Capacity Description	; ;	Sheet Flow, A-B	Smooth surfaces n= 0.011 P2= 3.45"
ocy Javos	, , , ,	verage	ervious Are	Capacity	(cts)		
Area (sf) CN Description	98 Parking Lot	Weighted Average	98.18% Impervious Area	Velocity	(#/sec)	1.01	
CN 42	98 F	98	- 0,	Slope	(11/11)	42 0.0129	
ea (st)	1,402	1,428	1,402	Length	(teet)	42	
Ā	*			L J	(min)	0.7	

Summary for Pond 3P: Ex. Drainage Manhole

for WQv Parking event		%, Lag= 0.0 min	
15,240 sf, 94.92% Impervious, Inflow Depth = 1.38" for	1,750 cf	1,750 cf, Atten= 0%, Lag= 0.0 min	1,750 cf
f, 94.92% Impervious,	3.22 cfs @ 12.01 hrs, Volume=	3.22 cfs @ 12.01 hrs, Volume=	3.22 cfs @ 12.01 hrs, Volume=
rea = 15,240 sf	= 0.22 cfs @	= 0.22 cfs @	= 0.22 cfs @
Inflow Ar	Inflow	Outflow	Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 22.42' @ 12.01 hrs Flood Elev= 26.50'

Invert Outlet Devices	22.16' 12.0" Round 12" PVC	L= 101.5' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 22.16 / 20.74 S= 0.0140 / Cc= 0.900	n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf
Inve	22.1			
Device Routing	#1 Primary			
Device	#1			

Type III 24-hr WQv Parking Rainfall=1.69"

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Primary OutFlow Max=0.22 dfs @ 12.01 hrs HW=22.42' TW=21.26' (Dynamic Tailwater) —1=12" PVC (Inlet Controls 0.22 dfs @ 1.37 fps)

Summary for Pond 4P: Ex. Drain Inlet

23.102 st, 95.45% Impervious, Inflow Depth = 1.38" for WQv Parking event 2.65 ds @ 12.01 hrs, Volume= 2,659 cf, Atten= 0%, Lag= 0.0 min 2.56 ds @ 12.01 hrs, Volume= 2,659 cf	0.00 hrs, dt= 0.01 hrs / 3
23,102 sf, 95,45% Impervious, 0.56 cfs @ 12.01 hrs, Volume= 0.56 cfs @ 12.01 hrs, Volume= 0.56 cfs @ 12.01 hrs, Volume=	Routing by Dyn-Stor-Ind method, Time Span= 0.00 - 60.00 hrs, d= 0.01 hrs / 3 Peak Elev= 21.26° @ 12.01 hrs Flood Elev= 23.90°
Inflow Area = Inflow = Outflow = Primary =	Routing by Dyn-Sto Peak Elev= 21.26' Flood Elev= 23.90'

12.0" Round 12" PVC
L= 14.0" CPP, projecting, no headwall, Ke= 0.900
Inlet / Oullet Invert= 20.74', 20.45' S= 0.0207' /' Cc= 0.900
Inlet / Oullet Rinvert= 20.74' Flow Area= 0.79 sf Invert Outlet Devices 20.74 Device Routing Primary

¥

Primary OutFlow Max=0.55 cfs @ 12.01 hrs HW=21.26' TW=21.13' (Dynamic Tailwater) $^-$ 1=12" PVC (Outlet Controls 0.55 cfs @ 1.94 fps)

WQv = 0.43 cfs 25-Year = 3.65 CFS Summary for Pond 5P: Ex. Hydrodynamic Separator

, Inflow Depth = 1.38" for WQv Parking event	2,659 cf	2,659 cf, Atten= 0%, Lag= 0.0 min	2,659 cf
23,102 sf, 95.45% Impervious,	0.56 cfs @ 12.01 hrs, Volume=	0.56 cfs @ 12.01 hrs, Volume=	0.56 ds @ 12.01 hrs, Volume=
Inflow Area =	= lutiow =	Ontflow =	Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 21.13' @ 12.01 hrs Flood Elev= 24.12'

Invert Outlet Devices	20.74' 15.0" Round Ex. 15" RCP	L= 52.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 20.74' / 20.12' S= 0.0119 '/' Cc= 0.900	n= 0.011 Concrete pipe, straight & clean, Flow Area= 1.23 sf
Invert	20.74			
Device Routing	Primary			
Device	#			

Summary for Pond 12P: Trench Drain

17" for WOv Parking event		175 cf, Atten= 0%, Lag= 0.0 min	
Inflow Denth = 1.4	175 cf		
1 428 sf 98 18% Impervious Inflow Denth = 1 47" for WQv Parking event	0.06 cfs @ 12.01 hrs. Volume=	0.06 cfs @ 12.01 hrs, Volume=	0.06 cfs @ 12.01 hrs. Volume=
II	II	II	II
Inflow Are	Inflow	Outflow	Primary

Type III 24-hr WQv Parking Rainfall=1.69"

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Proposed Condtion

Type III 24
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Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 23.49 @ 12.01 hrs Flood Elev= 25.96'

Invert Outlet Devices	23.35' 12.0" Round 12" HDPE	L= 31.0' CPP, projecting, no headwall, Ke= 0.900	nlet / Outlet Invert= 23.35 / 22.26' S= 0.0352 '/ Cc= 0.900	n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
Invert	23.35			
Device Routing	Primary			
Device	#1			

Primary OutFlow Max=0.06 cfs @ 12.01 hrs HW=23.49' TW=22.42' (Dynamic Tailwater) \uparrow 1=12" HDPE (Inlet Controls 0.06 cfs @ 0.99 fps)

Summary for Pond 13P: Relocated Drain Inlet

	3,079 St, 97.69% Impervious, Inflow Dep	= 0.1	= 0.13 cfs @ 12.01 hrs, Volume=	= 0.13 cfs @ 12.01 hrs, Volume=	ng by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3	Peak Elev= 22.66' @ 12.01 hrs	Flav. 25 05'
V	Inflow Area =	Inflow =	Outflow =	Primary =	Routing by Dyn	Peak Elev= 22.	FLOOD FLOOD 25 OF!

Invert Outlet Devices	22.45' 1 2.0" Round 12" HDPE	L= 35.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 22.45' / 22.26' S= 0.0054 '/ Cc= 0.900	n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
Invert	22.45			
Device Routing	#1 Primary			
Device	#1			

Summary for Pond 14P: Ex. Drain Inlet

iflow Depth = 1.47" for WQv Parking event	560 cf	560 cf, Atten= 0%, Lag= 0.0 min	560 cf
4,579 sf, 99.28% Impervious, Inflow Depth = 1.47" f	0.20 cfs @ 12.01 hrs, Volume=	0.20 cfs @ 12.01 hrs, Volume=	0.20 cfs @ 12.01 hrs, Volume=
Inflow Area =	= luflow =	Outflow =	Primary =

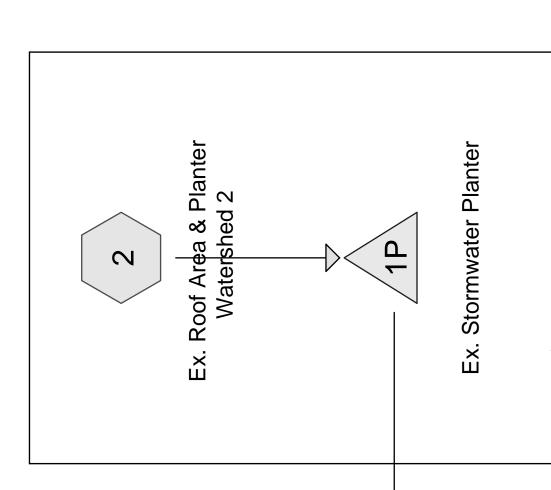
Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 21.49 @ 12.01 hrs Flood Elev= 23.63'

Invert Outlet Devices	21.25' 15.0" Round 12" PVC	L= 45.0' CPP, projecting, no headwall, Ke= 0.900	Inlet / Outlet Invert= 21.25 / 20.79' S= 0.0102 '/ Cc= 0.900	n= 0.010 PVC, smooth interior. Flow Area= 1.23 sf
Invert	21.25'			
Device Routing	#1 Primary			
Device	#1			

Type III 24-hr WQv Parking Rainfall=1.69"

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Type III 24-hr WQv Ex. Roof Rainfall=1.67"

Page 2

Summary for Subcatchment 2: Ex. Roof Area & Planter Watershed 2

1,206 cf, Depth= 1.35" 0.44 cfs @ 12.01 hrs, Volume= II Runoff Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr WQv Ex. Roof Rainfall=1.67"

Area (sf) CN Description 10,056 98 Roof 677 79 Planter 10,733 97 Weighted Average 677 6.31% Pervious Area 10,056 93.69% Impervious Area TC Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)									
rea (sf) CN Description 10,056 98 Roof 677 79 Planter 10,733 97 Weighted Average 677 6,31% Pervious Area 10,056 93,69% Impervious Area Length Slope Velocity (feet) (ft/ft) (ft/sec) (feet) (ft/ft) (ft/sec)									
rea (sf) CN Description 10,056 98 Roof 677 79 Planter 10,733 97 Weighted Average 677 6,31% Pervious Area 10,056 93,69% Impervious Area Length Slope Velocity (feet) (ft/ft) (ft/sec) (feet) (ft/ft) (ft/sec)									
rea (sf) CN Description 10,056 98 Roof 677 79 Planter 10,733 97 Weighted Average 677 6,31% Pervious Area 10,056 93,69% Impervious Area Length Slope Velocity (feet) (ft/ft) (ft/sec) (feet) (ft/ft) (ft/sec)									
rea (sf) CN Description 10,056 98 Roof 677 79 Planter 10,733 97 Weighted Average 677 6,31% Pervious Area 10,056 93,69% Impervious Area Length Slope Velocity (feet) (ft/ft) (ft/sec) (feet) (ft/ft) (ft/sec)									
rea (sf) 10,056 677 10,733 677 10,056 Length (feet)						ea	Description		Direct Entry.
rea (sf) 10,056 677 10,733 677 10,056 Length (feet)				verage	ious Area	ervious Are	Capacity	(cfs)	
rea (sf) 10,056 677 10,733 677 10,056 Length (feet)	escription	oof	lanter	eighted A	31% Perv	3.69% Imp	Velocity	(ft/sec)	
Area (sf) 10,056 677 10,733 677 10,056 TC Length (min) (feet)	CN	98 R	79 P	26		6	Slope	(ft/ft)	
T C	ea (st)	10,056	677	10,733	229	10,056	Length	(feet)	
* *	Ā	*	*				٦ ۲	(min)	1.0

Summary for Pond 1P: Ex. Stormwater Planter

10,733 sf, 93.69% Impervious, Inflow Depth = 1.35" for WQv Ex. Roof event 0.04 cfs @ 12.01 hrs, Volume= 1,206 cf 0.03 cfs @ 11.59 hrs, Volume= 1,206 cf, Atten= 93%, Lag= 0.0 min 0.03 cfs @ 11.59 hrs, Volume= 1,206 cf Inflow Area = Inflow = = Outflow Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 27.18' @ 12.96 hrs Surf.Area= 669 sf Storage= 455 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 112.3 min (892.4 - 780.1)

	elow (Recalc)					000		w Area= 0.79 sf		
Description	1,004 cf Custom Stage Data (Prismatic)Listed below (Recalc)	Cum.Store (cubic-feet)	0	1,004		Culvert	L= 04.0 CFP, projectifig, fig fleatwar, NE= 0.300 inlet / Outlet Invert= 23.50 / 22.26 S= 0.0194 // Cc= 0.900	n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf	6.0" Horiz. Orifice/Grate X 10.00 C= 0.600	Limited to weir flow at low heads 2.000 in/hr Exfiltration over Surface area
Invert Avail.Storage Storage Description	t cf Custom	Inc.Store (cubic-feet)	0	1,004	Invert Outlet Devices	23.50' 12.0" Round Culvert	L= 64.0 CFF Inlet / Outlet In	n= 0.013 Corr	6.0" Horiz. Ori	Limited to weir 2.000 in/hr Ext
Avail.Stora	1,00	Surf.Area (sq-ft)	699	699	Invert	23.50			27.75	26.50
Invert	26.50		C	0	Routing	Primary			Device 1	Device 1
Volume	#1	Elevation (feet)	26.50	28.00	Device Routing	#1			#2	#3

Routing Diagram for Proposed Condition
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Type III 24-hr WQv Ex. Roof Rainfall=1.67"

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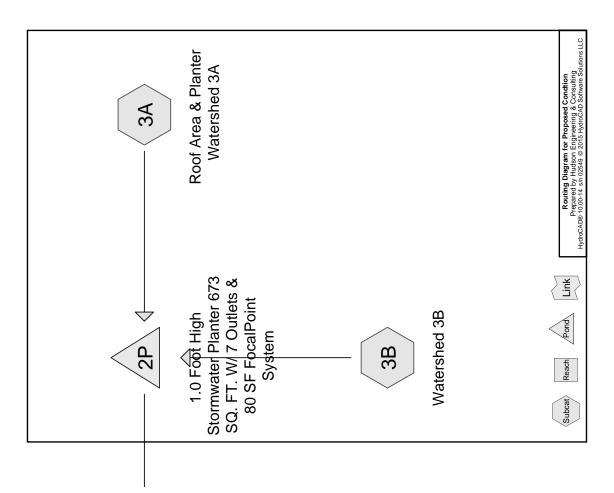
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Primary OutFlow Max=0.03 ds @ 11.59 hrs HW=26.52' TW=22.29' (Dynamic Tailwater)

—1=Culvert (Passes 0.03 ds of 4.74 ds potential flow)

—2=Orifice/Grate (Controls 0.00 ds)

—3=Exfiltration (Exfiltration Controls 0.03 dts)



Type III 24-hr WQv Prop. Roof Rainfall=1.69"

Proposed Condtion

Type III 24-hr
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Summary for Subcatchment 3A: Roof Area & Planter Watershed 3A

1,682 cf, Depth= 1.37" 0.62 cfs @ 12.01 hrs, Volume= II Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr WQv Prop. Roof Rainfall=1.69"

Area (sf) CN Description	Roof	79 Planter	Weighted Average	1.56% Pervious Area	95.44% Impervious Area	To Length Slope Velocity Capacity Description	(T/Sec) (CfS)	Direct Entry,
Des	Roc	Plar	Wei	4.56	92.	> e	₽	
S	86	79	97			Slop		
rea (sf)	14,082	673	14,755	673	14,082	Length	(reet)	
∢	*	*				J C	(min)	1.0

Summary for Subcatchment 3B: Watershed 3B

382 cf, Depth= 1.37" 0.14 cfs @ 12.01 hrs, Volume=

Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr WQv Prop. Roof Rainfall=1.69"

									Ŧ
									P2 = 3.45
									n = 0.011
	74 >75% Grass cover, Good, HSG C				33	Slope Velocity Capacity Description		Sheet Flow, A-B	Smooth surfaces n= 0.011 P2= 3.45"
	s cover, Go		verage	ious Area	96.95% Impervious Area	Capacity	(cts)		
Area (sf) CN Description	.75% Gras	Parking Lot	Neighted Average	3.05% Pervious Area	16.95% Imp	Velocity	(ft/sec)	1.29	
CN	74 >	98 F	97 ۷	(*)	0)	Slope	(ft/ft)	74 0.0180	
rea (sf)	102	3,245	3,347	102	3,245	Tc Length	(feet)	74	
A		*				٦ ۲	(min)	1.0	

ummary for Pond 2P: 1.0 Foot High Stormwater Planter 673 SQ. FT. W/ 7 Outlets & 80 SF FocalPoint Sy:

18,102 sf, 95.72% Impervious, Inflow Depth = 1.37" for WQv Prop. Roof event	2,064 cf	2,065 cf, Atten= 76%, Lag= 0.0 min	2 DRF of
18,102 sf, 95.72% Impervious,	0.76 cfs @ 12.01 hrs, Volume=	0.19 cfs @ 11.75 hrs, Volume=	0.10 ofe @ 11.75 hrs Volumo=
Inflow Area =	lnflow =	Outflow =	Drimon

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 22.05' @ 12.34 hrs Surf.Area= 80 sf Storage= 350 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 8.4 min (788.1 - 779.7)

Type III 24-hr WQv Prop. Roof Rainfall=1.69" Proposed Condition

Type III 24-hr
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	oint	Stormwater Planter (Prismatic) Listed below (Recalc) -Impervious									, Ke= 0.900 -0.0121 // Cc= 0.900		e area	.600
Avail.Storage Storage Description	4.00'W x 20.00'L x 2.25'H FocalPoint 180 cf Overall x 20.0% Voids	rmwater Planter (Prismatic)	541 cf Total Available Storage	re Cum.Store	t) (cubic-feet)	0 0	337	902 202	evices	12.0" Round Culvert	== 19.0' CPP, projecting, no headwall, Ke= 0.900 nlet / Outlet Invert= 19.00' / 18.77' S= 0.0121'' C= 0.900	n= 0.013, Flow Area= 0.79 sf	100.000 in/hr Exfiltration over Surface area	8.0" Horiz. Orifice/Grate X 6.00 C= 0.600 Limited to weir flow at low heads
age Stor	36 cf 4.0 0 180	505 cf Sto	1 cf Tota	Inc.Store	(cubic-feet)		337	168	Invert Outlet Devices	12.0" Rc	L= 19.0' Inlet / Our	n= 0.013,	100.000 i	8.0" Hori
Avail.Stora	36	506	54.	Surf.Area	(sd-ft) (673	673	673	Invert	19.00′			19.33	22.08'
Invert	19.33'	21.58'				8	~	ω.	Routing	Primary			Device 1	Device 1
Volume	#	#5		Elevation	(feet)	21.58	22.08	22.33	Device Routing	#			4	#3

Primary OutFlow Max=0.19 cfs @ 11.75 hrs HW=19.38' TW=19.01' (Dynamic Tailwater)
—1=Culvert (Passes 0.19 cfs of 0.45 cfs potential flow)
—2=Exfiltration (Exfiltration Controls 0.19 cfs)
—3=OrficedGrave (Controls 0.00 cfs)

9.) AquaSwirl Sizing Chart & Spec Sheet



Aqua-Swirl® Stormwater Treatment System

Inspection and Maintenance Manual



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rione: (423) 870-8888 Fax: (423) 826-2112

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March 2014

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www.aquashieldinc.com



AquaShield™, Inc Stormwater Treatment Solutions

The highest priority of AquaShieldTM, Inc. (AquaShieldTM) is to protect waterways by providing stormwater treatment solutions to businesses across the world. These solutions have a reliable foundation based on over 20 years of water treatment experience.

Local regulators, engineers, and contractors have praised the AquaShield™ systems for their simple design and ease of installation. All the systems are fabricated from high performance, durable and lightweight materials. Contractors prefer the quick and simple installation of our structures that saves them money.

The patented line of AquaShieldTM stormwater treatment products that provide high levels of stormwater treatment include the following:

- Aqua-Swirl® Stormwater Treatment System: hydrodynamic separator, which provides a highly effective means for the removal of sediment, floating debris and free-oil.
- Aqua-FilterTM Stormwater Filtration System: treatment train stormwater filtration system capable of removing gross contaminants, fine sediments, waterborne hydrocarbons, heavy metals and total phosphorous.



Aqua-Swirl® Stormwater Treatment System



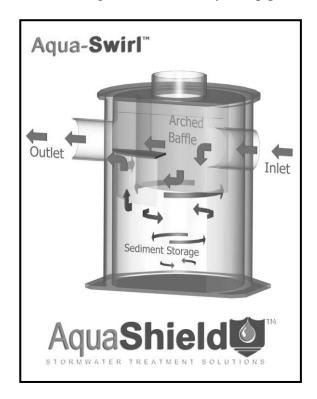
Aqua-Filter™ Stormwater Filtration System



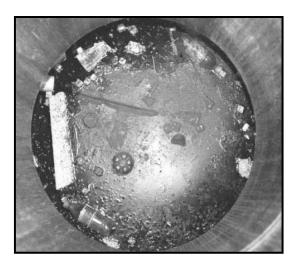
Aqua-Swirl® Stormwater Treatment System

The patented Aqua-Swirl® Stormwater Treatment System is a single chamber hydrodynamic separator which provides a highly effective means for the removal of sediment, free oil, and floating debris. Both treatment and storage are accomplished in the swirl chamber without the use of multiple or "blind" chambers. Independent laboratory and field performance verifications have shown that the Aqua-Swirl® achieves over 80% suspended solids removal efficiency on a net annual basis.

The Aqua-Swirl® is most commonly installed in an "off-line" configuration. Or, depending on local regulations, an "in-line" (on-line) conveyance flow diversion (CFD) system can be used. The CFD model allows simple installation by connecting directly to the existing storm conveyance pipe thereby providing full treatment of the "first flush," while the peak design storm is diverted and channeled through the main conveyance pipe.



The patented Aqua-Swirl® Stormwater Treatment System provides a highly effective means for the removal of sediment, floating debris, and free oil. Swirl technology, or vortex separation, is a proven form of treatment utilized in the stormwater industry to accelerate gravitational separation.



Floatable debris in the Aqua-Swirl®

Each Aqua-Swirl[®] is constructed of high performance, lightweight and durable materials including polymer coated steel (PCS), high density polyethylene (HDPE), or fiberglass reinforced polymer (FRP). These materials eliminate the need for heavy lifting equipment during installation.



System Operation

The treatment operation begins when stormwater enters the Aqua-Swirl® through a tangential inlet pipe that produces a circular (or vortex) flow pattern that causes contaminates to settle to the base of the unit. Since stormwater flow is intermittent by nature, the Aqua-Swirl® retains water between storm events providing both dynamic and quiescent settling of solids. The dynamic settling occurs during each storm event while the quiescent settling takes place between successive storms. A combination of gravitational and hydrodynamic drag forces encourages the solids to drop out of the flow and migrate to the center of the chamber where velocities are the lowest.

The treated flow then exits the Aqua-Swirl® behind the arched outer baffle. The top of the baffle is sealed across the treatment channel, thereby eliminating floatable pollutants from escaping the system. A vent pipe is extended up the riser to expose the backside of the baffle to atmospheric conditions, preventing a siphon from forming at the bottom of the baffle.



Custom Applications

The Aqua-Swirl® system can be modified to fit a variety of purposes in the field, and the angles for inlet and outlet lines can be modified to fit most applications. The photo below demonstrates the flexibility of Aqua-Swirl® installations using a "twin" configuration in order to double the

water quality treatment capacity. Two Aqua-Swirl® units were placed side by side in order to treat a high volume of water while occupying a small amount of space.



Custom designed AS-9 Twin Aqua-Swirl®



Retrofit Applications

The Aqua-Swirl[®] system is designed so that it can easily be used for retrofit applications. With the invert of the inlet and outlet pipe at the same elevation, the Aqua-Swirl[®] can easily be connected directly to the existing storm conveyance drainage system. Furthermore, because of the lightweight nature and small footprint of the Aqua-Swirl[®], existing infrastructure utilities (i.e., wires, poles, trees) would be unaffected by installation.



The long term performance of any stormwater treatment structure, including manufactured or land based systems, depends on a consistent maintenance plan. Inspection and maintenance functions are simple and easy for the AquaShieldTM Stormwater Treatment Systems allowing all inspections to be performed from the surface.

It is important that a routine inspection and maintenance program be established for each unit based on: (a) the volume or load of the contaminants of concern, (b) the frequency of releases of contaminants at the facility or location, and (c) the nature of the area being drained.

In order to ensure that our systems are being maintained properly, AquaShieldTM offers a maintenance solution to all of our customers. We will arrange to have maintenance performed.





Inspection

All AquaShieldTM products can be inspected from the surface, eliminating the need to enter the systems to determine when cleanout should be performed. In most cases, AquaShieldTM recommends a quarterly inspection for the first year of operation to develop an appropriate schedule of maintenance. Based on experience of the system's first year in operation, we recommend that the inspection schedule be revised to reflect the site-specific conditions encountered. Typically, the inspection schedule for subsequent years is reduced to semi-annual inspection.



Aqua-Swirl® Maintenance

The Aqua-Swirl® has been designed to minimize and simplify the inspection and maintenance process. The single chamber system can be inspected and maintained entirely from the surface thereby eliminating the need for confined space entry. Furthermore, the entire structure (specifically, the floor) is accessible for visual inspection from the surface. There are no areas of the structure that are blocked from visual inspection or periodic cleaning. Inspection of any free-floating oil and floatable debris can be directly observed and maintained through the manhole access provided directly over the swirl chamber.

Aqua-Swirl® Inspection Procedure

To inspect the Aqua-Swirl®, a hook is needed to remove the manhole cover. AquaShieldTM provides a customized manhole cover with our distinctive logo to make it easy for maintenance crews to locate the system in the field. We also provide a permanent metal information plate

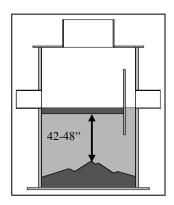
affixed inside the access riser which provides our contact information, the Aqua-Swirl® model size, and serial number.

The only tools needed to inspect the Aqua-Swirl® system are a flashlight and a measuring device such as a stadia rod or pole. Given the easy and direct accessibility provided, floating oil and debris can be observed directly from the surface. Sediment depths can easily be determined by lowering a measuring device to the top of the sediment pile and to the surface of the water.

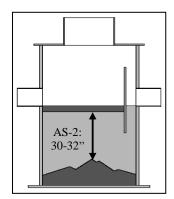


Sediment inspection using a stadia rod in a single chamber

The maintenance trigger for Aqua-Swirl® Models AS-3 through AS-13 occurs when the sediment pile is within 42 to 48 inches of the standing water surface. For the Aqua-Swirl® Model AS-2, maintenance is needed when the top of the sediment pile is measured to be 30 to 32 inches below the standing water surface.



Maintenance trigger for Aqua-Swirt® Models AS-3 through AS-13 occurs when sediment pile is 42-48 inches below water surface.



Maintenance trigger for Aqua-Swirl® Model AS-2 occurs when sediment pile is 30 to 32 inches below water surface.

It should be noted that in order to avoid underestimating the volume of sediment in the chamber, the measuring device must be carefully lowered to the *top* of the sediment pile. Keep in mind that the finer sediment at the top of the pile may offer less resistance to the measuring device than the larger particles which typically occur deeper within the sediment pile.

The Aqua-Swirl[®] design allows for the sediment to accumulate in a semi-conical fashion as illustrated above. That is, the depth to sediment as measured below the water surface may be less in the center of the swirl chamber; and likewise, may be greater at the edges of the swirl chamber.

Aqua-Swirl® Cleanout Procedure

Cleaning the Aqua-Swirl® is simple and quick. Free-floating oil and floatable debris can be observed and removed directly through the 30-inch service access riser provided. A vacuum truck is typically used to remove the accumulated sediment and debris. An advantage of the Aqua-Swirl® design is that the entire sediment storage area can be reached with a vacuum hose from the surface (reaching all the sides). Since there are no multiple or limited (hidden or "blind") chambers in the Aqua-Swirl®, there are no restrictions to impede on-site maintenance tasks.

Disposal of Recovered Materials

Disposal of recovered material is typically handled in the same fashion as catch basin cleanouts. AquaShieldTM recommends that all maintenance activities be performed in accordance with appropriate health and safety practices for the tasks and equipment being used.

AquaShieldTM also recommends that all materials removed from the Aqua-Swirl[®] and any external structures (e.g, bypass features) be handled and disposed in full accordance with any applicable local and state requirements.



Vacuum truck quickly cleans the Aqua-Swirl® from a single chamber

Aqua-Swirl® Inspection and Maintenance Work Sheets on following pages

Aqua-Swirl® Inspection and Maintenance Manual Work Sheets

	SITE and OWNER INFORMATION
Site Name:	
Site Location:	
Date:	Time:
Inspector Name:	
Inspector Company:	Phone #:
Owner Name:	
Owner Address:	
Owner Phone #:	Emergency Phone #:
	INSPECTIONS

I. Floatable Debris and Oil

- 1. Remove manhole lid to expose liquid surface of the Aqua-Swirl®.
- 2. Remove floatable debris with basket or net if any present.
- 3. If oil is present, measure its depth. Clean liquids from system if one half $(\frac{1}{2})$ inch or more oil is present.

Note: Water in Aqua-Swirl® can appear black and similar to oil due to the dark body of the surrounding structure. Oil may appear darker than water in the system and is usually accompanied by oil stained debris (e.g. Styrofoam, etc.). The depth of oil can be measured with an oil/water interface probe, a stadia rod with water finding paste, a coliwasa, or collect a representative sample with a jar attached to a rod.

II. Sediment Accumulation

- 1. Lower measuring device (e.g. stadia rod) into swirl chamber through service access provided until top of sediment pile is reached.
- 2. Record distance to top of sediment pile from top of standing water: inches
- 3. For Aqua-Swirl® Models AS-3 through AS-13, schedule cleaning if value in Step #2 is 48 to 42 inches or less.
- 4. For Aqua-Swirl® Model AS-2, schedule cleaning if value in Step #2 is 32 to 30 inches or less.

III. Diversion Structures (External Bypass Features)

If a diversion (external bypass) configuration is present, it should be inspected as follows:

- 1. Inspect weir or other bypass feature for structural decay or damage. Weirs are more susceptible to damage than off-set piping and should be checked to confirm that they are not crumbling (concrete or brick) or decaying (steel).
- 2. Inspect diversion structure and bypass piping for signs of structural damage or blockage from debris or sediment accumulation.
- 3. When feasible, measure elevations on diversion weir or piping to ensure it is consistent with site plan designs.
- 4. Inspect downstream (convergence) structure(s) for sign of blockage or structural failure as noted above.

CLEANING

Schedule cleaning with local vactor company or AquaShieldTM to remove sediment, oil and other floatable pollutants. The captured material generally does not require special treatment or handling for disposal. Site-specific conditions or the presence of known contaminants may necessitate that appropriate actions be taken to clean and dispose of materials captured and retained by the Aqua-Swirl[®]. All cleaning activities should be performed in accordance with property health and safety procedures.

AquaShieldTM always recommends that all materials removed from the Aqua-Swirl[®] during the maintenance process be handled and disposed in accordance with local and state environmental or other regulatory requirements.

MAINTENANCE SCHEDULE

I. During Construction

Inspect the Aqua-Swirl® every three (3) months and clean the system as needed. The Aqua-Swirl® should be inspected and cleaned at the end of construction regardless of whether it has reached its maintenance trigger.

II. First Year Post-Construction

Inspect the Aqua-Swirl® every three (3) months and clean the system as needed.

Inspect and clean the system once annually regardless of whether it has reached its sediment or floatable pollutant storage capacity.

III. Second and Subsequent Years Post-Construction

If the Aqua-Swirl® did not reach full sediment or floatable pollutant capacity in the First Year Post-Construction period, the system can be inspected and cleaned once annually.

If the Aqua-Swirl® reached full sediment or floatable pollutant capacity in less than 12 months in the First Year Post-Construction period, the system should be inspected once

every six (6) months and cleaned as needed. The Aqua-Swirl® should be cleaned annually regardless of whether it reaches its sediment or floatable pollutant capacity.

IV. Bypass Structures

Bypass structures should be inspected whenever the Aqua-Swirl[®] is inspected. Maintenance should be performed on bypass structures as needed.

	MAINT	TENANCE COMP	ANY INFORM	IATION
Company Name:				
Street Address:				
City:		State	e/Prov.:	Zip/Postal Code:
Contact:				Title:
Office Phone:			Cell Phone:	_
		ACTIVIT	Y LOG	
Date of Cleaning:			(Next inspections) (Next inspection)	ction should be 3 months from first year).
Time of Cleaning:	Start: _		End:	
Date of Next Inspectio	n: _		<u>—</u>	
Floatable debris presen	it:	Yes No		
Notes:				
Oil present: Yes Measurement n		1 `		
ST	RUCTU	RAL CONDITION	NS and OBSE	RVATIONS
Structural damage:	Yes 1	No Where:		

Structural wear:	Yes	No	Where:							
Odors present: Yes No			Describe:							
Clogging: Yes	No	Desc	ribe:							
Other Observations	:									
			NOTES							
Additional Co	omment	s and/o	or Actions To Be Taken	Time Frame						

ATTACHMENTS

- Attach site plan showing Aqua-Swirl® location.
- Attach detail drawing showing Aqua-Swirl® dimensions and model number.
- If a diversion configuration is used, attach details showing basic design and elevations (where feasible).

Aqua-Swirl®

TABULAR MAINTENANCE SCHEDULE
Date Construction Started:
Date Construction Ended:

During Construction

	Month											
Activity	1	2	3	4	5	6	7	8	9	10	11	12
Inspect and Clean as needed			X			X			X			X
Inspect Bypass and maintain as needed			X			X			X			X
Clean System*												X*

^{*} The Aqua-Swirl® should be cleaned <u>once a year</u> regardless of whether it has reached full pollutant storage capacity. In addition, the system should be cleaned at the <u>end of construction</u> regardless of whether it has reach full pollutant storage capacity.

First Year Post-Construction

	Month											
Activity	1	2	3	4	5	6	7	8	9	10	11	12
Inspect and Clean as needed			X			X			X			X
Inspect Bypass and maintain as needed			X			X			X			X
Clean System*												X*

^{*} The Aqua-Swirl® should be cleaned <u>once a year</u> regardless of whether it has reached full pollutant storage capacity.

Second and Subsequent Years Post-Construction

	Month											
Activity	1	2	3	4	5	6	7	8	9	10	11	12
Inspect and Clean as needed												X*
Inspect Bypass, maintain as needed												X*
Clean System*											·	X*

^{*} If the Aqua-Swirl® did <u>not</u> reach full sediment or floatable pollutant capacity in the First Year Post-Construction period, the system can be inspected and cleaned once annually.

If the Aqua-Swirl® <u>reached</u> full sediment or floatable pollutant capacity in less than 12 months in the First Year Post-Construction period, the system should be inspected once every six (6) months or more frequently if past history warrants, and cleaned as needed. The Aqua-Swirl® should be cleaned annually regardless of whether it reaches its full sediment or floatable pollutant capacity.

Aqua-Swirl™ Model	Swirl Chamber Diameter	Maximum Stub-Out Pipe Outer Diameter		Water Quality Treatment Flow ²	Oil/Debris Storage Capacity	Sediment Storage Capacity
	(ft.)		1.)	(cfs)	(gal)	(ft³)
AS-2	2.50	On/Offline 8	CFD ¹ 12	1.1	37	10
AS-3	3.25	10	16	1.8	110	20
AS-4	4.25	12	18	3.2	190	32
AS-5	5.00	12	24	4.4	270	45
AS-6	6.00	14	30	6.3	390	65
AS-7	7.00	16	36	8.6	540	90
AS-8	8.00	18	42	11.2	710	115
AS-9	9.00	20	48	14.2	910	145
AS-10	10.0	22	54	17.5	1130	180
AS-12	12.0	24	48	25.2	1698	270
AS-XX	Custom			>26		

^{*}Higher water quality treatment flow rates can be designed with multiple swirls.

- 1) The **Aqua-Swir**[™] **Conveyance Flow Diversion (CFD)** provides full treatment of the "first flush," while the peak design storm is diverted and channeled through the main conveyance pipe. Please refer to your local representative for more information.
- 2) Many regulatory agencies are establishing "water quality treatment flow rates" for their areas based on the initial movement of pollutants into the storm drainage system. The treatment flow rate of the Aqua-Swirl™ system is engineered to meet or exceed the local water quality treatment criteria. This "water quality treatment flow rate" typically represents approximately 90% to 95% of the total annual runoff volume.

The design and orientation of the Aqua-Filter™ generally entails some degree of customization. For assistance in design and specific sizing using historical rainfall data, please refer to an AquaShield™ representative or visit our website at www.AquaShieldInc.com. CAD details and specifications are available upon request.

10.)	FocalPoint Biofilter System	

Hudson Engineering & Consulting, P.C.





Designing with FocalPoint in New York

Utilizing a High Performance Modular Biofiltration System for New Development, Redevelopment and Retrofit Projects

The New York State Department of Environmental Conservation (NYS DEC) has approved the FocalPoint (High Performance Modular Biofiltration System) as a proprietary stormwater management practice for use on New Development, Redevelopment and Retrofit Projects.

SYSTEM OVERVIEW:

The FocalPoint is an ultra-efficient, modular biofiltration system that treats and drains large volumes of stormwater runoff in a small footprint to meet post construction stormwater treatment requirements. The system can be installed along the edge of a roadway behind curb line, in landscaped stormwater basins and be incorporated into an urban green infrastructure streetscape. As an innovative micro-scale practice, the FocalPoint overcomes many of the inherent challenges with traditional micro-bioretention and other similar BMPs – improving media quality control, reduction in space needed and reduced maintenance footprint, and elimination of clog-prone geotextiles.

SYSTEM COMPONENTS:

Vegetated System:

Plants process pollutants removed from run-off and root system maintains drainage and aeration of media.

3" Layer of Shredded • Hardwood Mulch:

Pre-treatment mechanism.
Removal and Replacement of Mulch
Represents the Bulk of System
Maintenance!

6" Bridging Stone & Separation Layer:

Clog-Proof Clean Stone & Micro-Mesh Replace Traditional Geotextile Layer No geotextile = no clogging

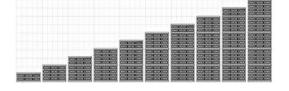
18" High Performance Media:

Flows at 100" Per Hour / 200 ft per day Resistant to Clogging

3rd Party Field and Lab Test Verified for 91% TSS, 66% P and 48% N

High Performance Underdrain:

9.45" Modular Tank, or "Flat Pipe" w/95% Open Surface Collects Water Efficiently. Expand into Modular Tanks for Larger Storage Needs.

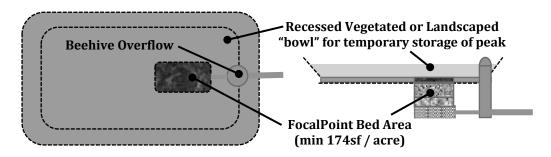




SIZING SUMMARY:

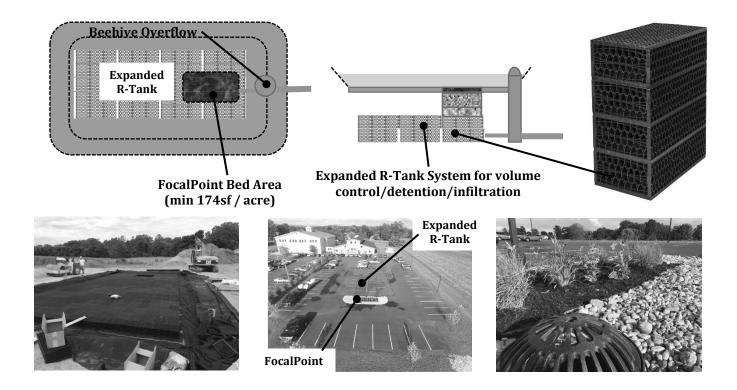
Water Quality (WQ) Treatment Only projects:

- The surface area of the FocalPoint media bed must be a minimum of **174 square feet per 1** acre of impervious area
- The system must also be modelled in HydroCAD (or similar TR-55 modelling software) to demonstrate that the entire volume of a Type II or Type III (depending on region) 24 hr storm is treated prior to activation of the bypass/overflow (typically set at 6-12" above the mulch surface). Note: a 1.20 to 1.50 inch rainfall event typically generates 1.0 inches of runoff depending on watershed characteristics



Managing Larger Storms (with expanded infiltration or detention):

The R-Tank modular underdrain at the bottom of the FocalPoint gives the designer the opportunity to satisfy both WQv, Channel Protection, Recharge and Detention for controlled release of major storm events all within one system. The R-Tank can be expanded both vertically and horizontally to meet the volume/storage goals to ensure runoff is not only treated by the FocalPoint but also achieves post development peak flowrate control. The benefit to designers is that the R-Tank portion of the system can be built under parking areas (H-20, HS-25 load rated) to improve site surface utilization.



Site Development Project Examples:



























ACCESSORY ITEMS TO CONSIDER:

Rain Guardian Turret/Foxhole Curbline precast pretreatment unit for collection of sediment and energy dissipation.







ACF Beehive Overflow Filter

Domed riser with geotextile insert for collection of gross solids during major storm events.

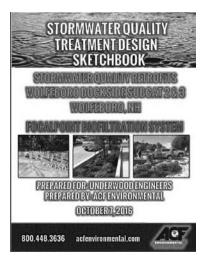




DESIGN SUPPORT:

ACF and Fabco's in house engineering support team provide site specific technical support to engineers, designers, landscape architects and contractors. ACF realizes that engineers today are working on several projects at one time and are always working against low engineering design budgets. The intent of our technical support is to not only provide you with product information but to work alongside you and develop solutions to your site development design challenges.

We offer site specific design computations and conceptual layout support at no charge which we typically bind up with all relevant attachments in a design "Sketchbook" - a helpful tool that ultimately brings value and saves you time and associated cost as you work through incorporating this innovative solution into your design plans.



CONTACT ACF ENVIRONMENTAL:

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FocalPoint

BIOFILTRATION SYSTEMS

HIGH PERFORMANCE MODULAR BIOFILTRATION SYSTEM (HPMBS)
Operations & Maintenance





GENERAL DESCRIPTION

The following general specifications describe the general operations and maintenance requirements for the FocalPoint® High Performance Modular Biofiltration System (HPMBS). The system utilizes physical, chemical and biological mechanisms of a soil, plant and microbe complex to remove pollutants typically found in urban stormwater runoff. The treatment system is a fully equipped, modular, constructed in place system designed to treat contaminated runoff.

Stormwater enters the FocalPoint® HPMBS, is filtered by the High Flow Biofiltration Media and passes through to the underdrain/storage system where the treated water is detained, retained or infiltrated to sub-soils, prior to discharge to the storm sewer system of any remaining flow.

Higher flows bypass the FocalPoint® HPMBS via a downstream inlet or other overflow conveyance. Maintenance is a simple, inexpensive and safe operation that does not require confined space entry, pumping or vacuum equipment, or specialized tools. Properly trained landscape personnel can effectively maintain FocalPoint® HPMBS by following instructions in this manual.



BASIC OPERATIONS

FocalPoint® is a modular, high performance biofiltration system that often works in tandem with other integrated management practices (IMP). Contaminated stormwater runoff enters the biofiltration bed through a conveyance swale, planter box, or directly through a curb cut or false inlet. Energy is dissipated by a rock or vegetative dissipation device and is absorbed by a 3-inch layer of aged, double shredded hardwood mulch, with fines removed, (when specified) on the surface of the biofiltration media.

As the water passes through the mulch layer, most of the larger sediment particles and heavy metals are removed through sedimentation and chemical reactions with the organic material in the mulch. Water passes through the biofiltration media where the finer particles are removed and numerous chemical reactions take place to immobilize and capture pollutants in the soil media.

The cleansed water passes into the underdrain/storage system and remaining flows are directed to a storm sewer system or other appropriate discharge point. Once the pollutants are in the soil, bacteria begin to break down and metabolize the materials and the plants begin to uptake and metabolize the pollutants. Some pollutants such as heavy metals, which are chemically bound to organic particles in the mulch, are released over time as the organic matter decomposes to release the metals to the feeder roots of the plants and the cells of the bacteria in the soil where they remain and are recycled. Other pollutants such as phosphorus are chemically bound to the soil particles and released slowly back to the plants and bacteria and used in their metabolic processes. Nitrogen goes through a variety of very complex biochemical processes where it can ultimately end up in the plant/bacteria biomass, turned to nitrogen gas or dissolves back into the water column as nitrates depending on soil temperature, pH and the availability of oxygen. The pollutants ultimately are retained in the mulch, soil and biomass with some passing out of the system into the air or back into the water.

DESIGN AND INSTALLATION

Each project presents different scopes for the use of FocalPoint® HPMBS. To ensure the safe and specified function of this stormwater BMP, Convergent Water Technologies and/or its Value Added Resellers (VAR) review each application before supply. Information and design assistance is available to the design engineer during the planning process. Correct FocalPoint® sizing is essential to optimum performance. The engineer shall submit calculations for approval by the local jurisdiction when required. The contractor and/or VAR is responsible for the correct installation of FocalPoint® HPMBS units as described in approved plans. A comprehensive installation manual is available at www.convergentwater.com.







MAINTENANCE

Why Maintain?

All stormwater treatment systems require maintenance for effective operation. This necessity is often incorporated in your property's permitting process as a legally binding BMP maintenance agreement. Other reasons for maintenance include:

- Avoid legal challenges from your jurisdiction's maintenance enforcement program.
- Prolong the lifespan of your FocalPoint® HPMBS.
- Avoid costly repairs.
- Help reduce pollutant loads leaving your property.

Simple maintenance of the FocalPoint® HPMBS is required to continue effective pollutant removal from stormwater runoff before any discharge into downstream waters. This procedure will also extend the longevity of the living biofiltration system. The unit will recycle and accumulate pollutants within the biomass, but may also subjected to other materials entering the surface of the system. This may include trash, silt and leaves etc. which will be contained above the mulch and/or biofiltration media layer. Too much silt may inhibit the FocalPoint's® HPMBS flow rate, which is a primary reason for system maintenance. Removal of accumulated silt/sediment and/or replacement of the mulch layer (when specified), is an important activity that prevents over accumulation of such silt/sediment.

When to Maintain?

Convergent Water Technologies and/or its VAR includes a 1-year maintenance plan with each system purchased. Annual included maintenance consists of two (2) scheduled maintenance visits. Additional maintenance may be necessary depending on sediment and trash loading (by Owner or at additional cost). The start of the maintenance plan begins when the system is activated for full operation. Full operation is defined as when the site is appropriately stabilized, the unit is installed and activated (by VAR), i.e., when mulch (if specified) and plantings are added.

Activation should be avoided until the site is fully stabilized (full landscaping, grass cover, final paving and street sweeping completed). Maintenance visits are scheduled seasonally; the spring visit aims to clean up after winter loads including salts and sands. The fall visit helps the system by removing excessive leaf litter.

A first inspection to determine if maintenance is necessary should be performed at least twice annually after storm events of greater than (1) one inch total depth (subject to regional climate). Please refer to the maintenance checklist for specific conditions that indicate if maintenance is necessary.

It has been found that in regions which receive between 30-50 inches of annual rainfall, (2) two visits are generally required. Regions with less rainfall often only require (1) one visit per annum. Varying land uses can affect maintenance frequency.





Some sites may be subjected to extreme sediment or trash loads, requiring more frequent maintenance visits. This is the reason for detailed notes of maintenance actions per unit, helping the VAR/Maintenance contractor and Owner predict future maintenance frequencies, reflecting individual site conditions.

Owners must promptly notify the VAR/Maintenance contractor of any damage to the plant(s), which constitute(s) an integral part of the biofiltration technology. Owners should also advise other landscape or maintenance contractors to leave all maintenance of the FocalPoint® HPMBS to the VAR/Maintenance contractor (i.e. no pruning or fertilizing).

EXCLUSION OF SERVICES

It is the responsibility of the owner to provide adequate irrigation when necessary to the plant(s) in the FocalPoint® HPMRS.

Clean up due to major contamination such as oils, chemicals, toxic spills, etc. will result in additional costs and are not covered under the VAR/Maintenance contractor maintenance contract. Should a major contamination event occur, the Owner must block off the outlet pipe of the FocalPoint® (where the cleaned runoff drains to, such as drop-inlet) and block off the point where water enters of the FocalPoint® HPMBS. The VAR/Maintenance contractor should be informed immediately.

MAINTENANCE VISIT SUMMARY

Each maintenance visit consists of the following simple tasks (detailed instructions below).

- 1. Inspection of FocalPoint® HPMBS and surrounding area
- 2. Removal of debris, trash and mulch
- 3. Mulch replacement
- 4. Plant health evaluation (including measurements) and pruning or replacement as necessary
- 5. Clean area around FocalPoint® HPMBS
- 6. Complete paperwork, including date stamped photos of the tasks listed above.

MAINTENANCE TOOLS, SAFETY EQUIPMENT AND SUPPLIES

Ideal tools include: camera, bucket, shovel, broom, pruners, hoe/rake, and tape measure. Appropriate Personal Protective Equipment (PPE) should be used in accordance with local or company procedures. This may include impervious gloves where the type of trash is unknown, high visibility clothing and barricades when working in close proximity to traffic and also safety hats and shoes.



MAINTENANCE VISIT PROCEDURE



Inspection of FocalPoint® HPMBS and s	surrounding are	ea	
Record individual unit before mainte in this document) the following:	nance with pho	otograph (numbered). Record on Maint	enance Report (see example
Standing Water	yes no	□ Damage to HPMBS System	yes no
─── Is Bypass Inlet Clear?	yes no	to Overflow conveyance	yes no
Removal of Silt / Sediment / Clay			
Dig out silt (if any) and mulch and re	move trash & fo	oreign items.	
Silt / Clay Found? Cups / Bags Found?	yes no yes no		yes no d (volume or weight)
Removal of debris, trash and mulch			
the flow line elevation of the adjace (typ. 6" - 12"), add media (not top so	nt overflow con I or other) to re ow line of overfl	te from the top of the FocalPoint® HPM inveyance. If this distance is greater that charge to the distance specified. How conveyance (inches)	3
# Of Buckets of Media Added			
Mulch Replacement			
mulch with fines removed. For small and for larger projects, one cubic ya	er projects, one rd of mulch will	nulch (if utilized) which must be, aged, e cubic foot of mulch will cover four squ l cover 108 square feet of biofiltration bia ia available from the VAR/Contractor.	uare feet of biofiltration bed,
biofiltration media bed to a dep	oth of 3". rom energy disa	which has been screened to remove fi	,
Plant health evaluation and pruning o	replacement a	as necessary	
Examine the plant's health and repla Prune as necessary to encourage gro			
Height above Grate (feet) Width at Widest point (feet)		Health Damage to Plant	alive dead yes no
Clean area around FocalPoint® HPMBS	_		
Clean area around unit and ren	nove all refuse to	o be disposed of appropriately.	
Complete paperwork			
Deliver Maintenance Report an Some jurisdictions may require It is the responsibility of the Ow	submission of r	maintenance reports in accordance wi	th approvals.



FocalPoint Warranty

Seller warrants goods sold hereunder against defects in materials and workmanship only, for a period of (1) year from date the Seller activates the system into service. Seller makes no other warranties, express or implied.

Seller's liability hereunder shall be conditioned upon the Buyer's installation, maintenance, and service of the goods in strict compliance with the written instructions and specifications provided by the Seller. Any deviation from Seller's instructions and specifications or any abuse or neglect shall void warranties.

In the event of any claim upon Seller's warranty, the burden shall be upon the Buyer to prove strict compliance with all instructions and specifications provided by the Seller.

Seller's liability hereunder shall be limited only to the cost or replacement of the goods. Buyer agrees that Seller shall not be liable for any consequential losses arising from the purchase, installation, and/or use of the goods.



Maintenance Checklist

Element	Problem	What To Check	Should Exist	Action
Inlet	Excessive sediment or trash accumulation	Accumulation of sediment or trash impair free flow of water into FocalPoint	Inlet free of obstructions allowing free flow into FocalPoint System	Sediments or trash should be removed
Mulch Cover	Trash and floatable debris accumulation	Excessive trash or debris accumulation.	Minimal trash or other debris on mulch cover	Trash and debris should be removed and mulch cover raked level. Ensure that bark nugget
Mulch Cover	Ponding of water on mulch cover	Ponding in unit could be indicative of clogging due to excessive fine sediment accumulation or spill of petroleum oils	Stormwater should drain freely and evenly over mulch cover.	Contact VAR for advice.
Plants	Plants not growing, or in poor condition	Soil/mulch too wet, evidence of spill. Pest infestation. Vandalism to plants.	Plants should be healthy and pest free.	Contact VAR for advice.
Plants	Plant growth excessive	Plants should be appropriate to the species and location of FocalPoint		Trim/prune plants in accordance with typical landscaping and



















Is your stormwater detention system taking up too much space? Bring it down to size with the R-Tank System, the most efficient and versatile underground stormwater storage system available today. Whether you need to reduce your system footprint to resolve a utility conflict or free up space for a future expansion, R-Tank will give you the smallest footprint, provide more options for vehicular loading and cover depths, and deliver more installation versatility than any other system around.



The R-Tank System includes five different module configurations, providing system height options from 2" to over 7' tall. And it delivers support for HS-20 and HS-25 traffic with cover depths from 6" all the way up to over 16'. Whether you're designing a project at the beach with minimal depth over the water table, or a deep system in the hills, R-Tank has you covered.

With an unlimited array of system footprints and configurations, R-Tank solves tough stormwater problems by perfectly adapting to the needs of your site. Give R-Tank a shot on your next project, and prepare to be impressed.



BENEFITS

High Capacity

• 95% void internal area

Strength

- Easily supports traffic loading from parking lots and roads
- Module options for HS-20 and HS-25 rating with cover depths from 6 inches to 16 feet

Design & Construction Versatility

- Combine modules into any shape to efficiently use space
- Vary height from 2 inches to 7 feet

Increased Infiltration and Exfiltration

- Outer shell is 90% open
- Increases groundwater recharge, reducing postconstruction discharge volumes

Easy to Transport

• Can be supplied unassembled for reduced delivery costs

Lightweight and Quick to Install

- Installed by hand; no cranes required
- Reduces site access delays

Recycled Content

Manufactured with recycled polypropylene





- Light Duty module (30 psi)
- Ideal for applications in green space
- Not rated for vehicular traffic
- 12" Minimum cover, 36" maximum cover
- Four internal plates



- Heavy Duty module (33.4 psi)
- Standard module for HS-20 traffic applications
- 20" Minimum cover, 84" Maximum cover
- Five internal plates





- Super Duty module (42.9 psi)
- Higher safety factors for shallow traffic applications and deeper cover
- 18" Minimum cover, 120" Maximum cover
- Five internal plates





- Ultra Duty module (134.2 psi)
- Traffic loads with 12" of cover
- Available from 14" 66" tall
- Ideal for high water table sites





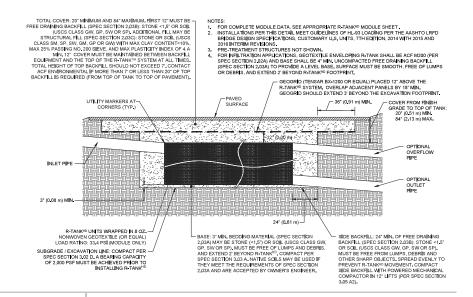
- Extreme Duty module (320 psi)
- Traffic loads with 6" cover
- 16.5' maximum cover
- Available from 2" 10' tall
- 90% void



DESIGN CONSIDERATIONS

Many factors will influence the design of the R-Tank® system. While this list is not intended to be all-inclusive, several design considerations are worth highlighting:

- 1. PRE-TREATMENT
- 2. BACKFILL MATERIALS
- 3. RUNOFF REDUCTION
- 4. WATER TABLE
- 5. CONSTRUCTION LOADS
- 6. LATERAL LOADS
- 7. R-TANK® MODULES
- 8. LOAD MODELING



1. PRE-TREATMENT

Removing pollutants from runoff before they enter an underground detention system is the only smart way to design & build a system. The best way to do that is with the Trash Guard Plus® (see page 6), but many other ways exist. Be sure the system you select will remove:

- Heavy Sediments
- Gross Pollutants (trash)
- Biodegradable Debris

2. BACKFILL MATERIALS

Backfill materials should be stone (smaller than 1.5" in diameter) or soil (GW, GP SW or SP as classified by the Unified Soil Classification System). Material must be free from lumps, debris and any sharp objects that could cut the geotextile. See the R-Tank® narrative specification section 2.03 for additional information.

3. RUNOFF REDUCTION

Most designs incorporate an outlet to drain the system at a controlled rate and/or an overflow to prevent flooding in extreme events. But be sure to take advantage of any infiltration you can achieve on the site. Consider raising the invert of your outlet or creating a sump to capture and infiltrate the water quality volume whenever possible.

4. WATER TABLE

While installing the R-Tank® below the water table is manageable, designers must be able to create a stable base and account for the system's ability to drain this water out or limit its ability to enter the system. If a liner is used to prevent ground water from entering the system, measures must be taken to prevent the system from floating.

5. CONSTRUCTION LOADS

Construction loads are often the heaviest loads the system will see throughout its life. Care must be taken during backfilling and compaction using the proper equipment (see specification section 3.05), and post-installation construction traffic should be routed around the system (Installation Guide step 12).

6. LATERAL LOADS

As systems get deeper, the loads acting on the sides of the tank increase. While vertical loads often control the design, be sure to consider lateral loading, as well.

7. R-TANK MODULES

Be sure to select the right module for your application. See the information on page 3 for more details on which module is the best fit. Also refer to the specifications for each module on the back of this brochure, or call us for assistance.

8. LOAD MODELING

A safety factor of 1.75 or higher is required when designing an R-Tank System using the AASHTO LRFD Bridge Design Specifications. Be sure to run your own loading model with all requirements specific to your site. Several example models can be found in our Tech Note on loading capabilities, and minimum cover requirements for various loads can be found in the spec on the back of this brochure.

LOW IMPACT DESIGN AND GREEN INFRASTRUCTURE

As much of the nation's Gray Infrastructure continues to decay, new concepts for a better way to rebuild it are emerging through Green Infrastructure (GI) and Low Impact Development (LID). This type of reconstruction moves beyond traditional systems that do ONE THING very well to systems that accomplish MULTIPLE objectives simultaneously. ACF has several technologies that dovetail with the goals of LID and GI that can play a significant role in the redevelopment process.



R-TANK®

Pipe and stone are used in traditional systems to move and store runoff. R-Tank does the same job, but with several additional benefits.

- Stores and moves runoff
- Open system encourages infiltration
- Stores 138% more water than stone
- Easily handles traffic loads beneath sidewalks and streets
- Ships flat to reduce site disturbance

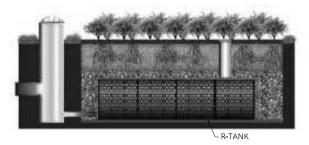
- Moves water slowly, increasing time of concentration
- Fully accessible for maintenance
- Maximizes storage potential of GI practices like bioretention, street tree pits, etc.



FOCALPOINT

Traditional landscaping adds aesthetic value to projects, but has more potential. Many developers turn to bioretention, but are forced to surrender massive land areas and dedicate significant future funds to maintenance. FocalPoint reduces the space requirements and maintenance costs of bioretention by up to 90% while providing all the water purification benefits.

- Adds aesthetic value to properties
- Cleans runoff to improve water quality
- Reduces space requirements and maintenance costs of traditional bioretention systems
- Encourages infiltration to reduce volume of water discharged
- Pair with R-Tank® to maximize water storage and transport

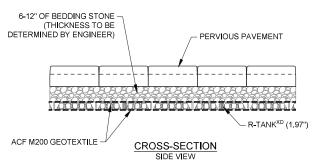




PERMEABLE PAVEMENTS

Traditional pavements move vehicles efficiently, but are easily damaged by stormwater. ACF specializes in pervious pavements that handle traffic easily while providing surface infiltration rates 10 times higher than traditional pervious pavements. High surface infiltration rates reduce the expense of long-term maintenance and the headaches that go with it.

- Handles all vehicular loads
- Drains ten times faster than competing pervious pavements
- Reduces long-term maintenance costs
- Encourages infiltration
- Pair with R-Tank® to maximize water storage and transport



MAINTENANCE

Designing an R-Tank System with longevity and maintenance in mind is a simple three-step process:

1. PREVENT

Keep debris and sediment out of the system by pre-treating runoff with the Trash Guard Plus® unit (see below). For a more centralized approach, you could consider having the R-Tank units penetrate the connecting structure, which allows the use of the R-Tank® as its own trash screen. This works best with a structure that includes a sump (see drawing to right).

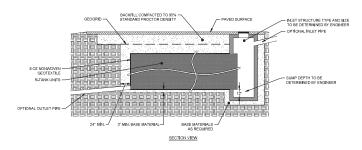
2. ISOLATE

Trap solid pollutants inside the maintenance row (see drawing to right) where they can be easily removed, using the Maintenance Modules (available in LD, HD, and UD only). These modules are wrapped in geotextile to retain solids and are fully accessible by conventional jet-vac systems to remove captured pollutants.

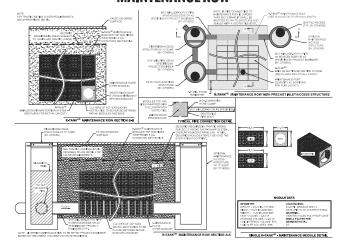
3. PROTECT

Ensure a long system life by including maintenance ports to remove any pollutants that evade the pretreatment system and maintenance row. Maintenance ports should be specified within 10' of inlet and outlet connections, and roughly 50' on center (see detail on page 7).

INLET CONNECTION



MAINTENANCE ROW



MAINTENANCE PREVENTION

TRASH GUARD PLUS®

Trash Guard Plus® is a patented stormwater pretreatment device that captures debris, sediment and floatables. Easy to install and maintain, it is a fraction of the cost of other pretreatment devices.

Benefits of Trash Guard Plus®

- Simple retrofit to existing catch basins
- Installs without heavy equipment
- Quick and easy assembly
- Adjusts to irregular catch basin bottoms and/or walls
- Eliminates eyesore stormwater trash at public parks, beaches, and waterways
- Removes harmful nutrients and regulated metals

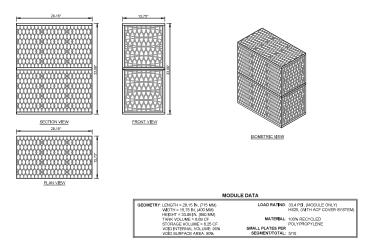




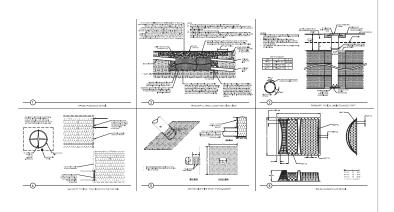
TYPICAL DESIGN

CAD DRAWINGS

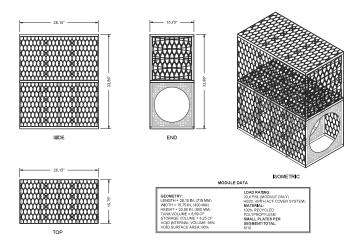
Module Drawing - Double



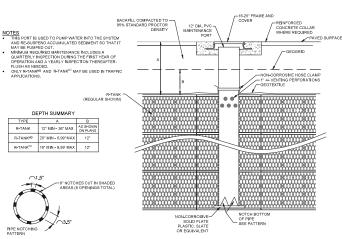
Composite Details



Maintenance Module - Double



Maintenance Port



	Selecting the Right R-Tank Module							
Cover Depth* (Inches)	LD	HD	SD	UD	XD			
Minimum 6"	Green Space - No Traffic	Green Space - No Traffic	Green Space - No Traffic	Green Space - No Traffic	HS-20			
12"	Green Space - No Traffic	Green Space - No Traffic	Green Space - No Traffic	HS-20**	HS-20			
14"	Green Space - No Traffic	Green Space - No Traffic	Green Space - No Traffic	HS-20	HS-20			
18"	Green Space - No Traffic	Green Space - No Traffic	HS-20	HS-20	HS-20			
20"	Green Space - No Traffic	HS-20	HS-20	HS-20	HS-20			
24"	Green Space - No Traffic	HS-20	HS-20	HS-20	HS-20			
36"	Green Space - No Traffic	HS-20	HS-20	HS-20	HS-20			
48"	-	HS-20	HS-20	HS-20	HS-20			
60"	-	HS-20	HS-20	HS-20	HS-20			
72"	-	HS-20	HS-20	-	HS-20			
84"	-	-	HS-20	-	HS-20			
120"	-	-	HS-20	-	HS-20			
160"	-	-	-	-	HS-20			
Maximum 200"	-	-	-	_	HS-20			

HS-20 designation based on AASHTO LRFD Bridge Design Specification for Single Lane Traffic

^{*} Cover depth is measured from the top of the module to the finished grade or top of pavement.

^{**} The UD module requires STONE backfill (not soils) on the sides at this depth.

PRODUCT SPECIFICATION 800.448.3636 acfenvironmental.com







Dimensions & Ca	apacity					
Module (Segments)	Width (inch)	Length (inch)	Height (in/ft)	Volume (cf)	Capacity (cf)	Weight* (lbs)
Mini	15.75	28.15	9.45"/0.79'	2.42	2.30	10.1/10.9
Single(1)	15.75	28.15	17.32"/1.44'	4.44	4.22	15.7/17.3
Single + Mini(1.5)	15.75	28.15	25.98"/2.17'	6.67	6.33	23.6/25.9
Double (2)	15.75	28.15	33.86"/2.82'	8.69	8.25	29.1/32.3
Double + Mini(2.5)	15.75	28.15	42.52"/3.54'	10.91	10.36	37.0/41.0
Triple (3)	15.75	28.15	50.39"/4.20'	12.93	12.28	42.5/47.4
Triple + Mini(3.5)	15.75	28.15	59.06"/4.92'	15.15	14.39	50.4/56.0
Quad(4)	15.75	28.15	66.93"/5.58'	17.17	16.31	55.9/62.4
Quad + Mini(4.5)	15.75	28.15	75.59"/6.30'	19.39	18.42	63.8/71.0
Pent(5)	15.75	28.15	83.46"/6.96'	21.41	20.34	69.3/77.4

Dimensions &	Capacity					
Module (Segments)	Width (inch)	Length (inch)	Height (in/ft)	Volume (cf)	Capacity (cf)	Weight (lbs)
Single (1)	15.75	28.15	9.45"/0.79'	2.42	2.30	10.95
Double (2)	15.75	28.15	18.12"/1.51'	4.64	4.41	19.58
Triple (3)	15.75	28.15	26.79"/2.23	6.86	6.52	28.21
Quad (4)	15.75	28.15	35.46"/2.96'	9.08	8.63	36.84
Pent (5)	15.75	28.15	44.13"/3.68'	11.30	10.74	45.47
Hex (6)	15.75	28.15	52.80"/4.40'	13.52	12.84	54.10
Septa (7)	15.75	28.15	61.47"/5.12	15.74	14.95	62.73
Octo (8)	15.75	28.15	70.14"/5.85'	17.96	17.06	71.36
Nono (9)	15.75	28.15	78.81"/6.57	20.18	19.17	79.99
Decka (10)	15.75	28.15	87.48"/7.29'	22.40	21.28	88.62

^{*}Weights shown are for LD/HD modules.





IK	RTANK
	Dimensions & Capacity

Dimensions & 0						
Module (Segments)	Width (inch)	Length (inch)	Height (in/ft)	Volume (cf)	Capacity (cf)	Weight (Ibs)
Single (1)	23.62	23.62	14.17"/1.18'	4.57	4.35	21.2
Double (2)	23.62	23.62	27.17"/2.26'	8.77	8.33	39.0
Triple (3)	23.62	23.62	40.16"/ 3.35'	12.97	12.32	56.8
Quad (4)	23.62	23.62	53.15"/4.43'	17.16	16.30	74.6
Pent (5)	23.62	23.62	66.14"/5.5'	21.35	20.29	92.4

Dimensions & Cap	oacity					
Module (Segments)	Width (inch)	Length (inch)	Height (inch)	Volume (cf)	Capacity (cf)	Weight (Ibs)
Single (1)	19.68	23.62	1.97	0.53	0.48	4
Double (2)	19.68	23.62	3.94	1.06	0.95	8
Triple (3)	19.68	23.62	5.91	1.59	1.43	12
Quad (4)	19.68	23.62	7.87	2.12	1.91	16
Pent (5)	19.68	23.62	9.84	2.65	2.38	20

Note: XD modules may be stacked up to 10' tall (60 layers).

Specificatio	ns	(F.D)	(HD)	(ED)	(FD)	SEDI
Item	Description				ريات	
Void Area	Volume available for water storage	95%	95%	95%	95%	90%
Surface Area Void	% of exterior available for infiltration	90%	90%	90%	90%	90%
Compressive Strength	ASTM D2412 / ASTM F2418	30.0 psi	33.4	42.9 psi	134.2 psi	240.2 psi
Unit Weight	Weight of plastic/cubic foot of tank	3.29 lbs/cf	3.62 lbs/cf	3.96 lbs/cf	4.33 lbs/cf	7.55 lbs/cf
Rib Thickness	Thickness of load-bearing members	0.18 inches	0.18 inches	0.18 inches	-	-
Service Temperature	Safe temperature range for use	-14 - 167º F	-14 - 167º F	-14 - 167º F	-14 - 167º F	-14 - 167º F
Recycled Content	Use of recycle polypropylene	100%	100%	100%	100%	100%
Minimum Cover	Cover required for HS-20 loading	Not Traffic Rated	20"	18"	12"-14"	6"
Minimum Cover	Cover required for HS-25 loading	Not Traffic Rated	24"	18"	15"-17"	6"
Maximum Cover	Maximum allowable cover depth	3.0'	6.99'	9.99'	5.0'	16.7'

FOCALPOINT



HIGH PERFORMANCE MODULAR BIOFILTRATION SYSTEM

NYS DEC DESIGN WORKSHEET/CHECKLIST

The New York State Department of Environmental Conservation (NYS DEC) has approved the FocalPoint (High Performance Modular Biofiltration System) as a proprietary stormwater management practice for use on New Development, Redevelopment and Retrofit Projects.

1.	FocalPoint Bed Area (min 174 square feet per acre of impervious	ıs area (e.g.	0.2 acres = 35 sf))
•	Tributary Impervious area		ac. (A)
•	Tributary Pervious area		ac. (B)
•	Min FocalPoint bed area req'd = $(((A) \times 1.0) + ((B) \times 0.4)) * 174$		
•	FocalPoint Bed Area provided *	/ =	
•	Dimensions of Proposed FocalPoint		ft xft
.1.			
* S(ee criteria 2. to determine if minimum size is appropriate.		
2.	A Type II 24hr rainfall event that generates the WQ volume shall storm volume is treated prior to activation of the overflow (type a 1.2 to 1.3" rainfall event usually generates 1 inch of runoff) co	ically set at	6-12" above the mulch) (Note:
•	Water Quality Volume Goal (WQv)		cubic feet
•	Type II 24hr Rainfall Depth to generate WQv	AND DATE OF THE PARTY.	inches
•	Temporary storage depth provided		inches (typ 6" to 12")
•	Temporary storage volume provided at above depth		cubic feet.
•	Peak ponding depth from Type II 24hr storm event		inches
3.	Size Harco Domed Overflow Riser		
•	Domed Overflow Riser:		
	o Rim Elev of Overflow Riser:	= 1000	(typ 6-12" above mulch surface)
	o Overflow Riser Diameter		(12, 15, 18, 24 or 30" dia)
	o 6" invert in Elev from FocalPoint		(typ 3 ft below mulch surface)
	o" invert out Elev	STATE OF THE PERSON NAMED IN	
•	Or other (spillway/weir etc)		
4.	RRv, Channel Protection and Flood Control/Peak flow attenuati	on of major	storms
•	The treated flow and bypass flow can be routed to a detention system system such as an expanded R-Tank system (contact ACF for addition Tank systems)		= = =
5.	The Design shall be reviewed by the manufacturer's representative.	tive prior to	submission and installation
•	The Design has been reviewed by ACF Environmental \Box Engineer will coordinate installation inspection with ACF \Box		

11.) Stormwater Management Construction Checklists

APPENDIX H

STATE POLLUTANT DISCHARGE ELIMINATION SYSTEM FOR CONSTRUCTION ACTIVITIES CONSTRUCTION SITE LOG BOOK

Table of Contents

- I. Pre-Construction Meeting Documents
 - a. Preamble to Site Assessment and Inspections
 - b. Operator's Certification
 - c. Qualified Professional's Credentials & Certification
 - d. Pre-Construction Site Assessment Checklist
- II. Construction Duration Inspections
 - a. Directions
 - b. Modification to the SWPPP
- III. Monthly Summary Reports
- IV. Monitoring, Reporting, and Three-Month Status Reports
 - a. Operator's Compliance Response Form

Properly completing forms such as those contained in Appendix H meet the inspection requirement of NYS-DEC SPDES GP for Construction Activities. Completed forms shall be kept on site at all times and made available to authorities upon request.

I. PRE-CONSTRUCTION MEETING DOCUMENTS Project Name Permit No. _____ Date of Authorization ______ Name of Operator ______ Prime Contractor ______

a. Preamble to Site Assessment and Inspections

The Following Information To Be Read By All Person's Involved in The Construction of Stormwater Related Activities:

The Operator agrees to have a qualified professional¹ conduct an assessment of the site prior to the commencement of construction² and certify in this inspection report that the appropriate erosion and sediment controls described in the SWPPP have been adequately installed or implemented to ensure overall preparedness of the site for the commencement of construction.

Prior to the commencement of construction, the Operator shall certify in this site logbook that the SWPPP has been prepared in accordance with the State's standards and meets all Federal, State and local erosion and sediment control requirements.

When construction starts, site inspections shall be conducted by the qualified professional at least every 7 calendar days and within 24 hours of the end of a storm event of 0.5 inches or greater (Construction Duration Inspections). The Operator shall maintain a record of all inspection reports in this site logbook. The site logbook shall be maintained on site and be made available to the permitting authorities upon request. The Operator shall post at the site, in a publicly accessible location, a summary of the site inspection activities on a monthly basis (Monthly Summary Report).

The operator shall also prepare a written summary of compliance with this general permit at a minimum frequency of every three months (Operator's Compliance Response Form), while coverage exists. The summary should address the status of achieving each component of the SWPPP.

Prior to filing the Notice of Termination or the end of permit term, the Operator shall have a qualified professional perform a final site inspection. The qualified professional shall certify that the site has undergone final stabilization³ using either vegetative or structural stabilization methods and that all temporary erosion and sediment controls (such as silt fencing) not needed for long-term erosion control have been removed. In addition, the Operator must identify and certify that all permanent structures described in the SWPPP have been constructed and provide the owner(s) with an operation and maintenance plan that ensures the structure(s) continuously functions as designed.

^{1 &}quot;Qualified Professional means a person knowledgeable in the principles and practice of erosion and sediment controls, such as a Certified Professional in Erosion and Sediment Control (CPESC), soil scientist, licensed engineer or someone working under the direction and supervision of a licensed engineer (person must have experience in the principles and practices of erosion and sediment control).

^{2 &}quot;Commencement of construction" means the initial removal of vegetation and disturbance of soils associated with clearing, grading or excavating activities or other construction activities.

^{3 &}quot;Final stabilization" means that all soil-disturbing activities at the site have been completed and a uniform, perennial vegetative cover with a density of eighty (80) percent has been established or equivalent stabilization measures (such as the use of mulches or geotextiles) have been employed on all unpaved areas and areas not covered by permanent structures.

b. Operators Certification

"I certify under penalty of law that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gathered and evaluated the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. Further, I hereby certify that the SWPPP meets all Federal, State, and local erosion and sediment control requirements. I am aware that false statements made herein are punishable as a class A misdemeanor pursuant to Section 210.45 of the Penal Law.

Name (please print):		
Title	Date:	
Address:		
	Email:	
Signature:		
c. Qualified Profession	al's Credentials & Certification	
project and that the appro- the following Pre-constru	beet the criteria set forth in the General Permit to conduct site inspections for priate erosion and sediment controls described in the SWPPP and as described in Site Assessment Checklist have been adequately installed or implementation of this site for the commencement of construction."	ibed in
Name (please print):		
Title	Date:	
Address:		
Phone:E	mail:	

Signature: _

d. Pre-construction Site Assessment Checklist (NOTE: Provide comments below as necessary) 1. Notice of Intent, SWPPP, and Contractors Certification: Yes No NA [] [] Has a Notice of Intent been filed with the NYS Department of Conservation? [] [] Is the SWPPP on-site? Where? [] [] Is the Plan current? What is the latest revision date? [] [] Is a copy of the NOI (with brief description) onsite? Where? [] [] Have all contractors involved with stormwater related activities signed a contractor's certification? 2. Resource Protection Yes No NA [] [] Are construction limits clearly flagged or fenced? [] [] Important trees and associated rooting zones, on-site septic system absorption fields, existing vegetated areas suitable for filter strips, especially in perimeter areas, have been flagged for protection. [] [] Creek crossings installed prior to land-disturbing activity, including clearing and blasting. 3. Surface Water Protection Yes No NA [] [] Clean stormwater runoff has been diverted from areas to be disturbed. [] [] Bodies of water located either on site or in the vicinity of the site have been identified and protected. [] [] Appropriate practices to protect on-site or downstream surface water are installed. [] [] Are clearing and grading operations divided into areas <5 acres? 4. Stabilized Construction Entrance Yes No NA [] [] A temporary construction entrance to capture mud and debris from construction vehicles before they enter the public highway has been installed. [] [] Other access areas (entrances, construction routes, equipment parking areas) are stabilized immediately as work takes place with gravel or other cover. [] [] Sediment tracked onto public streets is removed or cleaned on a regular basis. 5. Perimeter Sediment Controls Yes No NA [] [] Silt fence material and installation comply with the standard drawing and specifications. [] [] Silt fences are installed at appropriate spacing intervals [] [] Sediment/detention basin was installed as first land disturbing activity.

New York Standards and Specifications
For Erosion and Sediment Control

[] [] Sediment traps and barriers are installed.

avoidance and response plan.

[] [] The plan is contained in the SWPPP on page

Yes No NA

6. Pollution Prevention for Waste and Hazardous Materials

[] [] Appropriate materials to control spills are onsite. Where?

[] [] The Operator or designated representative has been assigned to implement the spill prevention

II. CONSTRUCTION DURATION INSPECTIONS

a. Directions:

Inspection Forms will be filled out during the entire construction phase of the project. Required Elements:

- (1) On a site map, indicate the extent of all disturbed site areas and drainage pathways. Indicate site areas that are expected to undergo initial disturbance or significant site work within the next 14-day period;
- (2) Indicate on a site map all areas of the site that have undergone temporary or permanent stabilization;
- (3) Indicate all disturbed site areas that have not undergone active site work during the previous 14-day period;
- (4) Inspect all sediment control practices and record the approximate degree of sediment accumulation as a percentage of sediment storage volume (for example, 10 percent, 20 percent, 50 percent);
- (5) Inspect all erosion and sediment control practices and record all maintenance requirements such as verifying the integrity of barrier or diversion systems (earthen berms or silt fencing) and containment systems (sediment basins and sediment traps). Identify any evidence of rill or gully erosion occurring on slopes and any loss of stabilizing vegetation or seeding/mulching. Document any excessive deposition of sediment or ponding water along barrier or diversion systems. Record the depth of sediment within containment structures, any erosion near outlet and overflow structures, and verify the ability of rock filters around perforated riser pipes to pass water; and
- (6) Immediately report to the Operator any deficiencies that are identified with the implementation of the SWPPP.

Page 1 of _____ CONSTRUCTION DURATION INSPECTIONS SITE PLAN/SKETCH **Date of Inspection** Inspector (print name) **Qualified Professional (print name) Qualified Professional Signature** The above signed acknowledges that, to the best of his/her knowledge, all information provided on the

forms is accurate and complete.

Maintaining Water Quality

Yes	No NA
[] []	[] [] Is there an increase in turbidity causing a substantial visible contrast to natural conditions? [] [] Is there residue from oil and floating substances, visible oil film, or globules or grease? [] [] All disturbance is within the limits of the approved plans. [] [] Have receiving lake/bay, stream, and/or wetland been impacted by silt from project?
Hoı	ısekeeping
1. G	General Site Conditions
	No NA
[]	 [] [] Is construction site litter and debris appropriately managed? [] Are facilities and equipment necessary for implementation of erosion and sediment control in working order and/or properly maintained?
[]	[] [] Is construction impacting the adjacent property? [] [] Is dust adequately controlled?
	emporary Stream Crossing
	No NA
[] []	[] [] Maximum diameter pipes necessary to span creek without dredging are installed. [] [] Installed non-woven geotextile fabric beneath approaches.
[]	[] [] Is fill composed of aggregate (no earth or soil)?
[]	[] [] Rock on approaches is clean enough to remove mud from vehicles & prevent sediment from entering stream during high flow.
Rui	noff Control Practices
1. E	xcavation Dewatering
	No NA
[] []	 [] Upstream and downstream berms (sandbags, inflatable dams, etc.) are installed per plan. [] Clean water from upstream pool is being pumped to the downstream pool. [] Sediment laden water from work area is being discharged to a silt-trapping device. [] Constructed upstream berm with one-foot minimum freeboard.
2. L	evel Spreader
	No NA
	[] [] Installed per plan.
[]	[] [] Constructed on undisturbed soil, not on fill, receiving only clear, non-sediment laden flow. [] [] Flow sheets out of level spreader without erosion on downstream edge.
	nterceptor Dikes and Swales
	No NA
[]	[] [] Installed per plan with minimum side slopes 2H:1V or flatter.
[]	 [] Stabilized by geotextile fabric, seed, or mulch with no erosion occurring. [] Sediment-laden runoff directed to sediment trapping structure

Page 3 of _____ CONSTRUCTION DURATION INSPECTIONS **Runoff Control Practices (continued)** 4. Stone Check Dam Yes No NA [] [] Is channel stable? (flow is not eroding soil underneath or around the structure). [] [] Check is in good condition (rocks in place and no permanent pools behind the structure). [] [] Has accumulated sediment been removed?. 5. Rock Outlet Protection Yes No NA [] [] Installed per plan. [] [] Installed concurrently with pipe installation. Soil Stabilization 1. Topsoil and Spoil Stockpiles Yes No NA [] [] Stockpiles are stabilized with vegetation and/or mulch. [] [] Sediment control is installed at the toe of the slope. 2. Revegetation Yes No NA [] [] Temporary seedings and mulch have been applied to idle areas. [] [] 4 inches minimum of topsoil has been applied under permanent seedings **Sediment Control Practices** 1. Stabilized Construction Entrance Yes No NA [] [] Stone is clean enough to effectively remove mud from vehicles. [] [] Installed per standards and specifications? [] [] Does all traffic use the stabilized entrance to enter and leave site? [] [] Is adequate drainage provided to prevent ponding at entrance? 2. Silt Fence

[] [] Installed on Contour, 10 feet from toe of slope (not across conveyance channels).
[] [] Joints constructed by wrapping the two ends together for continuous support.

[] [] Posts are stable, fabric is tight and without rips or frayed areas.

[] [] Fabric buried 6 inches minimum.

Sediment accumulation is ___% of design capacity.

Yes No NA

CONSTRUCTION DURATION INSPECTIONS

Page 4 of _____

Sediment Control Practices (continued)

3. Storm Drain Inlet Protection (Use for Stone & Block; Filter Fabric; Curb; or, Excavated practices)
Yes No NA
[] [] Installed concrete blocks lengthwise so open ends face outward, not upward.
[] [] Placed wire screen between No. 3 crushed stone and concrete blocks.
[] [] Drainage area is 1 acre or less.
[] [] Excavated area is 900 cubic feet.
[] [] Excavated side slopes should be 2:1.
[] [] 2" x 4" frame is constructed and structurally sound.
[] [] Posts 3-foot maximum spacing between posts.
[] [] Fabric is embedded 1 to 1.5 feet below ground and secured to frame/posts with staples at max 8
inch spacing.
[] [] Posts are stable, fabric is tight and without rips or frayed areas.
Sediment accumulation% of design capacity.
4. Temporary Sediment Trap
Yes No NA
[] [] Outlet structure is constructed per the approved plan or drawing.
[] [] Geotextile fabric has been placed beneath rock fill.
Sediment accumulation is% of design capacity.
5. Temporary Sediment Basin
Yes No NA
[] [] Basin and outlet structure constructed per the approved plan.
[] [] Basin side slopes are stabilized with seed/mulch.
[] [] Drainage structure flushed and basin surface restored upon removal of sediment basin facility.
Sediment accumulation is% of design capacity.
Note: Not all erosion and sediment control practices are included in this listing. Add additional pages
to this list as required by site specific design.
Construction inspection checklists for post-development stormwater management practices can
be found in Appendix F of the New York Stormwater Management Design Manual.

CONSTRUCTION DURATION INSPECTIONS

b. Modifications to the SWPPP (To be completed as described below)

The Operator shall amend the SWPPP whenever:

- 1. There is a significant change in design, construction, operation, or maintenance which may have a significant effect on the potential for the discharge of pollutants to the waters of the United States and which has not otherwise been addressed in the SWPPP; or
- 2. The SWPPP proves to be ineffective in:
 - a. Eliminating or significantly minimizing pollutants from sources identified in the SWPPP and as required by this permit; or
 - b. Achieving the general objectives of controlling pollutants in stormwater discharges from permitted construction activity; and
- 3. Additionally, the SWPPP shall be amended to identify any new contractor or subcontractor that will implement any measure of the SWPPP. **Modification & Reason:**

III. Monthly Summary of Site Inspection Activities

Name of Permitt	ted Facility:		Today's Date: Reporting Month			
Location:			Permit Identification #:			
Name and Telep	hone Number of Site Inspec	ctor:		vv =-		
Date of Inspection	Regular / Rainfall based Inspection	Name of Inspector	r Iter	ms of Concern		
				APAGE PROPERTY.		

-						
Owner/Onera	tor Certification:					
"I certify under paccordance with submitted. Based gathering the info	enalty of law that this docum a system designed to assure the on my inquiry of the person formation, the information sub ware that false statements man	hat qualified personnel prop or persons who manage the mitted is, to the best of my l	erly gathered and eva system, or those perso knowledge and belief	luated the information ons directly responsible for true, accurate, and		
Signature of Permi	ttee or Duly Authorized Represe	ntative Name of Per	mittee or Duly Authoriz	zed Representative Date		
Duly authorized documents.	representatives must have	e written authorization, su	bmitted to DEC, to	sign any permit		

NYSDEC SPDES General Permit for Stormwater Discharges from Construction Activity Monthly Summary of Site Inspection Activities Permit Number GP-02-01

Name of Permitted Facility:		Permit Identification #:	
Location:		Today's Date:	Reporting Month:
Name and Telephone Number of Site Inspector:	Name and Telephone Number of Site Inspector:	er of Site Inspector:	

Permit Reference; Part III.D.3.b (page 15):

"The operator shall post at the site, in a publich-accessible location, a summary of the site inspection activities on a monthly basis."

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Σ.	Date	Corrected							
The operator strait post at the site, in a particly-accessione tocation, a summary of the site inspection activities on a monthly basis.	Major items of concern related to compliance of the	SWPPP with all conditions of the general permit							
me sue, m a paviiciy-accessivie iocam	Name of Qualified Professional	conducting Site Inspections							
ne operator snatt post at		Inspection and 24 hr Rainfall							
7	Date of	Inspection							

Owner/Operator Certification:

persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I am aware "I certify under penalty of law that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gathered and evaluated the information submitted. Based on my inquiry of the person or persons who manage the system, or those that false statements made herein are punishable as a class A misdemeanor pursuant to Section 210.45 of the Penal Law."

Date	any permit documents.
Name of Permittee or Duly Authorized Representative	perator) must have written authorization, submitted to DEC, to sign a
Signature of Permittee or Duly Authorized Representative	Duly authorized representatives of the Permittee (Owner/O

Inspection and Maintenance Checklist Catch Basins, Manholes, and Inlets

Date:								
Type of Inspection:	Storm 🗌	Weekly		Monthly		Annual		
Site:		Ir	nspector(s)	:				
Description or location of Project:								

Defect	Conditions when Maintenance is Needed	Maintenance (1 or 2)*	Comments
General		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	A Dispress (i.i.d. affice dispress
Trash and Debris	Trash and debris which are		
	located immediately in front of		
	the catch basin opening or is		
	blocking inletting capacity of the		
	basin by more than 10%.		
	Trash or debris (in the basin) that		
	exceeds 60 percent of the sump		
	depth as measured from the		
	bottom of basin to invert of the		
	lowest pipe into or out of the		
	basin, but in no case less than a		
	minimum of six inches clearance		
	from the debris surface to the		
	invert of the lowest pipe.		
	Trash or debris in any inlet or		
	outlet pipe blocking more then		
	1/3 of its height.		
	Dead animals or vegetation that		
	could generate odors that could		
	cause complaints or dangerous		
	gases (e.g., methane).		
Sediment	Sediment (in the basin) that		
	exceeds 60 percent of the sump		
	depth as measured from the		
	bottom of basin to invert of the		
	lowest pipe into or out of the		
	basin, but in no case less than a		
	minimum of 6 inches clearance		
	from the sediment surface to the		
	invert of the lowest pipe.		
Structure Damage to	Top slab has holes larger than 2		
Frame and/or Top Slab	square inches or cracks wider		
	then ¼ inch.		
	Frame not sitting flush on top		
	slab, i.e., separation of more		
	than ¾ inch of the frame from		
	the top slab. Frame not securely		
	attached.		

^{*}Maintenance: Enter 1 if maintenance is needed. Enter 2 if maintenance was preformed same day.

energi (1918) i propinski	Conditions when Maintenance **		el Cresto.
Defect:	1997 a Grand of State	(1 of 2)†	Comments
Fractures or Cracks in	Maintenance person judges that		
Basin Walls/Bottom	structure is unsound.		
	Grout fillet has separated or		
	cracked wider then ½ inch and		
	longer than 1 foot at the joint of		
	any inlet/outlet pipe or any		
	evidence of soil particles		
	entering catch basin through		
	cracks.		
Settlement/Misalignment	If failure of basin has created a		
	safety, function, or design		
	problem.		
Vegetation	Vegetation growing across and		
	blocking more than 10% of the		
	basin opening.		
	Vegetation growing in		
	inlet/outlet pipe joints that is		
	more than 6 inches tall and less		
	than 6 inches apart.		
Contamination and	Any evidence of oil, gasoline,		
Pollution	contaminants or other		
	pollutants.		
Catch Basin Cover			
Cover Not in Place	Cover is missing or only partially		
	in place. Any open catch basin		
	requires maintenance.		
Locking Mechanism Not	Mechanism cannot be opened by		
Working	one maintenance person with		
9	proper tools. Bolts into frame		
	have less than ½ inch of thread.		
Cover Difficult to Remove	One maintenance person cannot		
	remove lid after applying normal		
	lifting pressure.		
	(Intent is keep cover from sealing		
	off access to maintenance).		
Ladder	on access to maintenance).		
Ladder Rungs Unsafe	Ladder is unsafe due to missing		
Ladder Rangs onsare	rungs, not securely attached to		
	basin wall, misalignment, rust,		
	cracks, or sharp edges.		
Metal Grates (If Applicable	· · · · · · · · · · · · · · · · · · ·		
Grate opening Unsafe			
Grate opening offsale	Grate with opening wider than		
Totals and Dalada	7/8 inch.		
Trash and Debris	Trash and debris that is blocking		
	more than 20% of grate surface		
	inletting capacity.		
Damaged or Missing	Grate missing or broken		
	member(s) of the grate.		

^{*}Maintenance: Enter 1 if maintenance is needed. Enter 2 if maintenance was preformed same day.

Inspection and Maintenance Checklist Conveyance Systems (Pipes & Ditches)

Date:				
Type of Inspection:	Storm 🗆	Weekly 🗆	Monthly 🗌	Annual 🗆
Site:	te: Inspector(s):			
translation (1) G	onditions When M	alintenance Walin	(enance	
Tofaet is				

	Conditions When Maintenance	Maintenance.	
Defect:	is Needed		Comments (**)
Pipes			
Sediment &	Accumulated Sediment that		
Debris	exceeds 20% of the diameter of		
	the pipe.		
Vegetation	Vegetation that reduces free		
	movement of water through		
	pipes		
Damaged Pipe	Protective coating is damaged;		
	rust is causing more than 50%		
	deterioration to any part of		
	pipe.		
	Any dent that decreases the		
	cross section area of pipe by		
	more than 20% or puncture that		
- ···	impacts performance.		
Open Ditches			
Trash and Debris	Trash and debris > 5 cf/1000 sf		
	(one standard size garbage can)		
	Visual evidence of dumping		
Sediment	Accumulated sediment that		
	exceeds 20% of the design		
	depth.		
Vegetation	Vegetation that reduces free		
	movement of water through		
	ditches.		
Erosion Damage	Eroded damage over 2 inches		
to Slopes and	deep where cause of damage is		
Channel Bottom	still present or where there is		
Deal Hair Out 6	potential for continued erosion.		
Rock Lining Out of	Maintenance person can see		
Place or Missing	native soil beneath the rock		
(If Applicable)	lining.		

^{*}Maintenance: Enter 1 if maintenance is needed. Enter 2 if maintenance was preformed same day.